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STORMWATER MANAGEMENT REPORT

PREPARED FOR:

EDGEWATER HILL ENTERPRISES, LLC

SALT POND APARTMENTS
000 EAST HIGH STREET (CT ROUTE 66)
EAST HAMPTON, CONNECTICUT

DECEMBER 2020
REVISED JANUARY 19, 2021
(PER TRINKAUS ENGINEERING LLC REVIEW)

PREPARED BY:

BOUNDARIES LLC

PROJECT I.D. No. 20-2853



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Introduction

On behalf of Edgewater Hill Enterprises, LLC., Boundaries, LLC. has prepared the following stormwater management report for the proposed forty-unit multifamily residential development located south of the East Hampton Town Hall and Police Department in the Edgewater Hill Mixed Use Development. Additional supporting information regarding the proposed development and the construction completed to date can be found in the approved development Master Plan documents prepared by others. The following analysis demonstrates that the proposed stormwater management system provides retention of the water quality volume and attenuation of peak stormwater flows.

The location of the project is shown on the Locus Map included as Figure 1. The FEMA Flood Insurance Rate Map is included as Figure 2.

Wetlands located on the subject properties include an existing man-made pond located in the central portion of the proposed development and upgradient wetland areas that contribute to the pond. Stormwater runoff from the man-made pond and from upgradient undeveloped and developed areas ultimately discharge through a series of open channels and pipes to Lake Pocotopaug.

According to the Natural Resources Conservation Service (NRCS) Web Soil Survey the soils in the project area consist of Woodbridge fine sandy loam, 8 to 15% slopes, very stony, and Paxton and Montauk fine sandy loams, 15 to 35% slopes, extremely stony. Woodbridge soils are classified as Hydrologic Soil Group C/D and Paxton and Montauk soils are classified as Hydrologic Soil Group C. The NRCS Web Soil Survey Soils Report is provided in Appendix A. Given that the soils in the project area are classified as Hydrologic Soil Group C little to no infiltration of runoff is anticipated as part of the stormwater management system.

Pre- and post-development conditions hydrographs were estimated using the hydrologic modeling program HydroCAD. The methodology selected was NRCS TR-20. Times of concentration were estimated using multiple segment flow paths as described in the NRCS TR-55 manual. The Type III 24-hour storm was analyzed under antecedent moisture condition two (2). Rainfall totals were as reported by the NOAA Precipitation Frequency Data Server accessed on April 27, 2020. HydroCAD modeling results are presented in Appendix B. Pipe sizing calculations were completed using the calculated Manning's capacity of the pipe reaches. The water quality volume was calculated using the methods detailed in the CT DEEP Stormwater Quality Manual. Supporting calculations are included in Appendix C.

The proposed improvements include the construction of five (5) eight (8) unit apartment buildings, approximately 800 linear feet of new access roadway, associated sidewalks, circulation drives and parking areas and the extension of sewer, water, gas, electric and communications utilities to service the proposed buildings. Stormwater runoff from the proposed impervious areas will be collected in catch basins with prior to discharging to two (2) stormwater basins for detention of peak stormwater runoff rates. The low-level outlets of the stormwater basins are elevated above the basin bottoms to retain the water quality volume on-site following storm events. The bottom of the basins will function as constructed stormwater wetlands providing treatment of all stormwater runoff. Runoff will discharge to the wetlands system upgradient of the manmade pond in the same location as an existing drainage discharge installed as part of the Town Hall and Police Department project. The proposed site development plans are included in Appendix D. The stormwater basins are intended to provide attenuation of post-development peak discharge rates to match pre-development rates, treatment of stormwater runoff, and retention of the water quality volume following storm events. The stormwater management system has been designed to meet the requirements of the Connecticut Department of Energy and Environmental Protection (CT DEEP)



Stormwater Quality Manual for both peak stormwater runoff flow rate attenuation and retention of the stormwater quality volume for the 2, 10, 25, 50 and 100-year storm events.

Pre-Development Conditions

The Edgewater Hill development is located within the Edgewater Hill Mixed Use Development District. The development is being completed utilizing a phased approach. To date, the first two buildings in the Market Square area, the first phase of residential apartment buildings and the new Town Hall and Police Department have been constructed. A third mixed use commercial building in Market Square and additional residential lots are currently under construction. The project area formerly included a motel, residential properties and associated infrastructure. Runoff from the frontage along East High Street (CT Route 66) drains to CT DOT's 30-inch RCP culvert that carries flow under CT Route 66 and ultimately discharges to Lake Pocotopaug. Stormwater runoff from the Town Hall and Police Department, apartments, a small portion of the residential development and upgradient undeveloped areas flows to the existing pond. The pond is drained through an 18-inch diameter HDPE pipe that discharges to the stormwater management system in Edgewater Circle. Runoff from the remainder of the site flows overland to the east (away from State facilities and Lake Pocotopaug) and is not included in this analysis. Existing conditions aerial photography of the properties is shown below.



Aerial Photograph of Site

Pre-development watersheds are shown on Figure 3. Pre-development watersheds were delineated using topographic survey data for the subject parcels and aerial mapping for off-site contributing areas. Land uses were estimated using aerial photography and topographic survey data. The pre-development



conditions analyzed in the model are based on the conditions before the Edgewater Hill project was initiated. DA-APT EX is the ±9.3-acre wooded area that will be developed as part of this project. The weighted CN of the watershed is 70. Runoff from this area flows overland to the wetland areas upgradient of the manmade pond. Reported peak flow rates are summarized below in Table 1. Detailed modeling results are included in Appendix B.

Runoff Curve Numbers (CN) used for the pre-development conditions analysis are as follows: 70 (woods with good ground cover) for wooded areas in Hydrologic Soil Group C and 77 (woods with good ground cover) for wooded areas in Hydrologic Soil Group D.

Table 1
Peak Runoff Rates – Pre-Development Conditions – Apartments Sub-Watershed

Design Storm Event	Apartments Sub-Watershed Peak Runoff Rate – Link 2L (CFS)
2-Year	6.77
10-Year	17.25
25-Year	24.52
50-Year	30.21
100-Year	36.44



Post-Development Conditions

The proposed improvements include the construction of approximately 800 feet of paved road, parking areas and circulation drives to serve the new apartment buildings. Stormwater runoff will be collected in deep sump catch basins with hooded outlets at the downstream structures. The catch basins will discharge to two stormwater basins intended to attenuate peak runoff rates. The water quality volume will be retained below the low-level outlets on the two stormwater basins following storm events.

The proposed stormwater management system components proposed for construction include the following:

- Fourteen (14) deep sump precast concrete catch basins;
- Seven (7) precast concrete drainage manholes;
- Two (2) precast concrete outlet control structures;
- Yard drains, cleanouts and drainage pipe of various diameters; and
- Two stormwater basins.

The proposed stormwater management system is intended to meet the following design standards:

- The post-development peak discharge rates from the 2-year, 10-year, 25-year, 50-year, and 100-year storms are less than or equal to pre-development peak discharge rates;
- The conveyance system leading to, from, and through stormwater management facilities has capacity for the 10-year, 24-hour storm, at a minimum;
- The groundwater recharge volume is captured;
- Stormwater runoff is treated by the constructed stormwater wetlands; and
- The water quality volume is retained following storm events.

The post-development conditions hydrologic model includes the proposed apartments, supporting infrastructure and areas contributing runoff to the proposed stormwater collection system and stormwater basins. Post-development conditions watersheds are shown on Figure 4. Post-development conditions watersheds were delineated using topographic survey data and the proposed development plans for the subject areas. Land uses were estimated using aerial photography and the proposed development plans. Site development plans are included in Appendix D.

Runoff Curve Numbers (CN) used for the post-development conditions analysis are as follows: 70 (woods with good ground cover) for wooded areas in Hydrologic Soil Group C, 77 (woods with good ground cover) for wooded areas in Hydrologic Soil Group D, 74 (>75% grass cover) for the grassed areas in Hydrologic Soil Group C, 80 (>75% grass cover) for the grassed areas in Hydrologic Soil Group D, and 98 (impervious) for existing and proposed impervious areas such as paved roads, driveways, buildings, and the stormwater basin surface.

The proposed conditions watersheds are described further below:

Drainage Area #2E (DA #2E)

This 3.0± acre watershed encompasses a portion of the southern half of the proposed apartments and contributing areas, and is comprised of the proposed buildings, parking lots and access drives, revegetated areas to be graded, and wooded areas that will remain undisturbed. The weighted CN of the watershed is 83. Runoff from this area will be collected by a series of catch basins and will discharge to Stormwater Basin 2.



Drainage Area #2F (DA #2F)

This 0.2± acre watershed encompasses the revegetated areas to be graded and wooded areas that will remain undisturbed which directly drain to Stormwater Basin 2. The weighted CN of the watershed is 86. Runoff from this area will flow overland and directly discharge to Stormwater Basin 2.

Drainage Area #2G (DA #2G)

This 0.6± acre watershed encompasses the revegetated areas to be graded that will directly drain to Stormwater Basin 1. The weighted CN of the watershed is 84. Runoff from this area will flow overland and directly discharge to Stormwater Basin 1.

Drainage Area #2H (DA #2H)

This 2.7± acre watershed encompasses the western half of the proposed apartments and contributing areas, and is comprised of the proposed buildings, parking lots and access drives, revegetated areas to be graded, and wooded areas that will remain undisturbed. The weighted CN of the watershed is 84. Runoff from this area will be collected by a series of catch basins and discharge to Stormwater Basin 1.

Drainage Area #2I (DA #2I)

This 0.5± acre watershed encompasses the eastern half of the northern apartments and contributing areas, and is comprised of the proposed buildings, parking lots and access drives, and revegetated areas to be graded. The weighted CN of the watershed is 92. Runoff from this area will be collected by a series of catch basins and discharge to Stormwater Basin 1.

Drainage Area #2J (DA #2J)

This 2.3± acre watershed encompasses the portion of the project area between the development and the wetlands boundary and areas that drain off site without entering the stormwater collection system. The area is comprised of a portion of the access road, undisturbed wooded areas, and grassed areas between the stormwater basin and the wetlands boundary. The weighted CN of the watershed is 80. Runoff from this area flows off-site overland.

Post-development conditions peak runoff rates were analyzed at the wetland boundary adjacent to the proposed development area. Comparisons of pre- and post-development peak runoff rates are presented below in Table 2.

Table 2

Peak Runoff Rates – Post-Development Conditions vs. Pre-Development Conditions – Apartments Only

Storm Event	Post-Development Conditions Total Off-Site Peak Runoff Rate – Link 20L (CFS)	Pre-Development Conditions Total Off-Site Peak Runoff Rate – Pond 2P (CFS)	Change in Peak Runoff Rate (CFS)
2-Year	5.97	6.77	-0.80
10-Year	13.70	17.25	-3.55
25-Year	20.53	24.52	-3.99
50-Year	23.57	30.21	-6.64
100-Year	27.76	36.44	-8.68

As presented above, the proposed stormwater management system does not result in increases to off-site flow rates or water surface elevations, and meets the recommendations of the CT DEEP Stormwater Quality Manual for peak flow rate attenuation.



Stormwater Management System Design

Pipe Sizing

Stormwater runoff from the proposed development area will be collected and discharged to two (2) stormwater basins. The proposed stormwater collection system consists of catch basins and curbing along the proposed roadway and parking lots. The proposed drains are sized for the 10-year storm event, at a minimum, based on the calculated Manning’s capacity of each pipe reach in accordance with the Town of East Hampton Zoning Regulations. Pipe sizing calculations are included in Appendix C.

Scour Protection

The piped discharge and overflow spillway will be protected from erosion by rip rap sized in accordance with the recommendations of the CT DEEP Stormwater Quality Manual. Sizing calculations for the scour protection are summarized in Table 3 and included in Appendix C.

Table 3
Scour Protection Sizing

Stormwater Discharge	25-year Discharge Flow (CFS)	Proposed Surface Treatment	Sizing Reference
Stormwater Basin 1 Inlet	24.3	Modified Rip Rap Apron	Per 2002 CT DEEP SESC Guidelines Chapter 5-10 Outlet Protection
Stormwater Basin 2 Inlet	13.1	Modified Rip Rap Apron	

Water Quality Volume

The stormwater management system is intended to provide treatment of the runoff from the proposed impervious areas. Treatment of runoff from the site will be accomplished using a treatment train consisting of sediment forebays in each stormwater basin and the constructed stormwater wetlands system following the sediment forebay. The stormwater basins are sized to retain the water quality volume associated with the upgradient impervious areas in the storage provided below the low-level outlets. The sediment forebays are sized for 25% of the water quality volume. Sizing calculations for the stormwater basins are summarized in Table 4 and are included in Appendix C.

Table 4
Water Quality Volume Sizing Criteria

Stormwater Basin	Contributing Impervious Area	Contributing Drainage Area	Water Quality Volume	Forebay Volume	Storage Volume Below Low-Level Outlet
Stormwater Basin 1	2.31 acres	7.00 acres	7,674 cubic feet	2,260 cubic feet (29.5%)	7,932 cubic feet (103.4%)
Stormwater Basin 2	0.99 acres	3.28 acres	3,278 cubic feet	1,516 cubic feet (46.3%)	3,293 cubic feet (100.5%)

Test holes were completed in the area of the stormwater basins to confirm soil conditions. The bottom of each basin was found to be above ledge rock encountered in the test holes. The soil profile also included a restrictive layer that varied from 3.5 feet in thickness to 4.5 feet in thickness overlaying a layer fine to medium sand with gravel. This restrictive layer has resulted in a perched groundwater table. The perched groundwater table will help in the establishment of wetland plant species in the constructed



stormwater wetland. Soil berms will also be constructed in the bottom of the basin to increase contact time between the vegetation and the runoff. This system will provide treatment of the water quality volume prior to discharge. Stormwater treatment calculations prepared by Trinkaus Engineering, LLC. are included in Appendix C.

Groundwater Recharge Volume

The soils in the project area are mapped as Hydrologic Soil Group C/D and as such have limited ability for infiltration of stormwater. As mentioned above, the limiting factor for infiltration of runoff is a compact layer of silty sand that results in a perched groundwater table. The groundwater recharge volume calculations are included in Appendix C and summarized below in Table 5. The volume of water retained in the bottom of the stormwater basins exceeds the groundwater recharge volume.

Table 5
Groundwater Recharge Volume Sizing Criteria

Sizing Criteria	Result
Groundwater Recharge Volume	926 cubic feet
Total Storage Volume in Stormwater Basins	11,225 cubic feet

Construction Phase Stormwater Management

Construction phase stormwater management is intended to be provided in accordance with the erosion and sedimentation control plans included in the Site Development Plans. The following best management practices will be implemented to protect downstream water quality:

- The downgradient sediment barrier will be a compost filter tube.
- An upgradient sediment fence barrier embedded in wood chip berm will be installed to divert clean runoff around the disturbed areas.
- Grubbing of stumps is intended to be completed by phase.
 - Phase 1 includes the construction of the haul road and staging/stockpile area. Disturbed area will be approximately 1.8 acres. Disturbed areas outside of the gravel road surface will be seeded and mulched.
 - Phase 2 includes the extension of the proposed roadway, sidewalks and utilities. Disturbed areas will be approximately 2.3 acres.
 - Phase 3 includes the mass earthwork required to establishing the pad sites for the proposed buildings. Disturbed area will be approximately 4.7 acres.
- Intermediate sediment barriers will be installed during grading operations.
- Water bars will be constructed in the roadway to direct runoff to the sediment traps.
- Sediment traps are sized for 134 cubic yards of storage per acre of upgradient contributing area.
- Temporary seeding with perennial rye grass is intended for all stockpiles and disturbed areas that will remain unworked for greater than 21 days.

Temporary sediment trap sizing criteria is included in Appendix C and summarized below in Table 6.



Table 6
Temporary Sediment Trap Sizing Criteria

Temporary Sediment Trap	Contributing Area	Storage Volume Required	Storage Volume Below Spillway Elevation
Temporary Sediment Trap 1	2.4 acres	8,683 cubic feet	8,994 cubic feet
Temporary Sediment Trap 2	3.34 acres	12,084 cubic feet	13,280 cubic feet
Temporary Sediment Trap 3	0.25 acres	905 cubic feet	1,037 cubic feet

At the completion of construction, the temporary sediment traps will be backfilled, brought to design grades and loamed and seeded for final restoration.

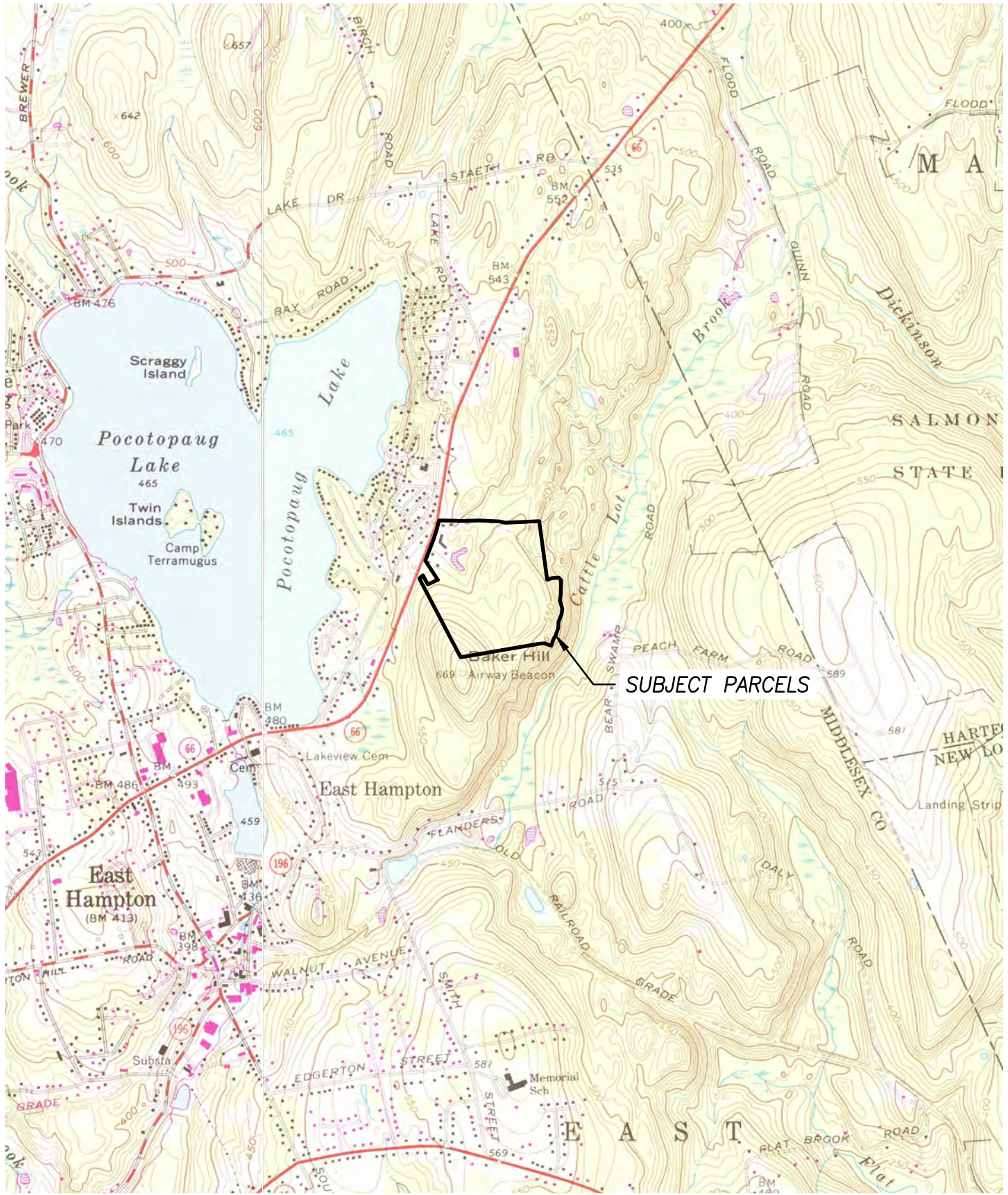
Summary

The proposed stormwater management system is intended to comply with the applicable requirements of CT DEEP and the Town of East Hampton.

The proposed improvements are shown on plans titled “Site Development Plan, Salt Pond Apartments, Prepared for Edgewater Hill Enterprises, LLC., 000 East High Street, East Hampton, Connecticut, December 2020, Job I.D. No. 20-2853, Sheet 1 through Sheet 25 of 25” prepared by Boundaries LLC.



Figures

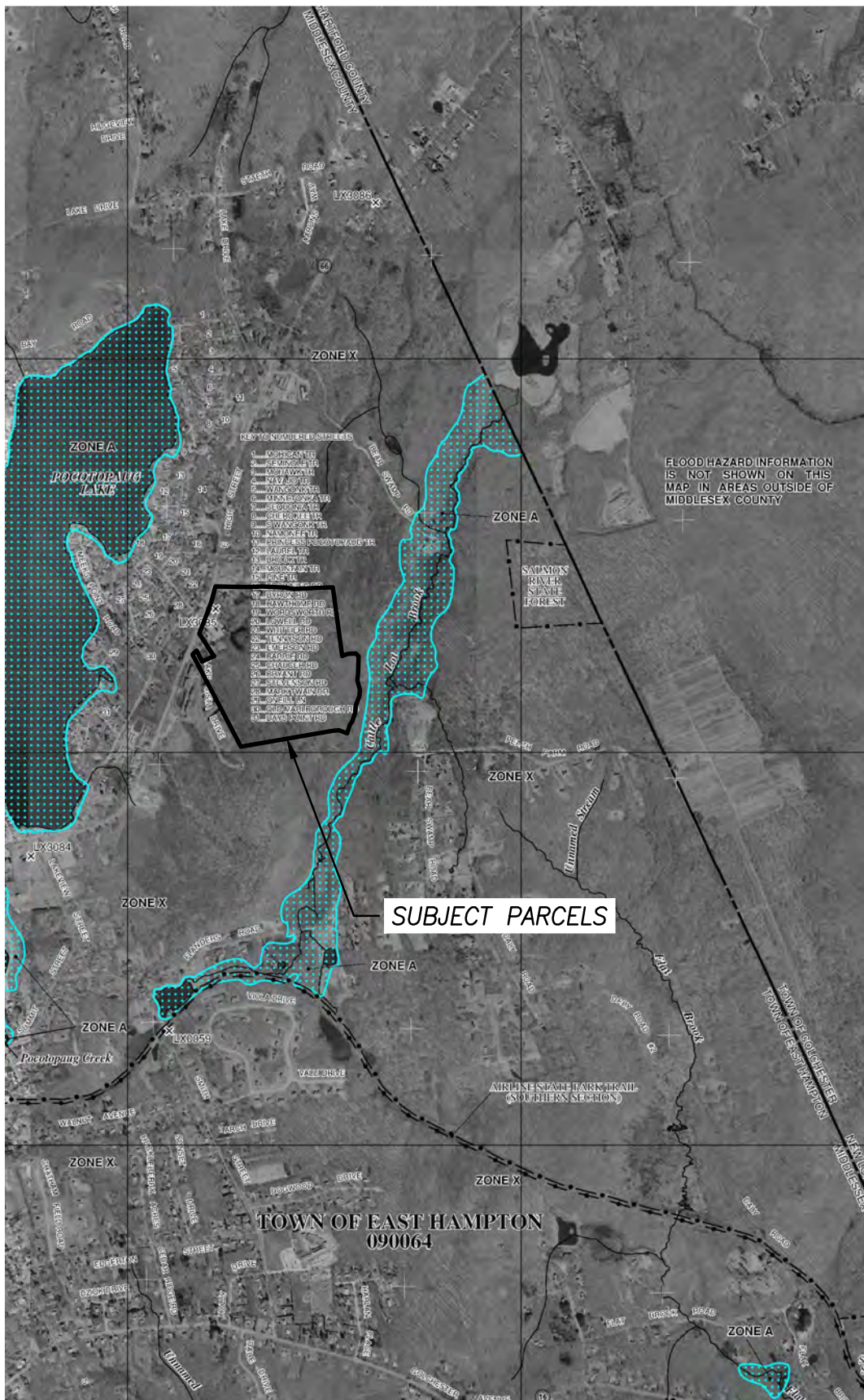


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Locus Map
 (Middle Haddam - 68 / Moodus - 69 Quads)
Salt Pond Apartments
 East High Street, East Hampton, CT

SCALE:	1"=2,000'
DATE:	December 2020
JOB NO.	20-2853
FIGURE	1



NFIP PANEL 0155G

FIRM
FLOOD INSURANCE RATE MAP
MIDDLESEX COUNTY,
CONNECTICUT
(ALL JURISDICTIONS)

SEE MAP INDEX FOR FIRM PANEL LAYOUT

CONTAINS:
 COMMUNITY NUMBER PANEL SUFFIX
 EAST HAMPTON, TOWN OF 090064 0155 G

Map Number shown below should be used when obtaining flood insurance. The Community Number shown above should be used on insurance applications for the subject community.

MAP NUMBER
 09007C0155G
EFFECTIVE DATE
 AUGUST 28, 2008

Federal Emergency Management Agency

SUBJECT PARCELS

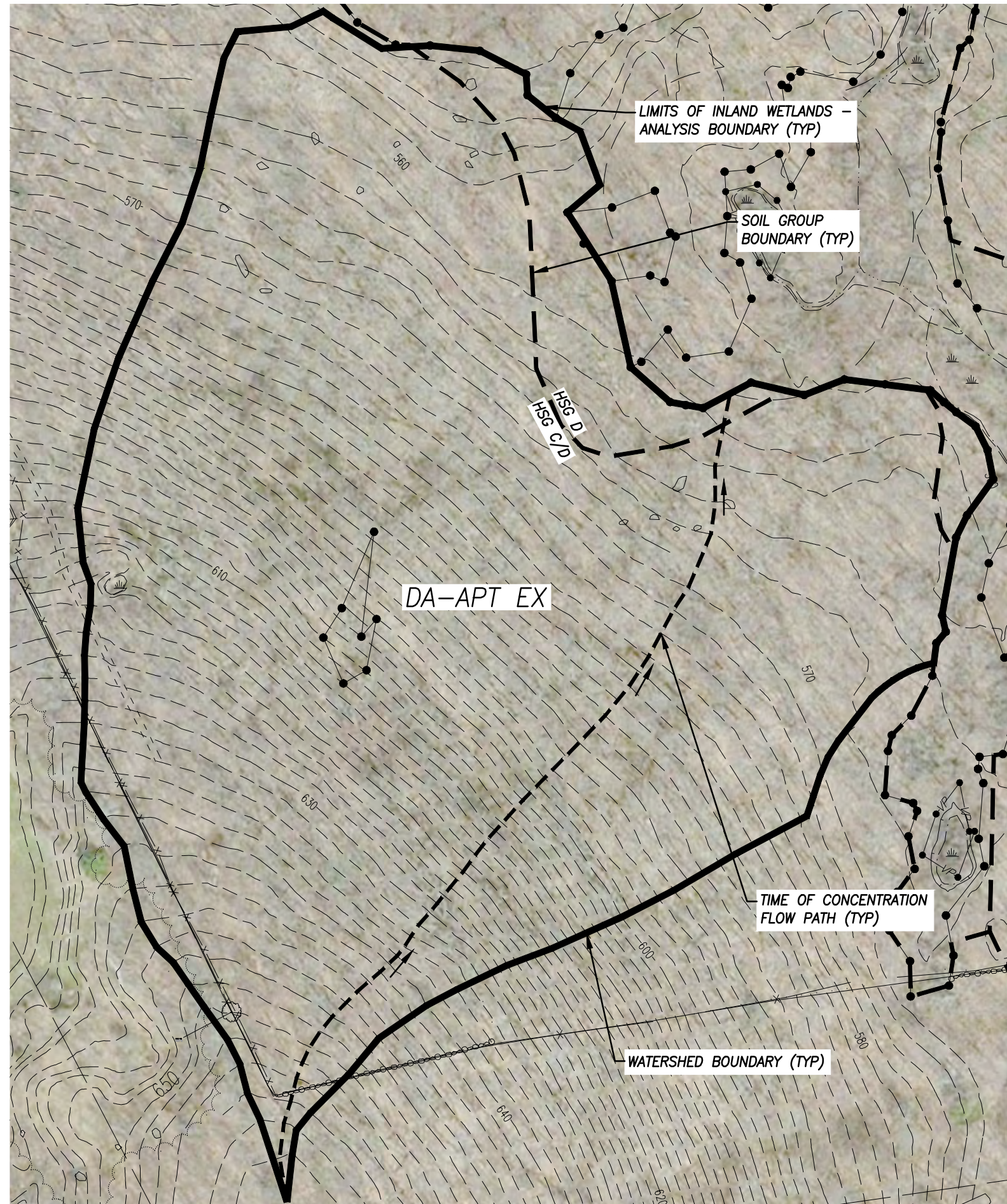
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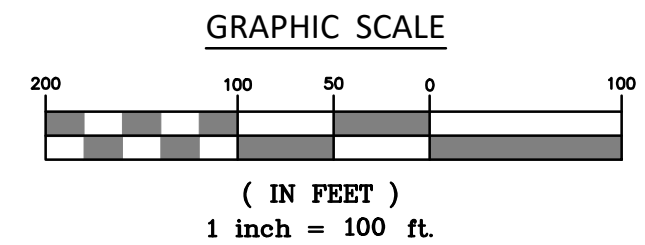


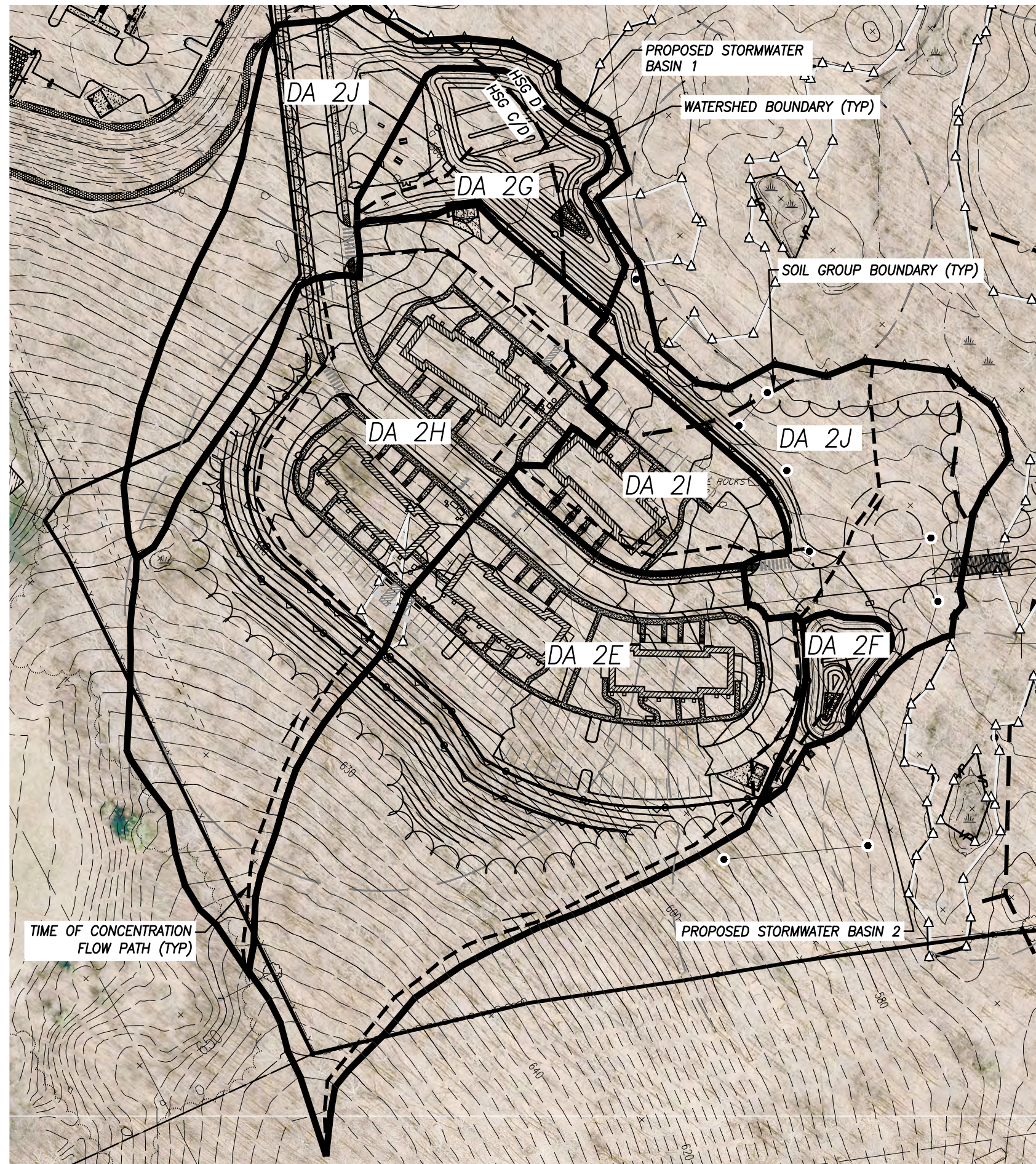
FEMA Flood Insurance Rate Map
 Map 090064 Panel 155 G
Salt Pond Apartments
 East High Street, East Hampton, CT

SCALE: 1"=2,000'
DATE: December 2020
JOB NO. 20-2853
FIGURE 2



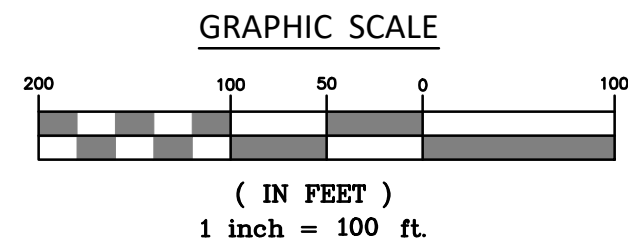
Pre-Development Conditions			
Watershed	Area (acres)	CN Value	Description
DA-APT EX	9.299	70	Wooded undeveloped land





Post-Development Conditions

Watershed	Area (acres)	CN Value	Description
DA-2E	3.023	83	Proposed apartments, roadway, parking (south) and grassed slope
DA-2F	0.152	86	Grassed slope and direct runoff to Stormwater Basin 2
DA-2G	0.554	84	Dog park and grassed slope and direct Runoff to Stormwater Basin 1
DA-2H	2.748	84	Proposed apartments, roadway, parking and grassed slope
DA-2I	0.536	92	Proposed apartments and parking (north)
DA-2J	2.286	80	Downgradient cleared areas and portions of Edgewater Circle
TOTAL	9.299	83	Apartments project area



Appendix A

NRCS Web Soil Survey Soils Report

Custom Soil Resource Report
Map—Hydrologic Soil Group



Soil Map may not be valid at this scale.


Map Scale: 1:4,190 if printed on A portrait (8.5" x 11") sheet.

0 50 100 200 300 Meters

0 200 400 800 1200 Feet









Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 18N WGS84

MAP LEGEND









Area of Interest (AOI)
 Area of Interest (AOI)

Soils





Soil Rating Polygons

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available


Soil Rating Lines

-  A
-  A/D
-  B
-  B/D
-  C
-  C/D
-  D
-  Not rated or not available






Soil Rating Points

-  A
-  A/D
-  B
-  B/D


Water Features

-  Streams and Canals





Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

-  Aerial Photography

Soils

-  C
-  C/D
-  D
-  Not rated or not available

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut
 Survey Area Data: Version 15, Sep 28, 2016

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 28, 2011—Apr 18, 2011

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Table—Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — State of Connecticut (CT600)				
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
3	Ridgebury, Leicester, and Whitman soils, 0 to 8 percent slopes, extremely stony	D	7.2	13.7%
46C	Woodbridge fine sandy loam, 8 to 15 percent slopes, very stony	C/D	4.9	9.4%
62C	Canton and Charlton fine sandy loams, 3 to 15 percent slopes, extremely stony	B	0.2	0.3%
72C	Nipmuck-Brookfield complex, 3 to 15 percent slopes, very rocky	B	26.1	50.0%
85C	Paxton and Montauk fine sandy loams, 8 to 15 percent slopes, very stony	C	1.0	1.9%
86D	Paxton and Montauk fine sandy loams, 15 to 35 percent slopes, extremely stony	C	9.3	17.7%
284B	Paxton-Urban land complex, 3 to 8 percent slopes	C	3.3	6.3%
308	Udorthents, smoothed	C	0.3	0.6%
Totals for Area of Interest			52.2	100.0%

Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition

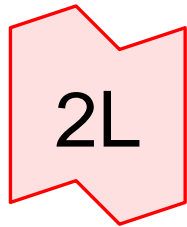
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

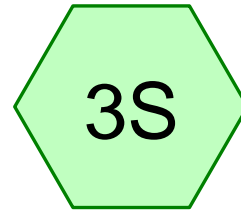
Appendix B

HydroCAD Modeling Results

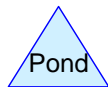
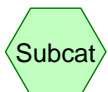
Pre-Development Conditions HydroCAD Results



Wetlands



DA-APTEX



Existing Apartments Only

Prepared by {enter your company name here}

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Page 2

Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type III 24-hr		Default	24.00	1	3.37	2
2	10-Year	Type III 24-hr		Default	24.00	1	5.18	2
3	25-Year	Type III 24-hr		Default	24.00	1	6.30	2
4	50-Year	Type III 24-hr		Default	24.00	1	7.14	2
5	100-Year	Type III 24-hr		Default	24.00	1	8.04	2

Existing Apartments Only

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Page 3

Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
8.687	70	Woods, Good, HSG C (3S)
0.612	77	Woods, Good, HSG D (3S)
9.299	70	TOTAL AREA

Existing Apartments Only

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Page 4

Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
8.687	HSG C	3S
0.612	HSG D	3S
0.000	Other	
9.299		TOTAL AREA

Existing Apartments Only

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	8.687	0.612	0.000	9.299	Woods, Good	3S
0.000	0.000	8.687	0.612	0.000	9.299	TOTAL	
						AREA	

Existing Apartments Only

Type III 24-hr 2-Year Rainfall=3.37"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 3S: DA-APTEX

Runoff Area=9.299 ac 0.00% Impervious Runoff Depth=0.93"
Flow Length=785' Tc=15.6 min CN=70 Runoff=6.77 cfs 0.720 af

Link 2L: Wetlands

Inflow=6.77 cfs 0.720 af
Primary=6.77 cfs 0.720 af

Total Runoff Area = 9.299 ac Runoff Volume = 0.720 af Average Runoff Depth = 0.93"
100.00% Pervious = 9.299 ac 0.00% Impervious = 0.000 ac

Existing Apartments Only

Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 3S: DA-APTEX

Runoff = 6.77 cfs @ 12.24 hrs, Volume= 0.720 af, Depth= 0.93"

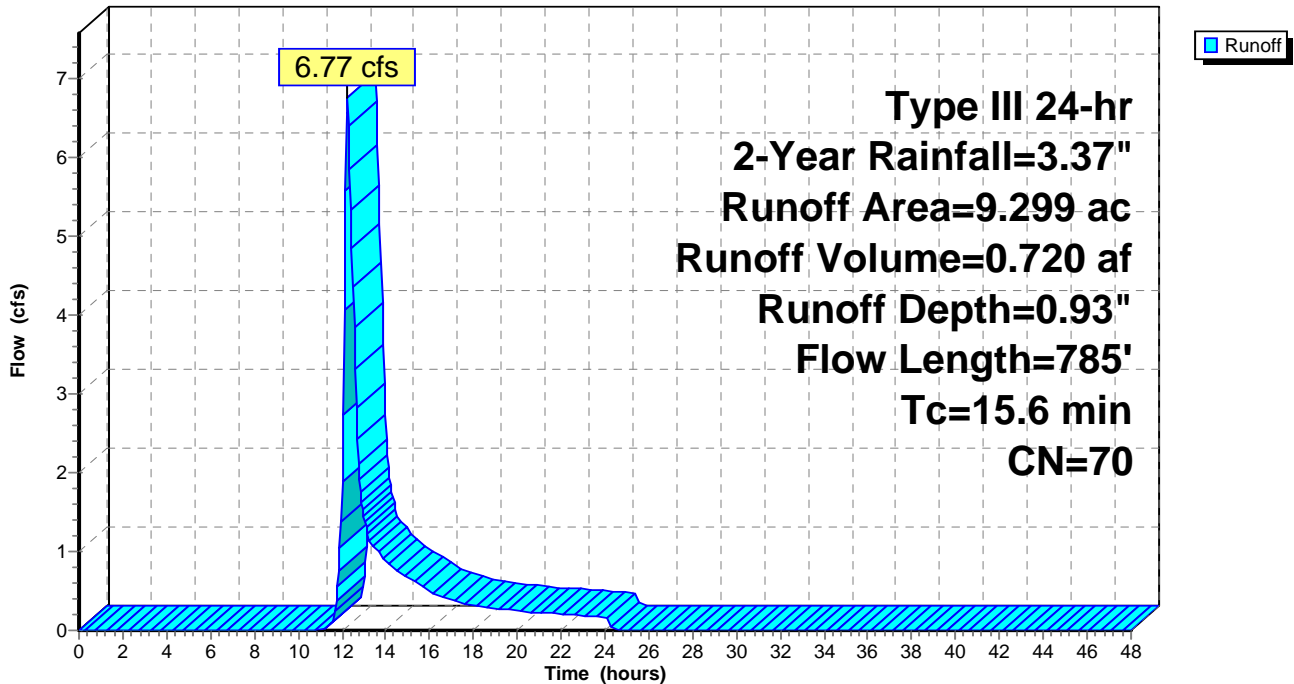
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
8.687	70	Woods, Good, HSG C
0.612	77	Woods, Good, HSG D
9.299	70	Weighted Average
9.299		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	50	0.0400	0.09		Sheet Flow, Grass Woods: Light underbrush n= 0.400 P2= 3.37"
6.5	735	0.1427	1.89		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
15.6	785	Total			

Subcatchment 3S: DA-APTEX

Hydrograph



Existing Apartments Only

Type III 24-hr 2-Year Rainfall=3.37"

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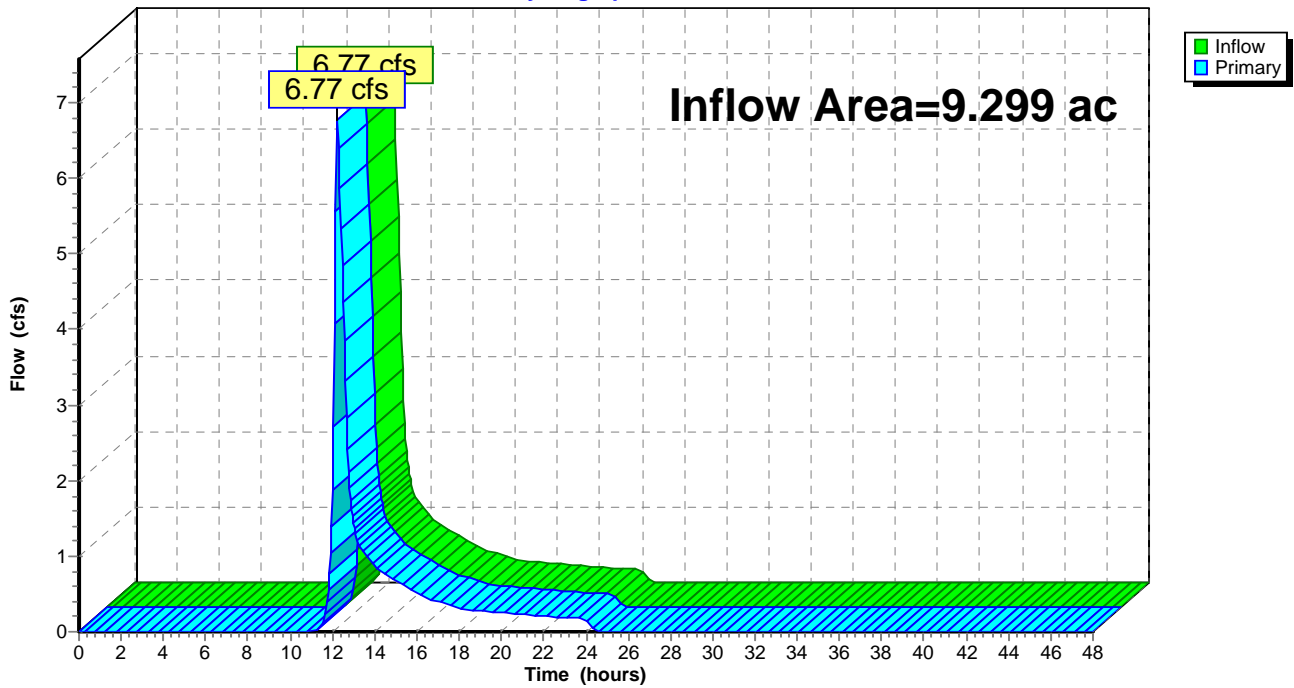
Summary for Link 2L: Wetlands

Inflow Area = 9.299 ac, 0.00% Impervious, Inflow Depth = 0.93" for 2-Year event
Inflow = 6.77 cfs @ 12.24 hrs, Volume= 0.720 af
Primary = 6.77 cfs @ 12.24 hrs, Volume= 0.720 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 2L: Wetlands

Hydrograph



Existing Apartments Only

Type III 24-hr 10-Year Rainfall=5.18"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 3S: DA-APTEX

Runoff Area=9.299 ac 0.00% Impervious Runoff Depth=2.17"
Flow Length=785' Tc=15.6 min CN=70 Runoff=17.25 cfs 1.682 af

Link 2L: Wetlands

Inflow=17.25 cfs 1.682 af
Primary=17.25 cfs 1.682 af

Total Runoff Area = 9.299 ac Runoff Volume = 1.682 af Average Runoff Depth = 2.17"
100.00% Pervious = 9.299 ac 0.00% Impervious = 0.000 ac

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Type III 24-hr 10-Year Rainfall=5.18"

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Summary for Subcatchment 3S: DA-APTEX

Runoff = 17.25 cfs @ 12.22 hrs, Volume= 1.682 af, Depth= 2.17"

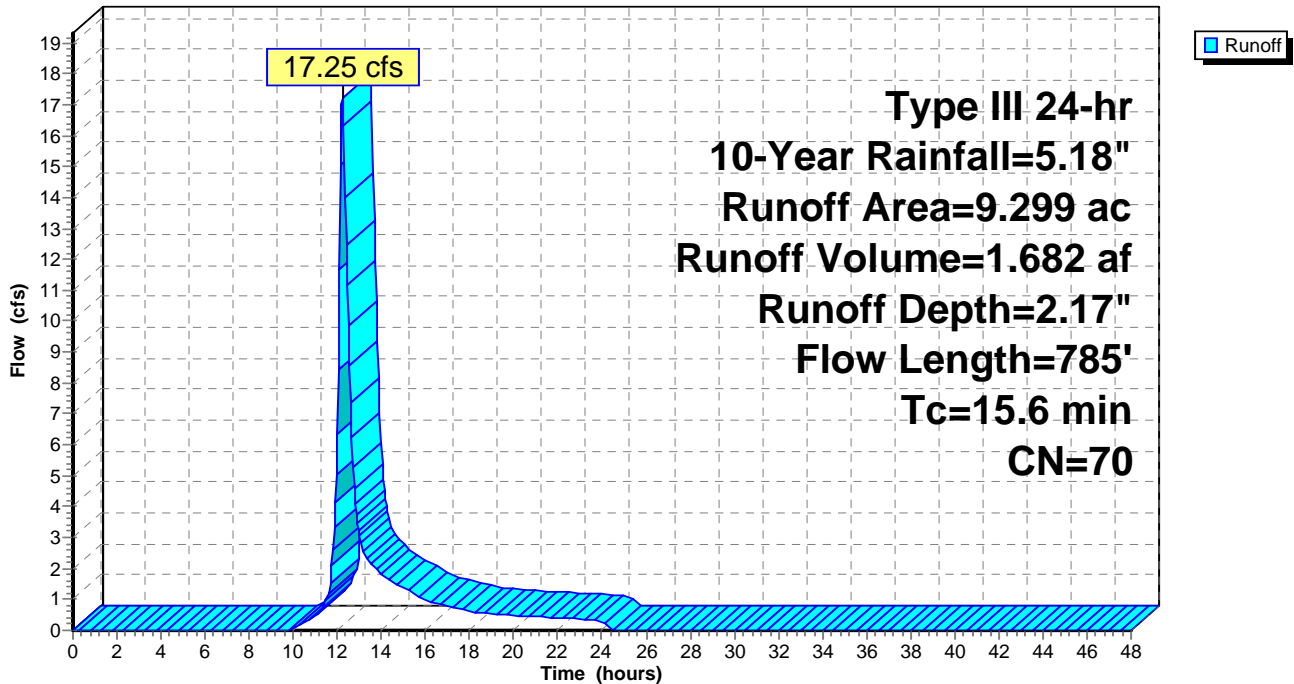
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
8.687	70	Woods, Good, HSG C
0.612	77	Woods, Good, HSG D
9.299	70	Weighted Average
9.299		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	50	0.0400	0.09		Sheet Flow, Grass Woods: Light underbrush n= 0.400 P2= 3.37"
6.5	735	0.1427	1.89		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
15.6	785	Total			

Subcatchment 3S: DA-APTEX

Hydrograph



Existing Apartments Only

Type III 24-hr 10-Year Rainfall=5.18"

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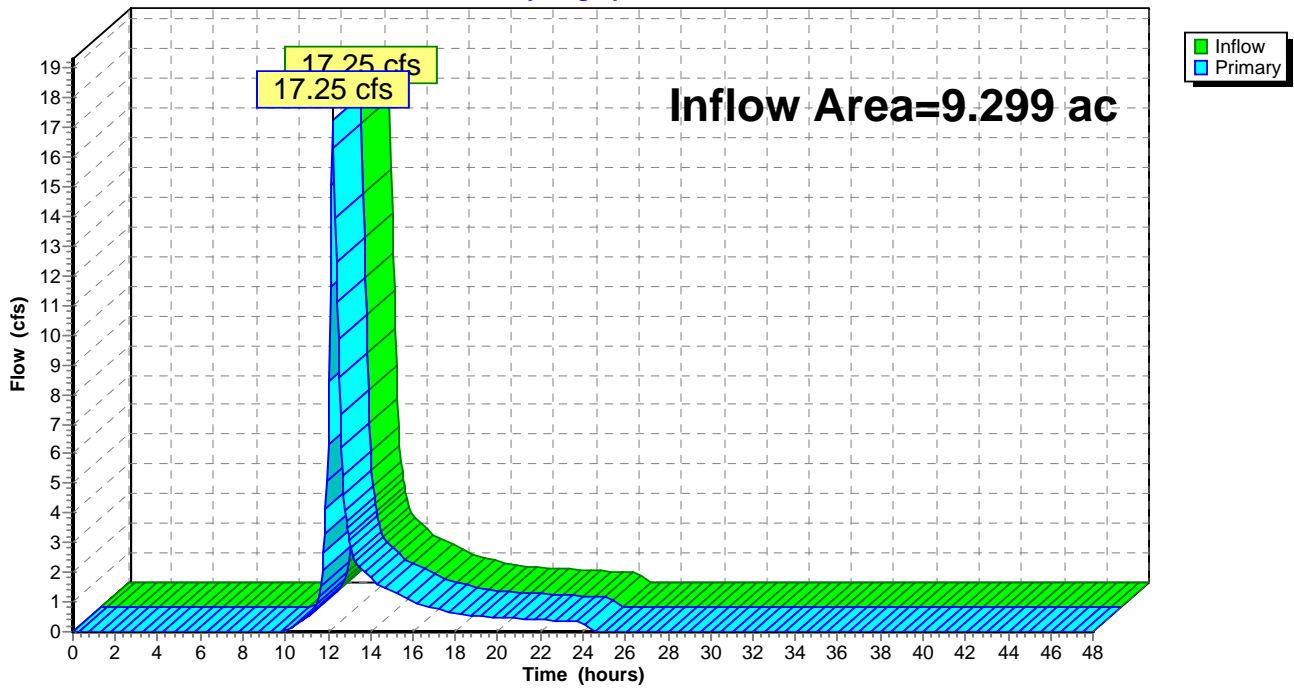
Summary for Link 2L: Wetlands

Inflow Area = 9.299 ac, 0.00% Impervious, Inflow Depth = 2.17" for 10-Year event
Inflow = 17.25 cfs @ 12.22 hrs, Volume= 1.682 af
Primary = 17.25 cfs @ 12.22 hrs, Volume= 1.682 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 2L: Wetlands

Hydrograph



Existing Apartments Only

Type III 24-hr 25-Year Rainfall=6.30"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 3S: DA-APTEX

Runoff Area=9.299 ac 0.00% Impervious Runoff Depth=3.05"
Flow Length=785' Tc=15.6 min CN=70 Runoff=24.52 cfs 2.360 af

Link 2L: Wetlands

Inflow=24.52 cfs 2.360 af
Primary=24.52 cfs 2.360 af

Total Runoff Area = 9.299 ac Runoff Volume = 2.360 af Average Runoff Depth = 3.05"
100.00% Pervious = 9.299 ac 0.00% Impervious = 0.000 ac

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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 3S: DA-APTEX

Runoff = 24.52 cfs @ 12.22 hrs, Volume= 2.360 af, Depth= 3.05"

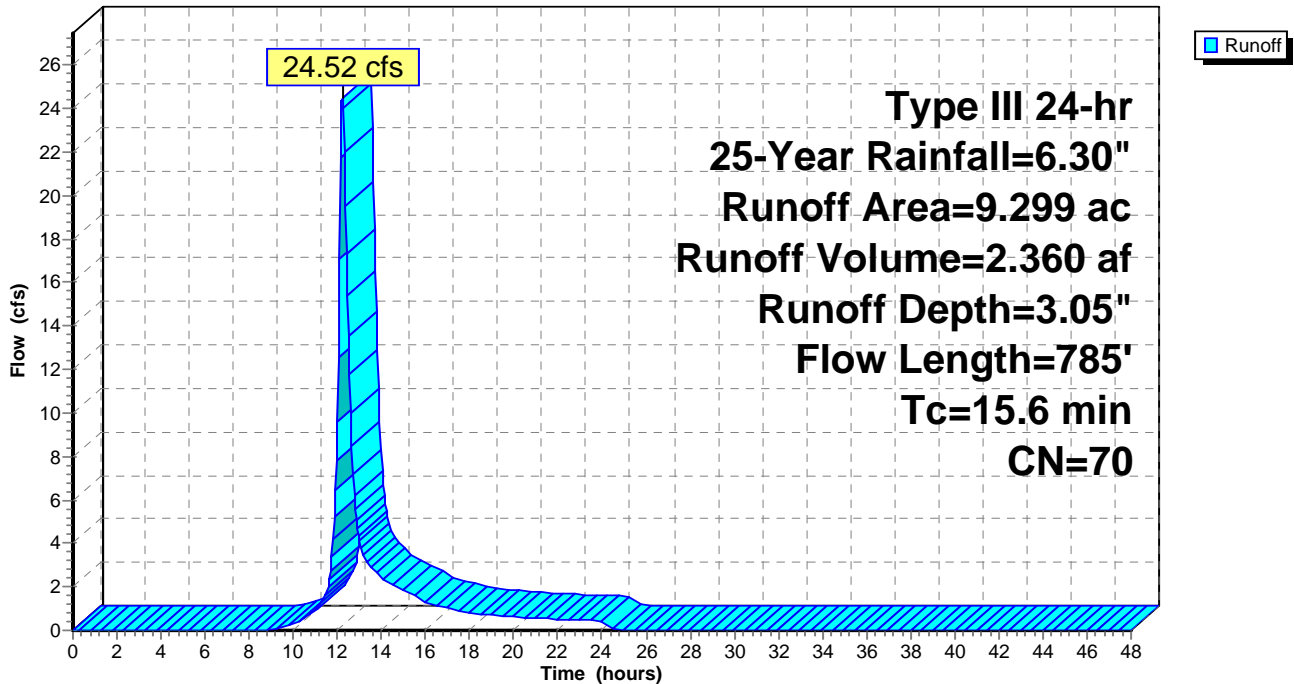
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
8.687	70	Woods, Good, HSG C
0.612	77	Woods, Good, HSG D
9.299	70	Weighted Average
9.299		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	50	0.0400	0.09		Sheet Flow, Grass Woods: Light underbrush n= 0.400 P2= 3.37"
6.5	735	0.1427	1.89		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
15.6	785	Total			

Subcatchment 3S: DA-APTEX

Hydrograph



Existing Apartments Only

Type III 24-hr 25-Year Rainfall=6.30"

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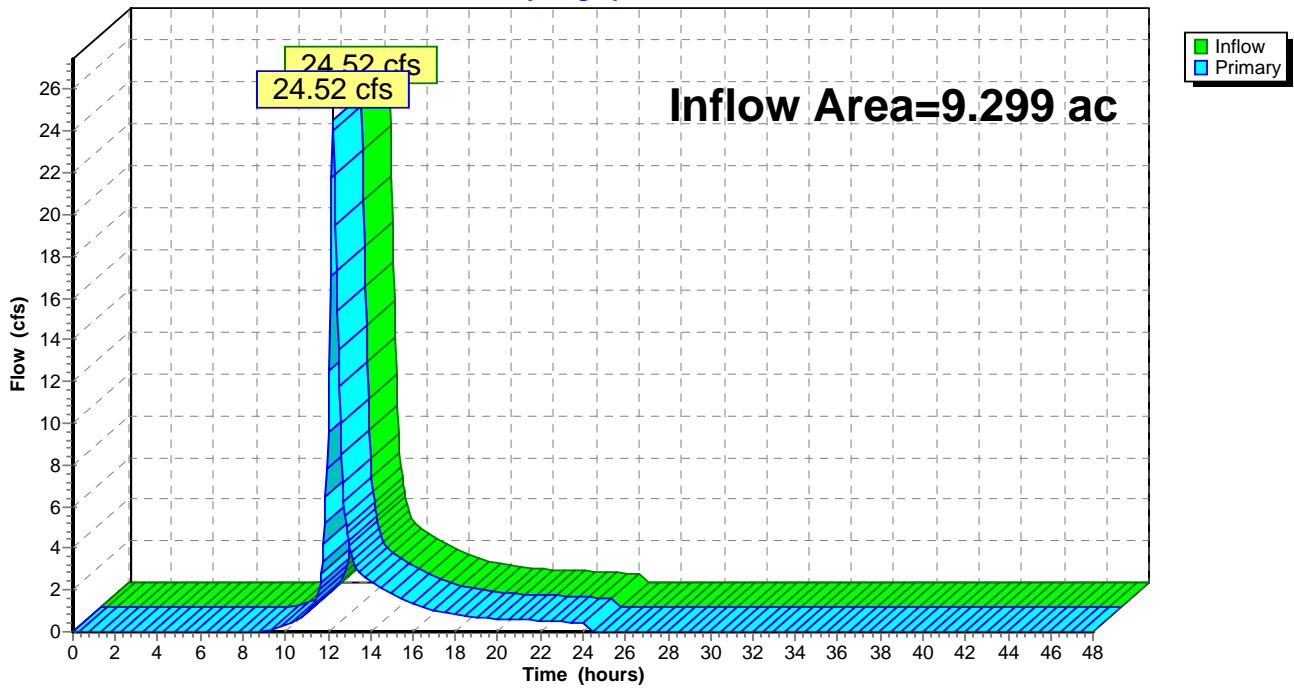
Summary for Link 2L: Wetlands

Inflow Area = 9.299 ac, 0.00% Impervious, Inflow Depth = 3.05" for 25-Year event
Inflow = 24.52 cfs @ 12.22 hrs, Volume= 2.360 af
Primary = 24.52 cfs @ 12.22 hrs, Volume= 2.360 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 2L: Wetlands

Hydrograph



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Type III 24-hr 50-Year Rainfall=7.14"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 3S: DA-APTEX

Runoff Area=9.299 ac 0.00% Impervious Runoff Depth=3.74"
Flow Length=785' Tc=15.6 min CN=70 Runoff=30.21 cfs 2.894 af

Link 2L: Wetlands

Inflow=30.21 cfs 2.894 af
Primary=30.21 cfs 2.894 af

Total Runoff Area = 9.299 ac Runoff Volume = 2.894 af Average Runoff Depth = 3.74"
100.00% Pervious = 9.299 ac 0.00% Impervious = 0.000 ac

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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Subcatchment 3S: DA-APTEX

Runoff = 30.21 cfs @ 12.22 hrs, Volume= 2.894 af, Depth= 3.74"

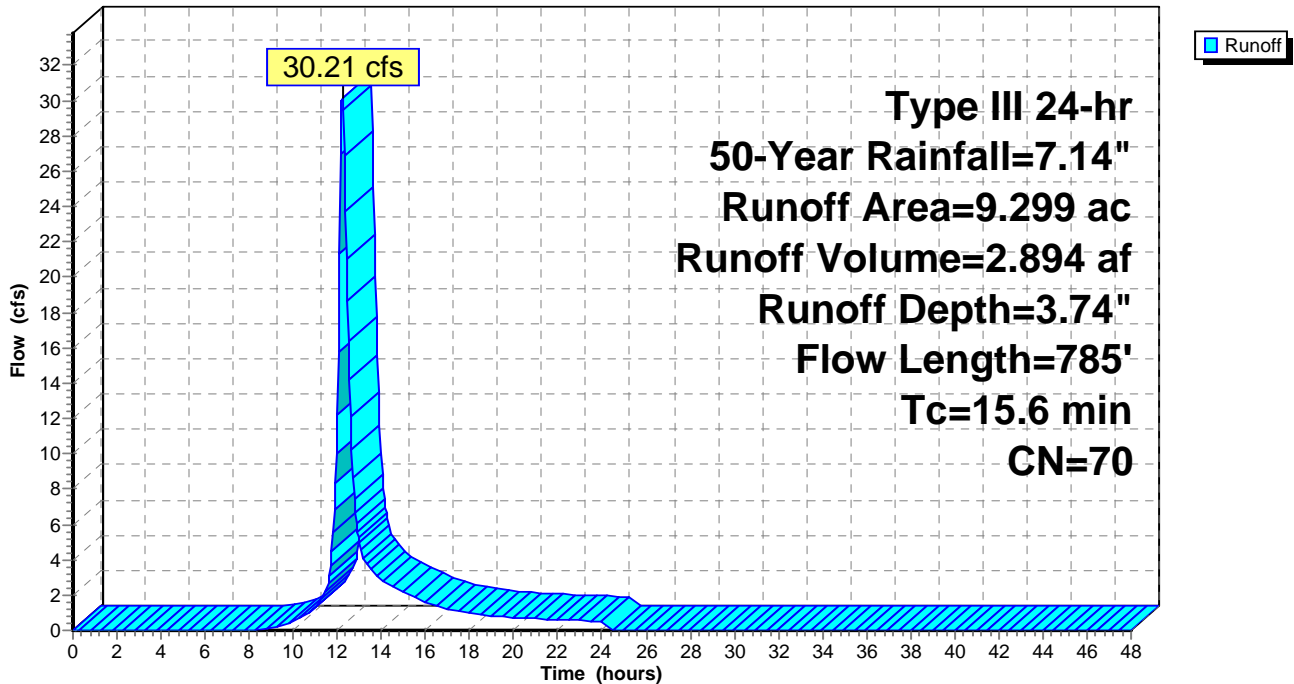
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
8.687	70	Woods, Good, HSG C
0.612	77	Woods, Good, HSG D
9.299	70	Weighted Average
9.299		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	50	0.0400	0.09		Sheet Flow, Grass Woods: Light underbrush n= 0.400 P2= 3.37"
6.5	735	0.1427	1.89		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
15.6	785	Total			

Subcatchment 3S: DA-APTEX

Hydrograph



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Type III 24-hr 50-Year Rainfall=7.14"

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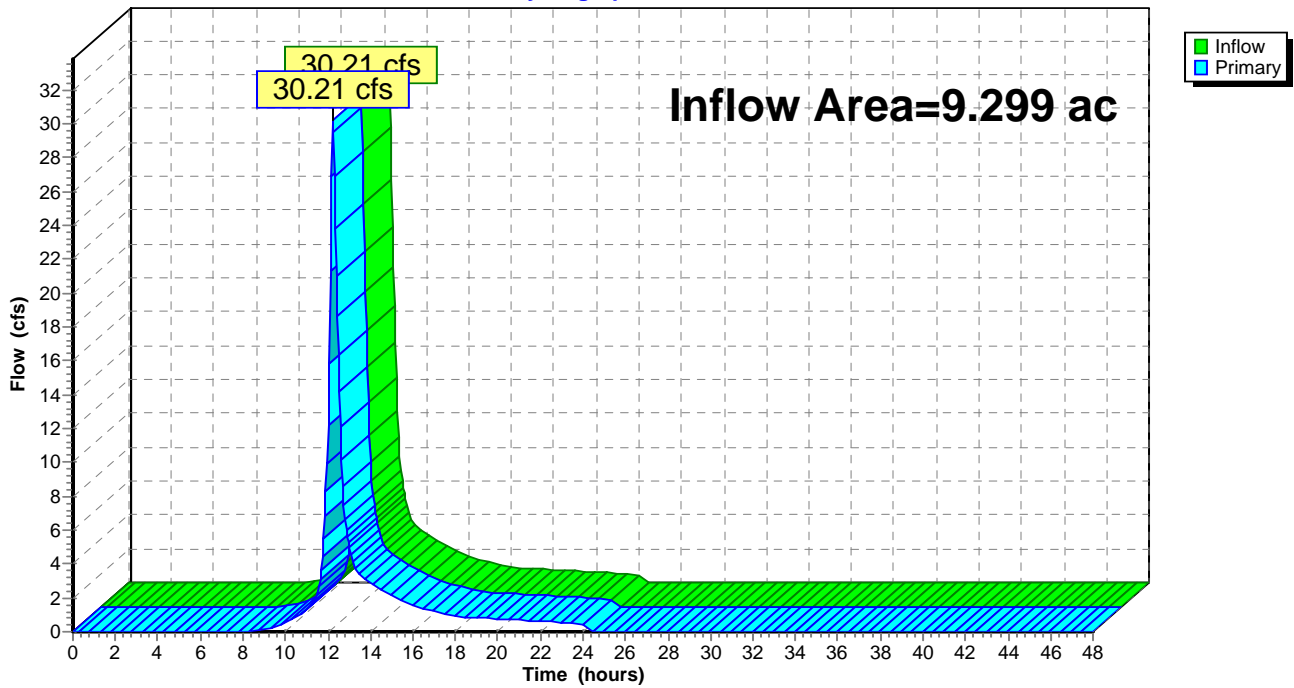
Summary for Link 2L: Wetlands

Inflow Area = 9.299 ac, 0.00% Impervious, Inflow Depth = 3.74" for 50-Year event
Inflow = 30.21 cfs @ 12.22 hrs, Volume= 2.894 af
Primary = 30.21 cfs @ 12.22 hrs, Volume= 2.894 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

Link 2L: Wetlands

Hydrograph



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Type III 24-hr 100-Year Rainfall=8.04"

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Time span=0.00-48.00 hrs, dt=0.05 hrs, 961 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 3S: DA-APTEX

Runoff Area=9.299 ac 0.00% Impervious Runoff Depth=4.50"
Flow Length=785' Tc=15.6 min CN=70 Runoff=36.44 cfs 3.486 af

Link 2L: Wetlands

Inflow=36.44 cfs 3.486 af
Primary=36.44 cfs 3.486 af

Total Runoff Area = 9.299 ac Runoff Volume = 3.486 af Average Runoff Depth = 4.50"
100.00% Pervious = 9.299 ac 0.00% Impervious = 0.000 ac

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Type III 24-hr 100-Year Rainfall=8.04"

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Summary for Subcatchment 3S: DA-APTEX

Runoff = 36.44 cfs @ 12.22 hrs, Volume= 3.486 af, Depth= 4.50"

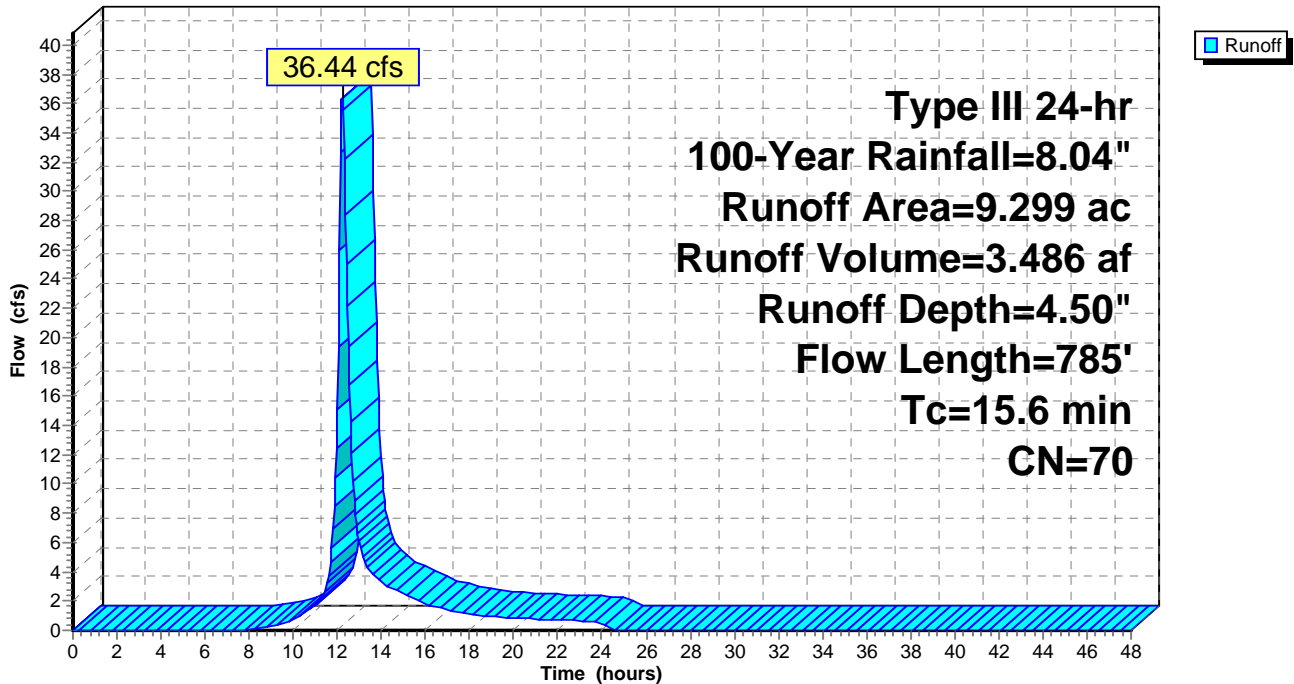
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
8.687	70	Woods, Good, HSG C
0.612	77	Woods, Good, HSG D
9.299	70	Weighted Average
9.299		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.1	50	0.0400	0.09		Sheet Flow, Grass Woods: Light underbrush n= 0.400 P2= 3.37"
6.5	735	0.1427	1.89		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
15.6	785	Total			

Subcatchment 3S: DA-APTEX

Hydrograph



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Type III 24-hr 100-Year Rainfall=8.04"

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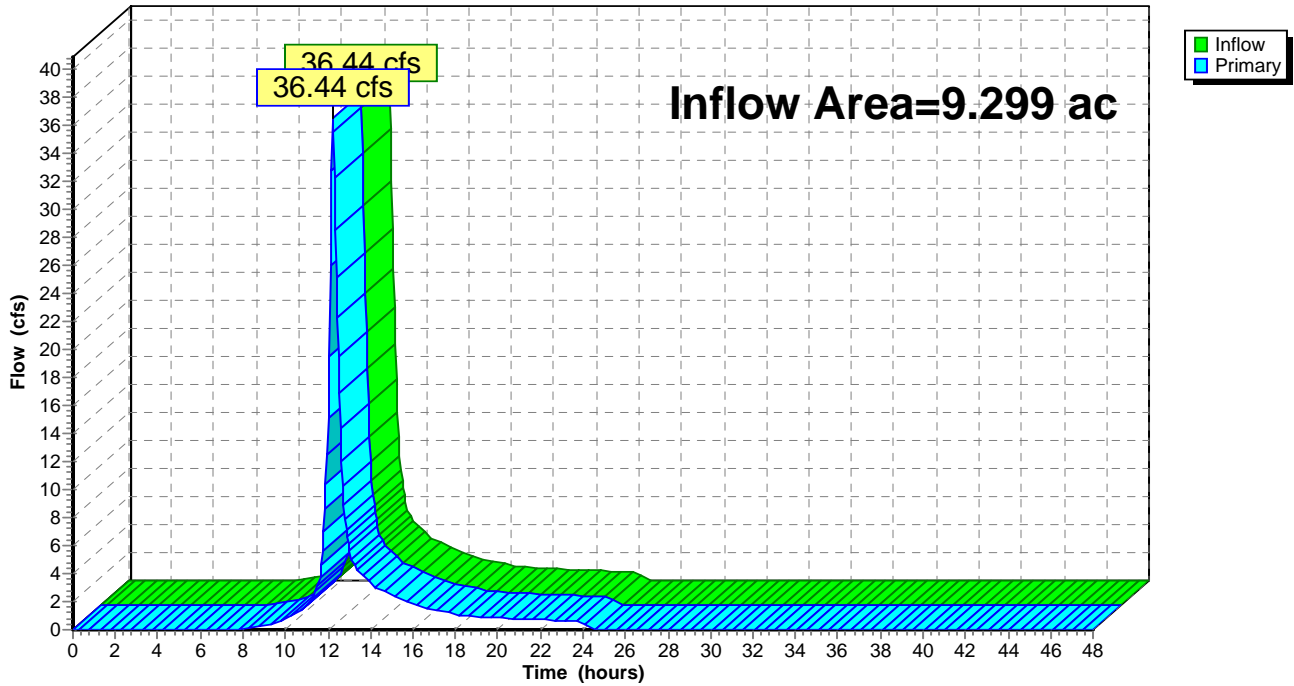
Summary for Link 2L: Wetlands

Inflow Area = 9.299 ac, 0.00% Impervious, Inflow Depth = 4.50" for 100-Year event
Inflow = 36.44 cfs @ 12.22 hrs, Volume= 3.486 af
Primary = 36.44 cfs @ 12.22 hrs, Volume= 3.486 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.05 hrs

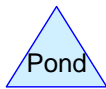
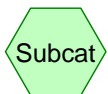
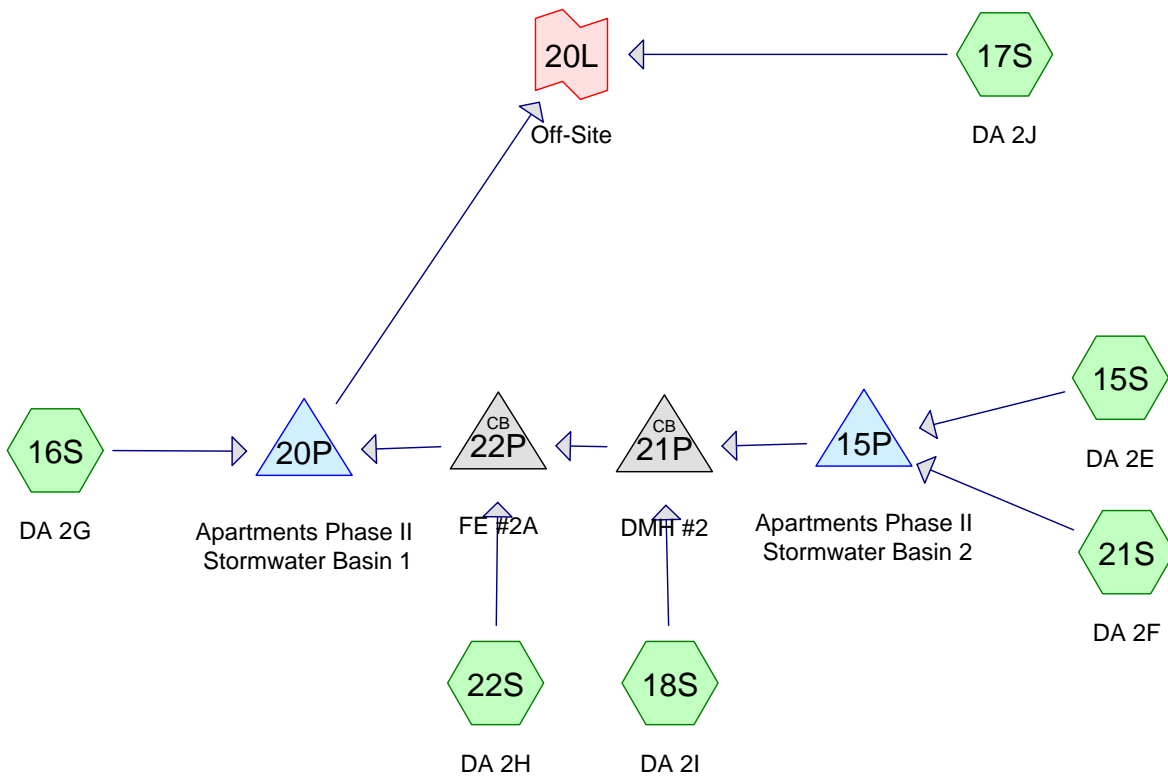
Link 2L: Wetlands

Hydrograph



Post-Development Conditions

HydroCAD Results



Routing Diagram for Proposed - Apartments Only
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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type III 24-hr		Default	24.00	1	3.37	2
2	10-Year	Type III 24-hr		Default	24.00	1	5.18	2
3	25-Year	Type III 24-hr		Default	24.00	1	6.30	2
4	50-Year	Type III 24-hr		Default	24.00	1	7.14	2
5	100-Year	Type III 24-hr		Default	24.00	1	8.04	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.782	74	>75% Grass cover, Good, HSG C (17S)
3.254	80	>75% Grass cover, Good, HSG D (15S, 16S, 17S, 18S, 21S, 22S)
0.010	80	>75% Grass cover, Good, HSG D, North (22S)
0.384	98	Paved parking, HSG C (17S)
0.775	98	Paved parking, HSG C, North (18S, 22S)
1.535	98	Paved parking, HSG C, South (15S, 22S)
0.184	98	Two single Family Houses and Paved Driveways (17S)
0.186	98	Water Surface, 0% imp, HSG C (16S, 21S)
2.189	70	Woods, Good, HSG C (15S, 17S, 22S)
9.299	83	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
0.000	HSG B	
5.851	HSG C	15S, 16S, 17S, 18S, 21S, 22S
3.264	HSG D	15S, 16S, 17S, 18S, 21S, 22S
0.184	Other	17S
9.299		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover
0.000	0.000	0.782	3.264	0.000	4.046	>75% Grass cover, Good
0.000	0.000	2.694	0.000	0.000	2.694	Paved parking
0.000	0.000	0.000	0.000	0.184	0.184	Two single Family Houses and Paved Driveways
0.000	0.000	0.186	0.000	0.000	0.186	Water Surface, 0% imp
0.000	0.000	2.189	0.000	0.000	2.189	Woods, Good
0.000	0.000	5.851	3.264	0.184	9.299	TOTAL AREA

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)
1	15P	566.00	564.27	68.0	0.0254	0.013	0.0	18.0	0.0
2	20P	554.00	552.00	102.0	0.0196	0.013	0.0	18.0	0.0
3	21P	563.77	559.50	260.0	0.0164	0.013	0.0	24.0	0.0
4	22P	556.50	555.00	60.0	0.0250	0.012	0.0	36.0	0.0

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Type III 24-hr 2-Year Rainfall=3.37"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 15S: DA 2E	Runoff Area=3.023 ac 32.58% Impervious Runoff Depth>1.75" Flow Length=671' Tc=12.0 min CN=83 Runoff=5.06 cfs 0.440 af
Subcatchment 16S: DA 2G	Runoff Area=0.554 ac 0.00% Impervious Runoff Depth>1.82" Flow Length=110' Tc=6.0 min CN=84 Runoff=1.16 cfs 0.084 af
Subcatchment 17S: DA 2J	Runoff Area=2.286 ac 24.85% Impervious Runoff Depth>1.53" Flow Length=240' Tc=6.0 min CN=80 Runoff=4.01 cfs 0.292 af
Subcatchment 18S: DA 2I	Runoff Area=0.536 ac 64.18% Impervious Runoff Depth>2.51" Flow Length=230' Slope=0.0200 '/' Tc=11.0 min CN=92 Runoff=1.30 cfs 0.112 af
Subcatchment 21S: DA 2F	Runoff Area=0.152 ac 0.00% Impervious Runoff Depth>1.98" Flow Length=107' Tc=6.0 min CN=86 Runoff=0.35 cfs 0.025 af
Subcatchment 22S: DA 2H	Runoff Area=2.748 ac 35.70% Impervious Runoff Depth>1.82" Flow Length=676' Tc=10.0 min CN=84 Runoff=5.08 cfs 0.417 af
Pond 15P: Apartments Phase II Stormwater	Peak Elev=568.22' Storage=5,058 cf Inflow=5.31 cfs 0.465 af Outflow=4.00 cfs 0.458 af
Pond 20P: Apartments Phase II	Peak Elev=556.81' Storage=18,654 cf Inflow=10.02 cfs 1.072 af Outflow=4.75 cfs 1.039 af
Pond 21P: DMH #2	Peak Elev=564.72' Inflow=4.92 cfs 0.570 af 24.0" Round Culvert n=0.013 L=260.0' S=0.0164 '/' Outflow=4.92 cfs 0.570 af
Pond 22P: FE #2A	Peak Elev=557.65' Inflow=9.12 cfs 0.988 af 36.0" Round Culvert n=0.012 L=60.0' S=0.0250 '/' Outflow=9.12 cfs 0.988 af
Link 20L: Off-Site	Inflow=5.97 cfs 1.330 af Primary=5.97 cfs 1.330 af

Total Runoff Area = 9.299 ac Runoff Volume = 1.370 af Average Runoff Depth = 1.77"
69.05% Pervious = 6.421 ac 30.95% Impervious = 2.878 ac

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Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 15S: DA 2E

Runoff = 5.06 cfs @ 12.17 hrs, Volume= 0.440 af, Depth> 1.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
* 0.985	98	Paved parking, HSG C, South
0.455	80	>75% Grass cover, Good, HSG D
0.917	70	Woods, Good, HSG C
0.666	80	>75% Grass cover, Good, HSG D
3.023	83	Weighted Average
2.038		67.42% Pervious Area
0.985		32.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	50	0.0600	0.11		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
3.3	417	0.1799	2.12		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	40	0.1000	2.21		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
0.7	164	0.0421	4.17		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
12.0	671	Total			

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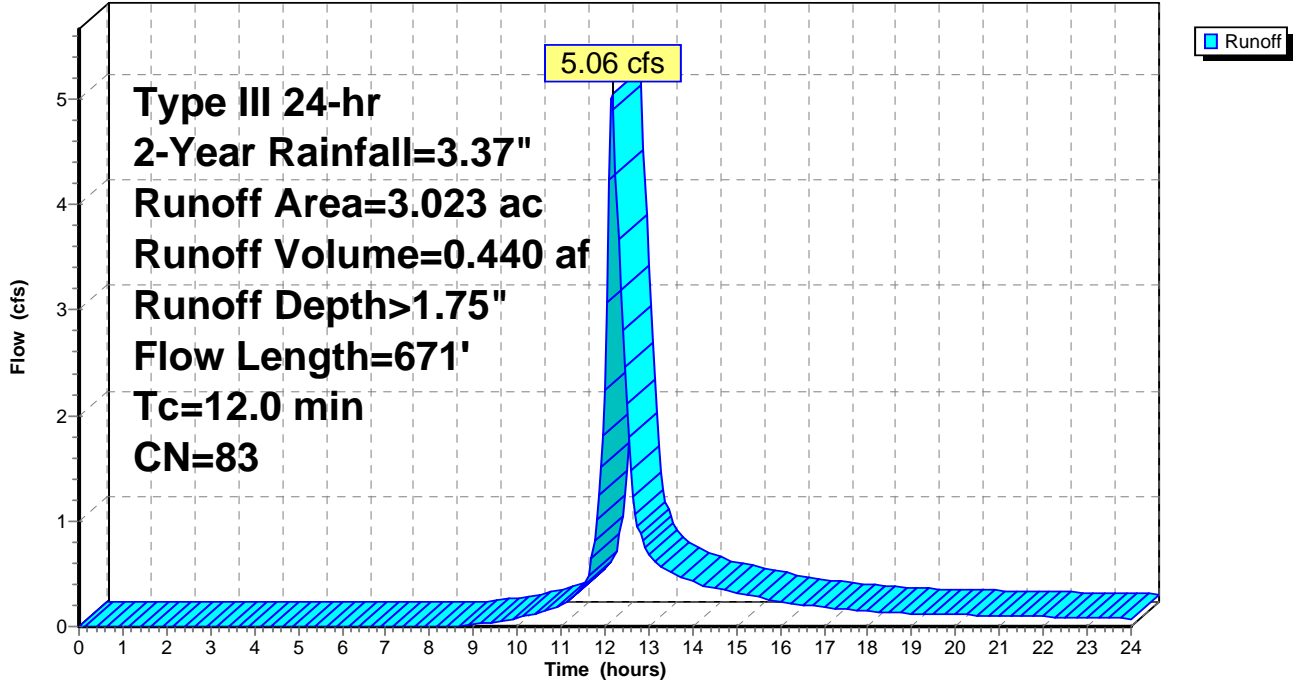
Type III 24-hr 2-Year Rainfall=3.37"

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Subcatchment 15S: DA 2E

Hydrograph



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Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 16S: DA 2G

Runoff = 1.16 cfs @ 12.09 hrs, Volume= 0.084 af, Depth> 1.82"

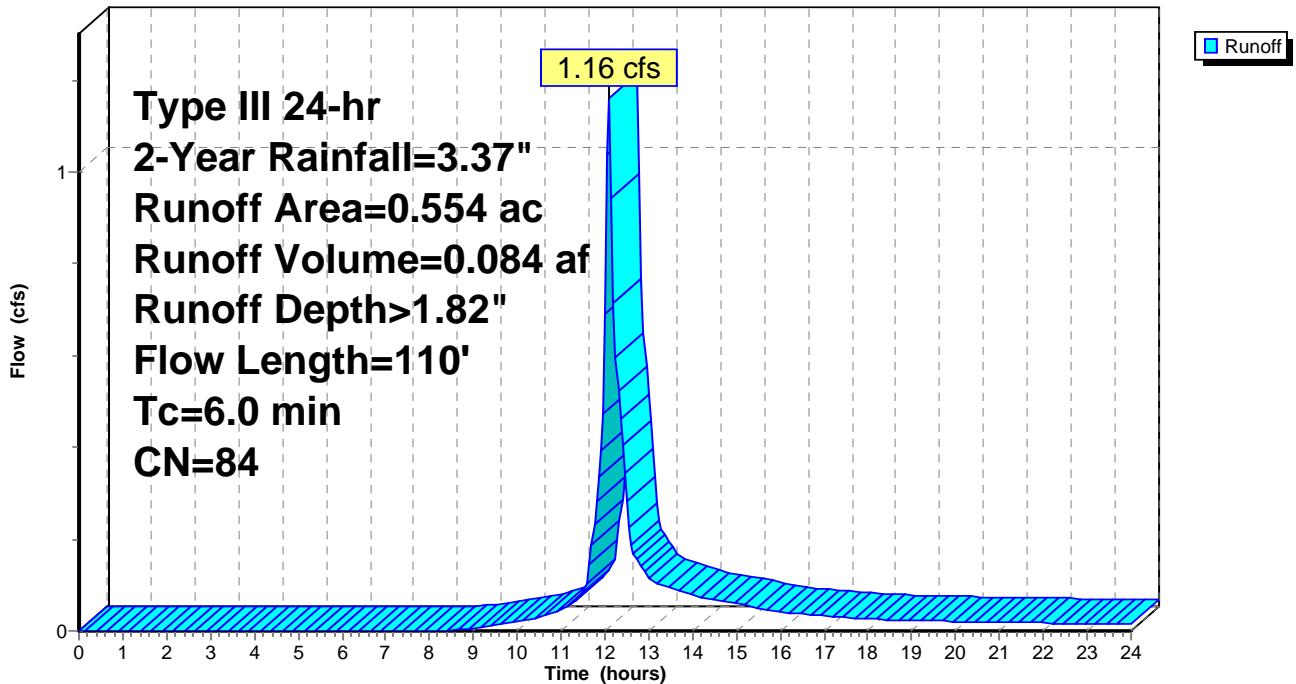
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
0.135	98	Water Surface, 0% imp, HSG C
0.017	80	>75% Grass cover, Good, HSG D
0.229	80	>75% Grass cover, Good, HSG D
0.157	80	>75% Grass cover, Good, HSG D
0.016	80	>75% Grass cover, Good, HSG D
0.554	84	Weighted Average
0.554		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.5	50	0.0500	0.15		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.2	60	0.3500	4.14		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
5.7	110	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 16S: DA 2G

Hydrograph



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Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 17S: DA 2J

Runoff = 4.01 cfs @ 12.10 hrs, Volume= 0.292 af, Depth> 1.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
0.412	80	>75% Grass cover, Good, HSG D
0.061	98	Paved parking, HSG C
0.032	74	>75% Grass cover, Good, HSG C
0.140	98	Paved parking, HSG C
0.721	74	>75% Grass cover, Good, HSG C
* 0.184	98	Two single Family Houses and Paved Driveways
0.183	98	Paved parking, HSG C
0.524	70	Woods, Good, HSG C
0.029	74	>75% Grass cover, Good, HSG C
2.286	80	Weighted Average
1.718		75.15% Pervious Area
0.568		24.85% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.3	24	0.1000	0.17		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	26	0.0500	1.56		Sheet Flow, Paved/Gravel Smooth surfaces n= 0.011 P2= 3.37"
0.3	85	0.0824	4.62		Shallow Concentrated Flow, Gravel Unpaved Kv= 16.1 fps
0.7	105	0.1333	2.56		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
3.6	240	Total, Increased to minimum Tc = 6.0 min			

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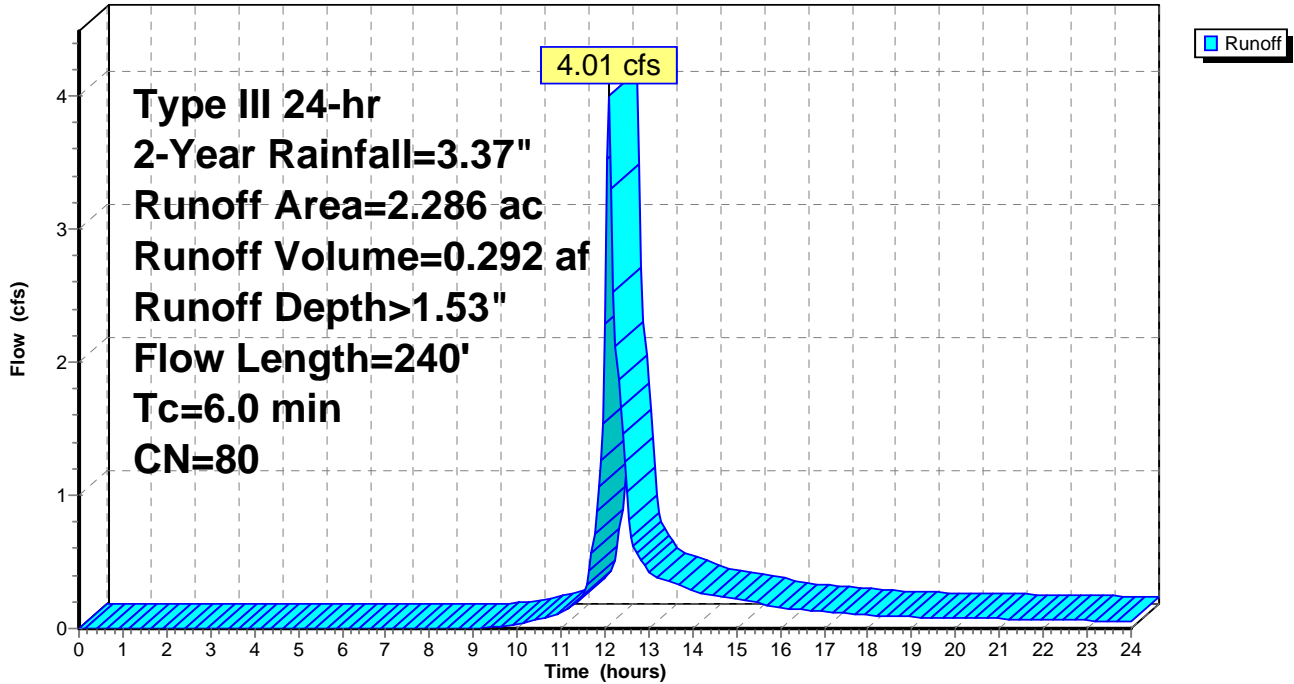
Type III 24-hr 2-Year Rainfall=3.37"

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Subcatchment 17S: DA 2J

Hydrograph



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Summary for Subcatchment 18S: DA 2I

Runoff = 1.30 cfs @ 12.15 hrs, Volume= 0.112 af, Depth> 2.51"

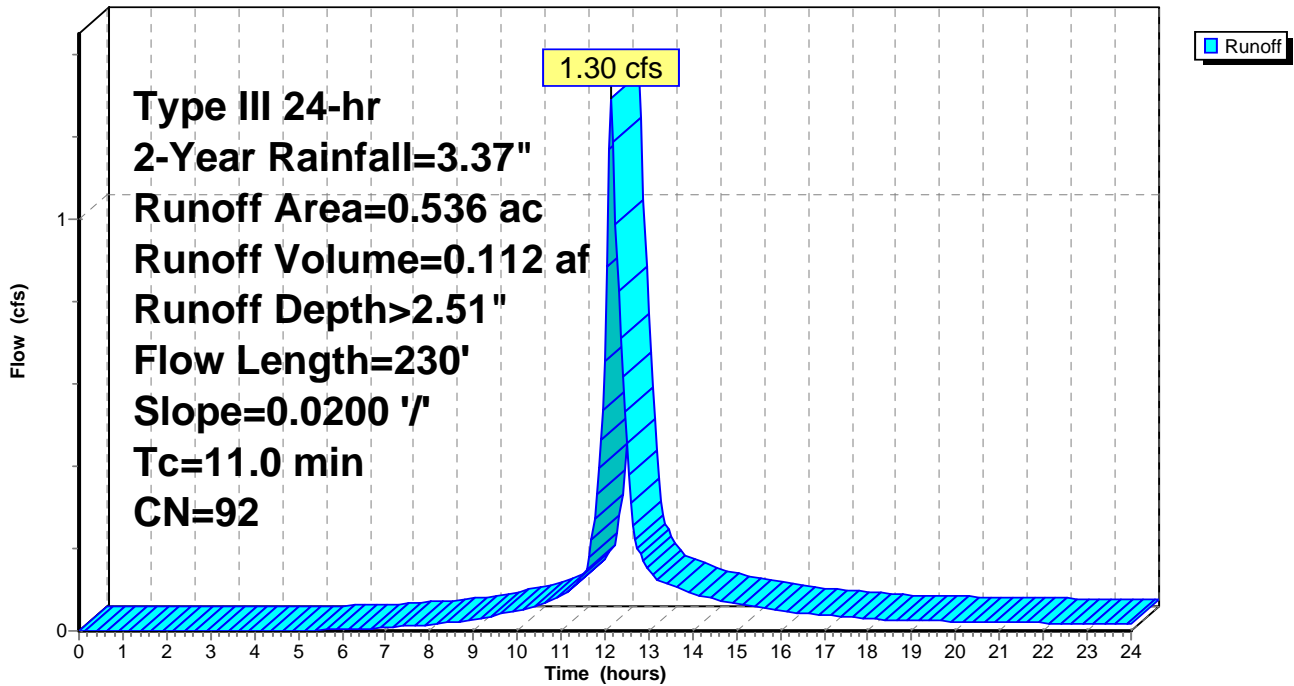
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
* 0.344	98	Paved parking, HSG C, North
0.192	80	>75% Grass cover, Good, HSG D
0.536	92	Weighted Average
0.192		35.82% Pervious Area
0.344		64.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0200	0.10		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
3.0	180	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
11.0	230	Total			

Subcatchment 18S: DA 2I

Hydrograph



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Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 21S: DA 2F

Runoff = 0.35 cfs @ 12.09 hrs, Volume= 0.025 af, Depth> 1.98"

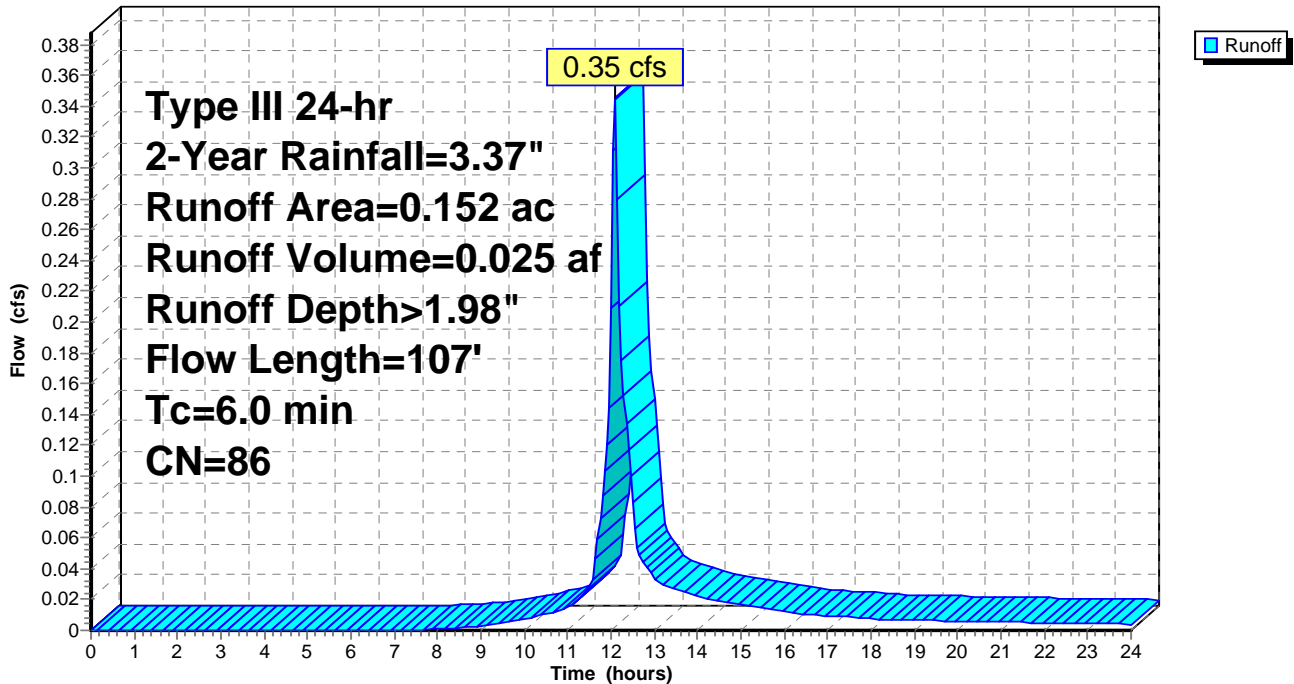
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
0.051	98	Water Surface, 0% imp, HSG C
0.101	80	>75% Grass cover, Good, HSG D
0.152	86	Weighted Average
0.152		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	50	0.1000	0.20		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	57	0.1754	2.93		Shallow Concentrated Flow, Woods Short Grass Pasture Kv= 7.0 fps
4.5	107	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 21S: DA 2F

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Type III 24-hr 2-Year Rainfall=3.37"

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Summary for Subcatchment 22S: DA 2H

Runoff = 5.08 cfs @ 12.14 hrs, Volume= 0.417 af, Depth> 1.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 2-Year Rainfall=3.37"

Area (ac)	CN	Description
* 0.431	98	Paved parking, HSG C, North
* 0.010	80	>75% Grass cover, Good, HSG D, North
0.313	80	>75% Grass cover, Good, HSG D
* 0.550	98	Paved parking, HSG C, South
0.360	80	>75% Grass cover, Good, HSG D
0.748	70	Woods, Good, HSG C
0.336	80	>75% Grass cover, Good, HSG D
2.748	84	Weighted Average
1.767		64.30% Pervious Area
0.981		35.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.3	50	0.1000	0.13		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
1.7	190	0.1316	1.81		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	81	0.3333	4.04		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
1.7	355	0.0310	3.57		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
10.0	676	Total			

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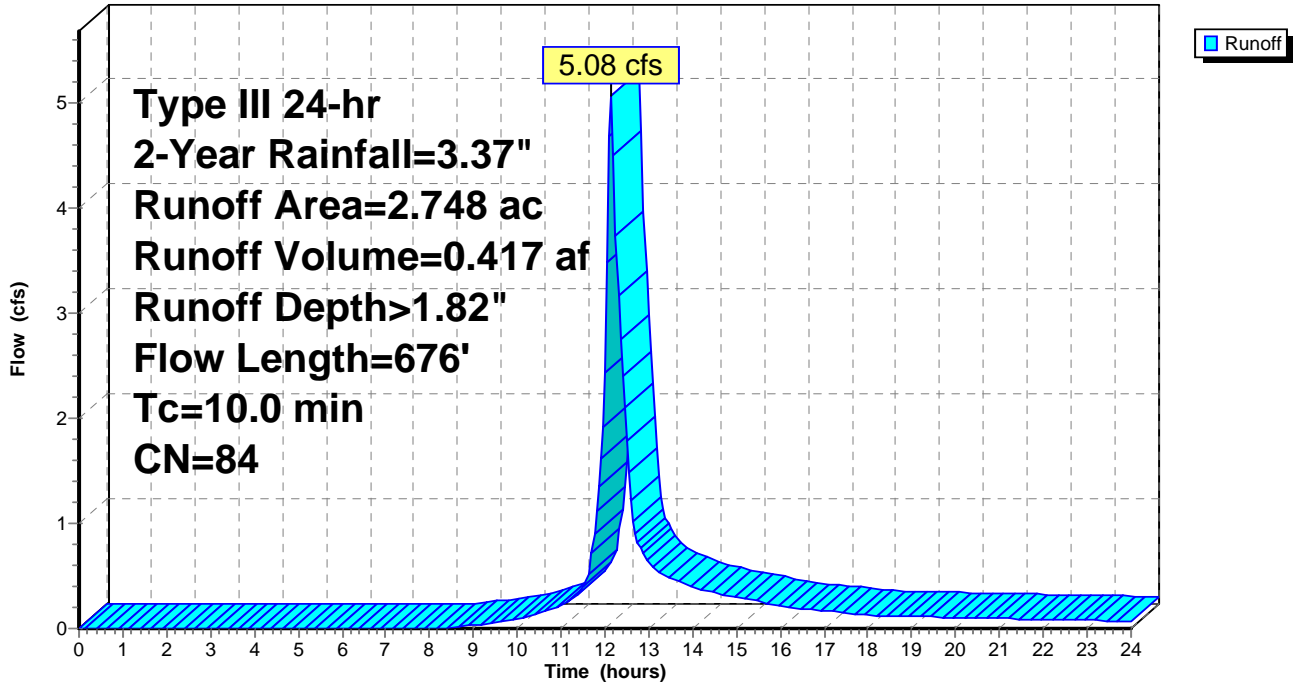
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Subcatchment 22S: DA 2H

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Summary for Pond 15P: Apartments Phase II Stormwater Basin 2

Inflow Area = 3.175 ac, 31.02% Impervious, Inflow Depth > 1.76" for 2-Year event
 Inflow = 5.31 cfs @ 12.17 hrs, Volume= 0.465 af
 Outflow = 4.00 cfs @ 12.29 hrs, Volume= 0.458 af, Atten= 25%, Lag= 7.6 min
 Primary = 4.00 cfs @ 12.29 hrs, Volume= 0.458 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 567.00' Surf.Area= 2,390 sf Storage= 1,777 cf
 Peak Elev= 568.22' @ 12.29 hrs Surf.Area= 2,982 sf Storage= 5,058 cf (3,281 cf above start)
 Flood Elev= 569.70' Surf.Area= 3,741 sf Storage= 10,022 cf (8,245 cf above start)

Plug-Flow detention time= 83.2 min calculated for 0.418 af (90% of inflow)
 Center-of-Mass det. time= 17.8 min (851.7 - 833.9)

Volume	Invert	Avail.Storage	Storage Description
#1	566.00'	11,168 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
566.00	1,164	0	0
567.00	2,390	1,777	1,777
568.00	2,867	2,629	4,406
570.00	3,895	6,762	11,168

Device	Routing	Invert	Outlet Devices
#1	Primary	566.00'	18.0" Round 18" HDPE L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 566.00' / 564.27' S= 0.0254 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	567.00'	6.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#3	Device 1	567.50'	12.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	568.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	569.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=3.99 cfs @ 12.29 hrs HW=568.22' TW=564.72' (Dynamic Tailwater)

- 1=18" HDPE (Passes 3.99 cfs of 10.32 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 1.86 cfs @ 4.74 fps)
- 3=Orifice/Grate (Orifice Controls 1.75 cfs @ 2.89 fps)
- 4=Orifice/Grate (Orifice Controls 0.37 cfs @ 1.60 fps)
- 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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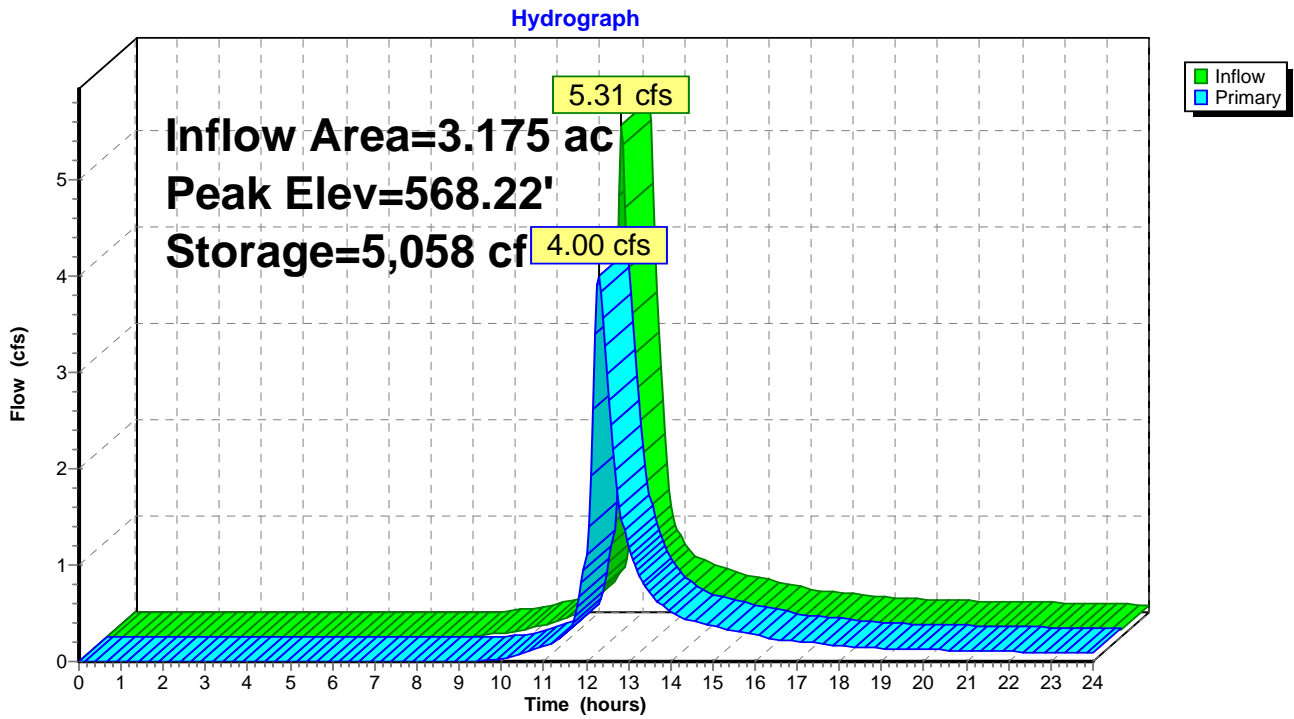
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Pond 15P: Apartments Phase II Stormwater Basin 2



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Summary for Pond 20P: Apartments Phase II Stormwater Basin 1

Inflow Area = 7.013 ac, 32.94% Impervious, Inflow Depth > 1.83" for 2-Year event
 Inflow = 10.02 cfs @ 12.17 hrs, Volume= 1.072 af
 Outflow = 4.75 cfs @ 12.56 hrs, Volume= 1.039 af, Atten= 53%, Lag= 23.2 min
 Primary = 4.75 cfs @ 12.56 hrs, Volume= 1.039 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 555.00' Surf.Area= 6,117 sf Storage= 5,401 cf
 Peak Elev= 556.81' @ 12.56 hrs Surf.Area= 8,345 sf Storage= 18,654 cf (13,252 cf above start)
 Flood Elev= 559.40' Surf.Area= 11,019 sf Storage= 43,681 cf (38,280 cf above start)

Plug-Flow detention time= 130.1 min calculated for 0.913 af (85% of inflow)
 Center-of-Mass det. time= 44.6 min (880.3 - 835.8)

Volume	Invert	Avail.Storage	Storage Description
#1	554.00'	50,485 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
554.00	4,686	0	0
556.00	7,547	12,233	12,233
558.00	9,522	17,069	29,302
560.00	11,661	21,183	50,485

Device	Routing	Invert	Outlet Devices
#1	Primary	554.00'	18.0" Round 18" HDPE L= 102.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 554.00' / 552.00' S= 0.0196 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	555.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	556.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	557.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	558.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=4.75 cfs @ 12.56 hrs HW=556.81' TW=0.00' (Dynamic Tailwater)

- 1=18" HDPE (Passes 4.75 cfs of 12.20 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 3.10 cfs @ 5.68 fps)
- 3=Orifice/Grate (Orifice Controls 1.65 cfs @ 3.06 fps)
- 4=Orifice/Grate (Controls 0.00 cfs)
- 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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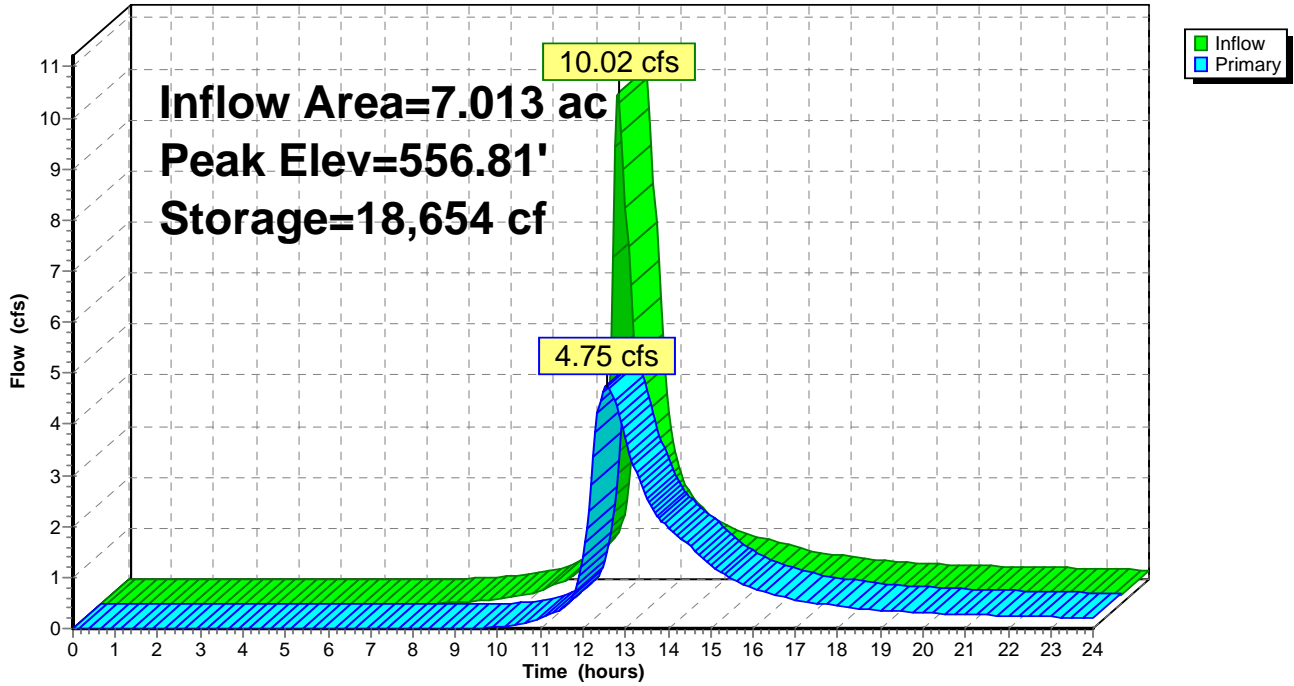
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Pond 20P: Apartments Phase II Stormwater Basin 1

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Summary for Pond 21P: DMH #2

Inflow Area = 3.711 ac, 35.81% Impervious, Inflow Depth > 1.84" for 2-Year event
Inflow = 4.92 cfs @ 12.27 hrs, Volume= 0.570 af
Outflow = 4.92 cfs @ 12.27 hrs, Volume= 0.570 af, Atten= 0%, Lag= 0.0 min
Primary = 4.92 cfs @ 12.27 hrs, Volume= 0.570 af

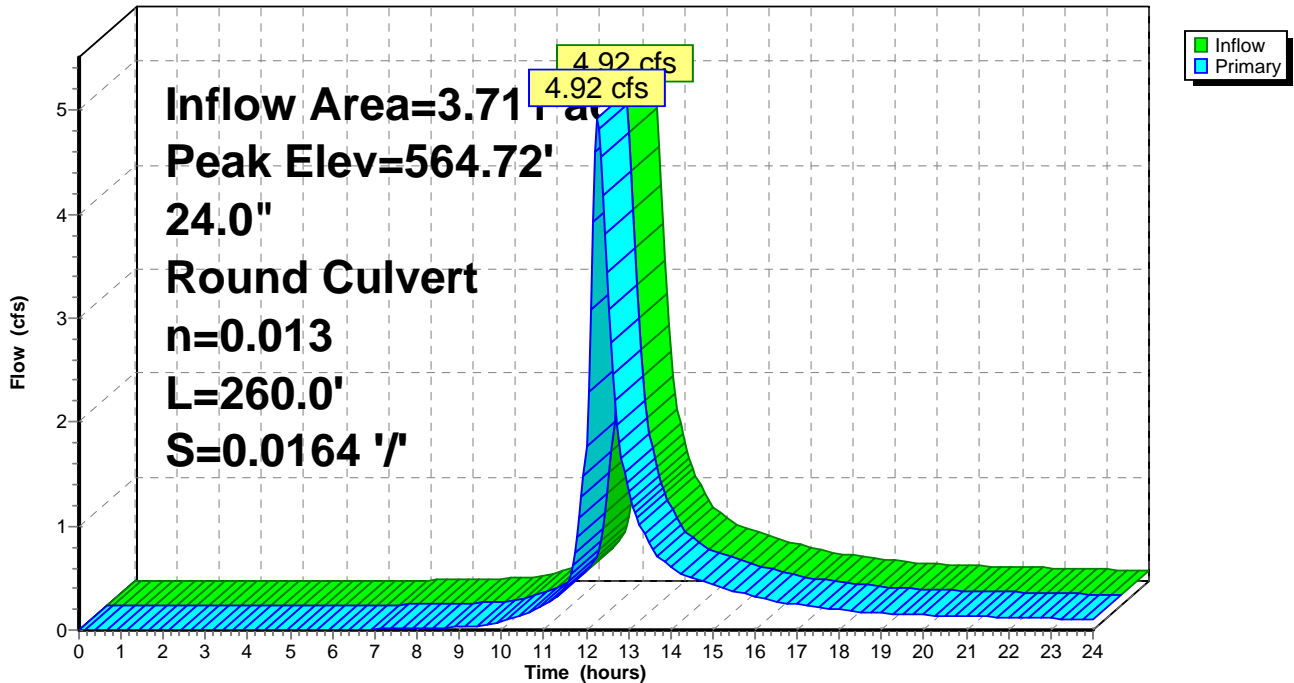
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 564.72' @ 12.27 hrs
Flood Elev= 569.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	563.77'	24.0" Round Culvert L= 260.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 563.77' / 559.50' S= 0.0164 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=4.88 cfs @ 12.27 hrs HW=564.72' TW=557.60' (Dynamic Tailwater)
↑**1=Culvert** (Inlet Controls 4.88 cfs @ 3.32 fps)

Pond 21P: DMH #2

Hydrograph



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Summary for Pond 22P: FE #2A

Inflow Area = 6.459 ac, 35.76% Impervious, Inflow Depth > 1.84" for 2-Year event
Inflow = 9.12 cfs @ 12.18 hrs, Volume= 0.988 af
Outflow = 9.12 cfs @ 12.18 hrs, Volume= 0.988 af, Atten= 0%, Lag= 0.0 min
Primary = 9.12 cfs @ 12.18 hrs, Volume= 0.988 af

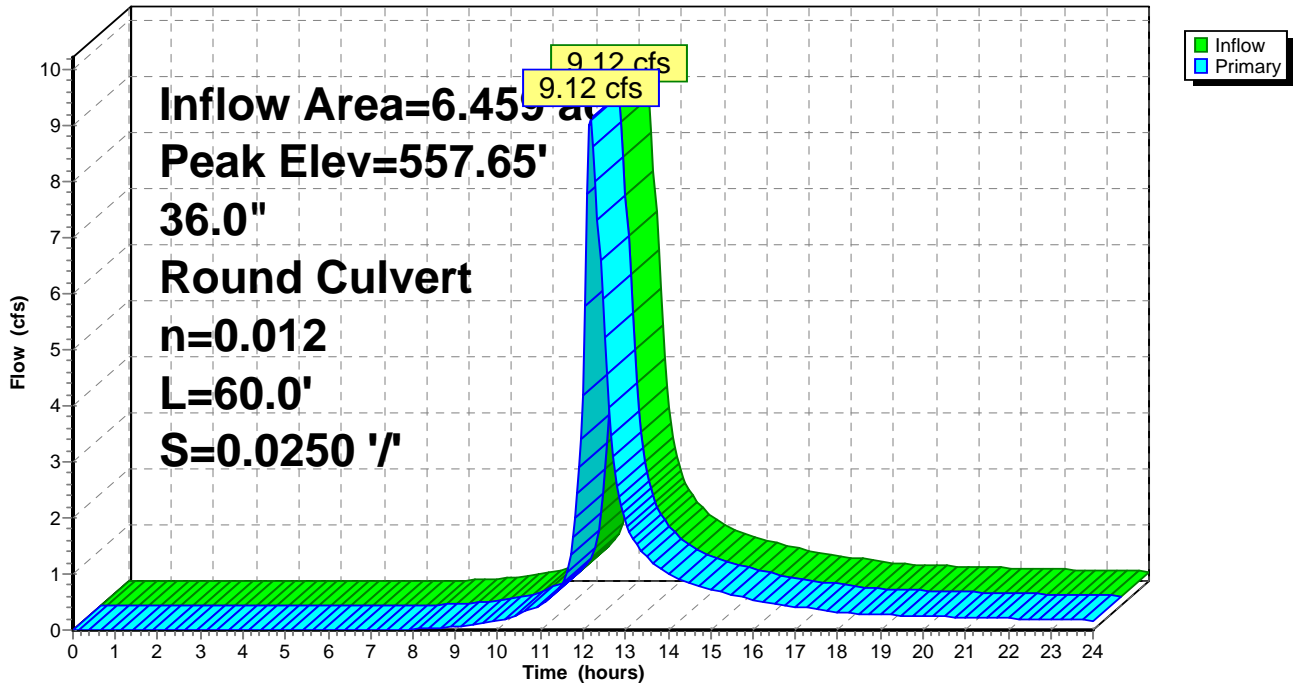
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 557.65' @ 12.18 hrs
Flood Elev= 564.47'

Device	Routing	Invert	Outlet Devices
#1	Primary	556.50'	36.0" Round Culvert L= 60.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 556.50' / 555.00' S= 0.0250 '/ Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 7.07 sf

Primary OutFlow Max=9.06 cfs @ 12.18 hrs HW=557.65' TW=556.25' (Dynamic Tailwater)
↑1=Culvert (Inlet Controls 9.06 cfs @ 3.65 fps)

Pond 22P: FE #2A

Hydrograph



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Type III 24-hr 2-Year Rainfall=3.37"

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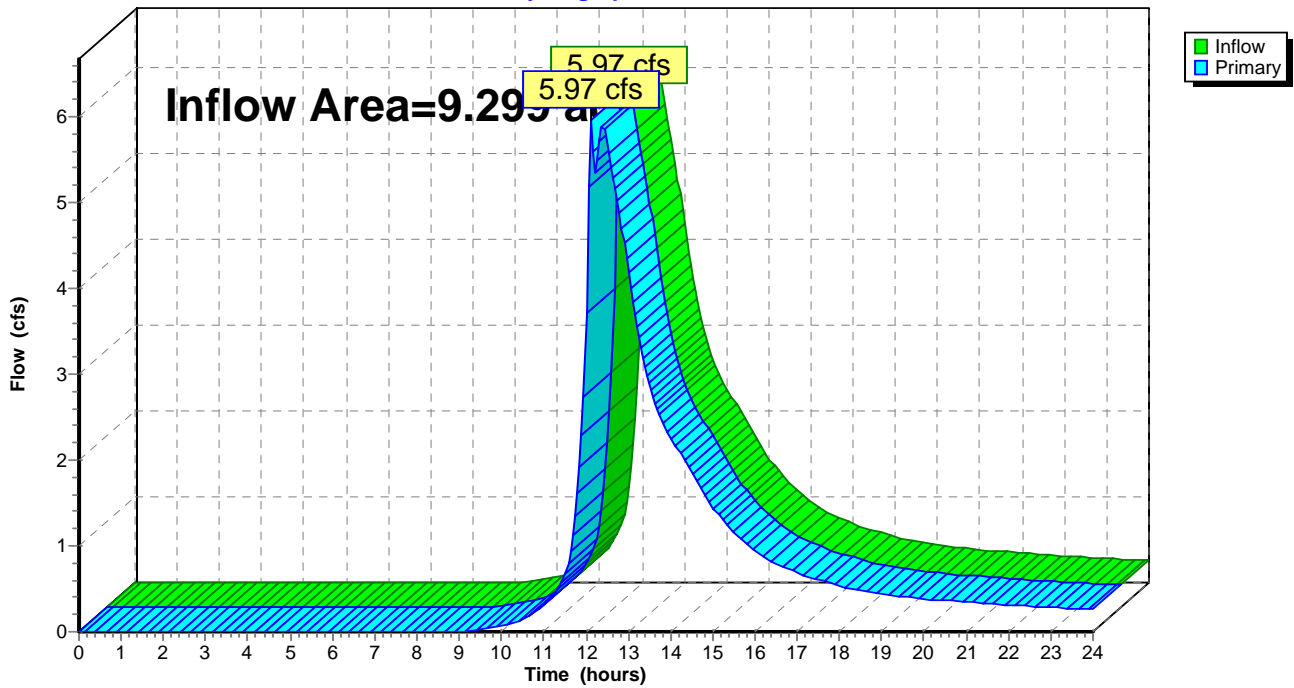
Summary for Link 20L: Off-Site

Inflow Area = 9.299 ac, 30.95% Impervious, Inflow Depth > 1.72" for 2-Year event
Inflow = 5.97 cfs @ 12.11 hrs, Volume= 1.330 af
Primary = 5.97 cfs @ 12.11 hrs, Volume= 1.330 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 20L: Off-Site

Hydrograph



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Type III 24-hr 10-Year Rainfall=5.18"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 15S: DA 2E Runoff Area=3.023 ac 32.58% Impervious Runoff Depth>3.33"
Flow Length=671' Tc=12.0 min CN=83 Runoff=9.62 cfs 0.839 af

Subcatchment 16S: DA 2G Runoff Area=0.554 ac 0.00% Impervious Runoff Depth>3.43"
Flow Length=110' Tc=6.0 min CN=84 Runoff=2.17 cfs 0.158 af

Subcatchment 17S: DA 2J Runoff Area=2.286 ac 24.85% Impervious Runoff Depth>3.05"
Flow Length=240' Tc=6.0 min CN=80 Runoff=8.00 cfs 0.581 af

Subcatchment 18S: DA 2I Runoff Area=0.536 ac 64.18% Impervious Runoff Depth>4.26"
Flow Length=230' Slope=0.0200 '/ Tc=11.0 min CN=92 Runoff=2.14 cfs 0.190 af

Subcatchment 21S: DA 2F Runoff Area=0.152 ac 0.00% Impervious Runoff Depth>3.63"
Flow Length=107' Tc=6.0 min CN=86 Runoff=0.62 cfs 0.046 af

Subcatchment 22S: DA 2H Runoff Area=2.748 ac 35.70% Impervious Runoff Depth>3.43"
Flow Length=676' Tc=10.0 min CN=84 Runoff=9.48 cfs 0.786 af

Pond 15P: Apartments Phase II Stormwater Peak Elev=568.73' Storage=6,631 cf Inflow=10.08 cfs 0.885 af
Outflow=8.47 cfs 0.877 af

Pond 20P: Apartments Phase II Peak Elev=557.90' Storage=28,390 cf Inflow=20.47 cfs 2.011 af
Outflow=11.01 cfs 1.967 af

Pond 21P: DMH #2 Peak Elev=565.24' Inflow=10.22 cfs 1.067 af
24.0" Round Culvert n=0.013 L=260.0' S=0.0164 '/ Outflow=10.22 cfs 1.067 af

Pond 22P: FE #2A Peak Elev=558.38' Inflow=18.88 cfs 1.852 af
36.0" Round Culvert n=0.012 L=60.0' S=0.0250 '/ Outflow=18.88 cfs 1.852 af

Link 20L: Off-Site Inflow=13.70 cfs 2.548 af
Primary=13.70 cfs 2.548 af

Total Runoff Area = 9.299 ac Runoff Volume = 2.600 af Average Runoff Depth = 3.36"
69.05% Pervious = 6.421 ac 30.95% Impervious = 2.878 ac

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Type III 24-hr 10-Year Rainfall=5.18"

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Summary for Subcatchment 15S: DA 2E

Runoff = 9.62 cfs @ 12.17 hrs, Volume= 0.839 af, Depth> 3.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
* 0.985	98	Paved parking, HSG C, South
0.455	80	>75% Grass cover, Good, HSG D
0.917	70	Woods, Good, HSG C
0.666	80	>75% Grass cover, Good, HSG D
3.023	83	Weighted Average
2.038		67.42% Pervious Area
0.985		32.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	50	0.0600	0.11		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
3.3	417	0.1799	2.12		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	40	0.1000	2.21		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
0.7	164	0.0421	4.17		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
12.0	671	Total			

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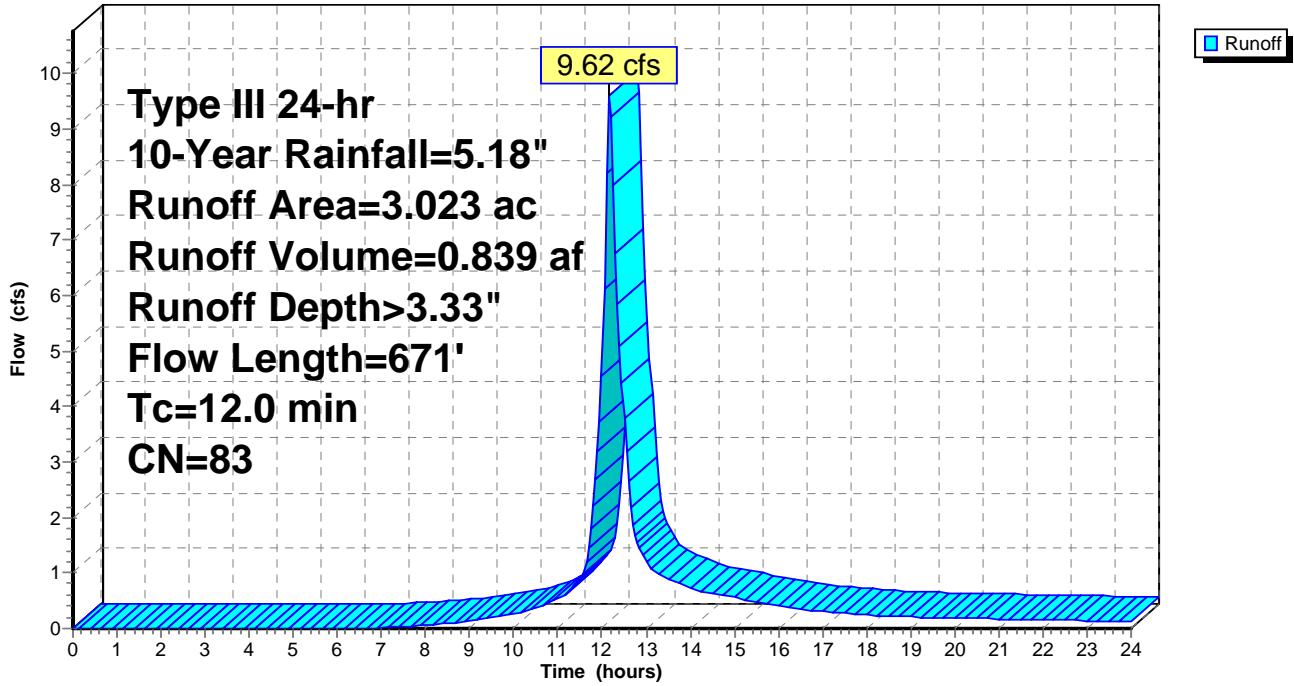
Type III 24-hr 10-Year Rainfall=5.18"

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Subcatchment 15S: DA 2E

Hydrograph



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Summary for Subcatchment 16S: DA 2G

Runoff = 2.17 cfs @ 12.09 hrs, Volume= 0.158 af, Depth> 3.43"

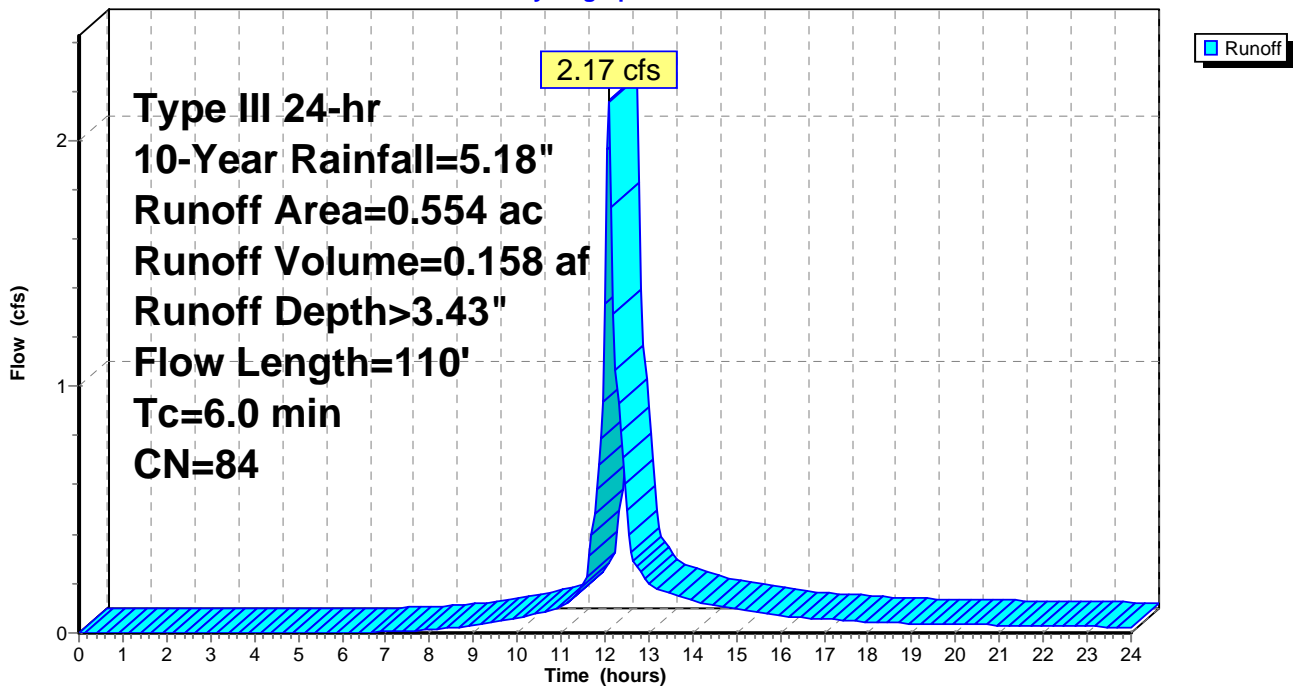
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
0.135	98	Water Surface, 0% imp, HSG C
0.017	80	>75% Grass cover, Good, HSG D
0.229	80	>75% Grass cover, Good, HSG D
0.157	80	>75% Grass cover, Good, HSG D
0.016	80	>75% Grass cover, Good, HSG D
0.554	84	Weighted Average
0.554		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.5	50	0.0500	0.15		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.2	60	0.3500	4.14		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
5.7	110	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 16S: DA 2G

Hydrograph



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Type III 24-hr 10-Year Rainfall=5.18"

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Summary for Subcatchment 17S: DA 2J

Runoff = 8.00 cfs @ 12.09 hrs, Volume= 0.581 af, Depth> 3.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
0.412	80	>75% Grass cover, Good, HSG D
0.061	98	Paved parking, HSG C
0.032	74	>75% Grass cover, Good, HSG C
0.140	98	Paved parking, HSG C
0.721	74	>75% Grass cover, Good, HSG C
* 0.184	98	Two single Family Houses and Paved Driveways
0.183	98	Paved parking, HSG C
0.524	70	Woods, Good, HSG C
0.029	74	>75% Grass cover, Good, HSG C
2.286	80	Weighted Average
1.718		75.15% Pervious Area
0.568		24.85% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.3	24	0.1000	0.17		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	26	0.0500	1.56		Sheet Flow, Paved/Gravel Smooth surfaces n= 0.011 P2= 3.37"
0.3	85	0.0824	4.62		Shallow Concentrated Flow, Gravel Unpaved Kv= 16.1 fps
0.7	105	0.1333	2.56		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
3.6	240	Total, Increased to minimum Tc = 6.0 min			

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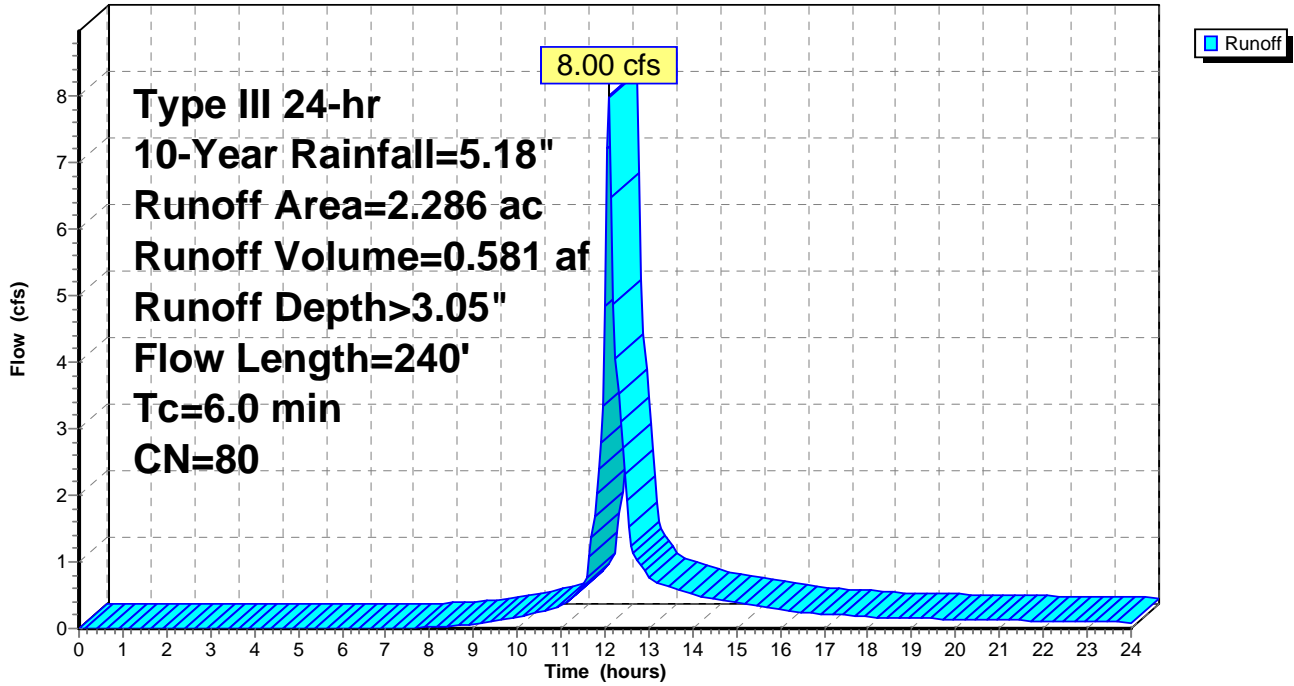
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Subcatchment 17S: DA 2J

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Summary for Subcatchment 18S: DA 2I

Runoff = 2.14 cfs @ 12.15 hrs, Volume= 0.190 af, Depth> 4.26"

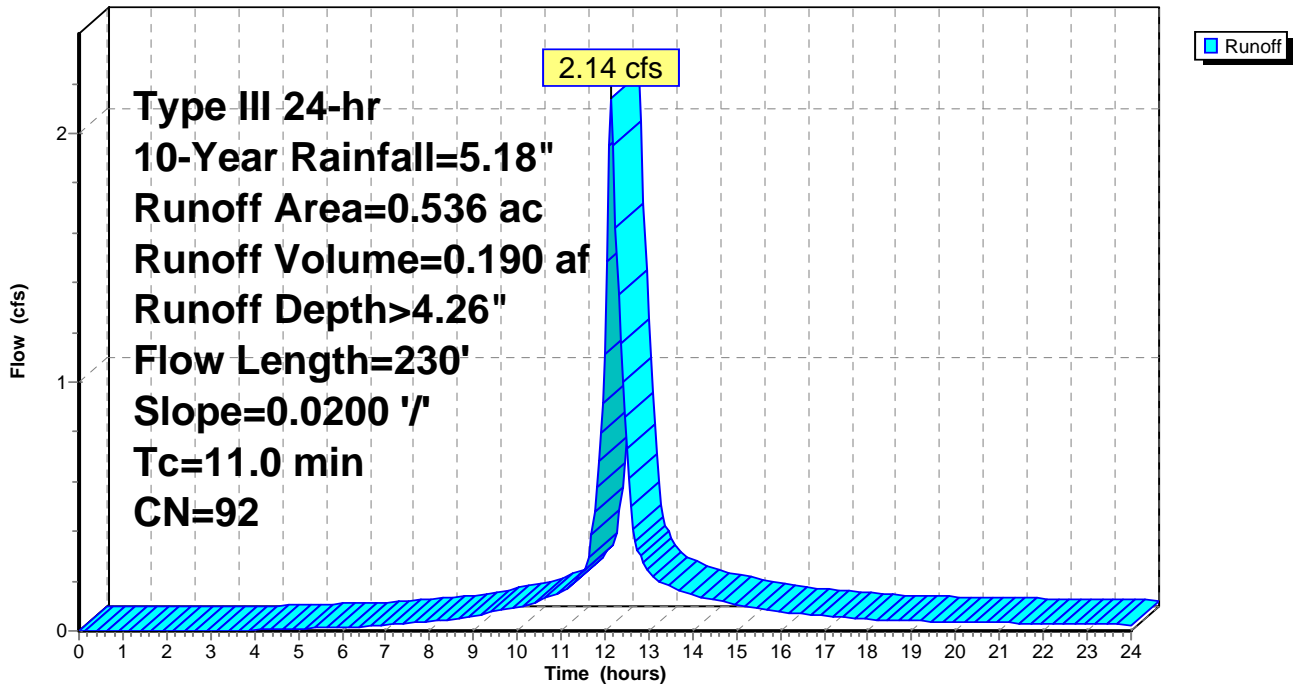
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
* 0.344	98	Paved parking, HSG C, North
0.192	80	>75% Grass cover, Good, HSG D
0.536	92	Weighted Average
0.192		35.82% Pervious Area
0.344		64.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0200	0.10		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
3.0	180	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
11.0	230	Total			

Subcatchment 18S: DA 2I

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Type III 24-hr 10-Year Rainfall=5.18"

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Summary for Subcatchment 21S: DA 2F

Runoff = 0.62 cfs @ 12.09 hrs, Volume= 0.046 af, Depth> 3.63"

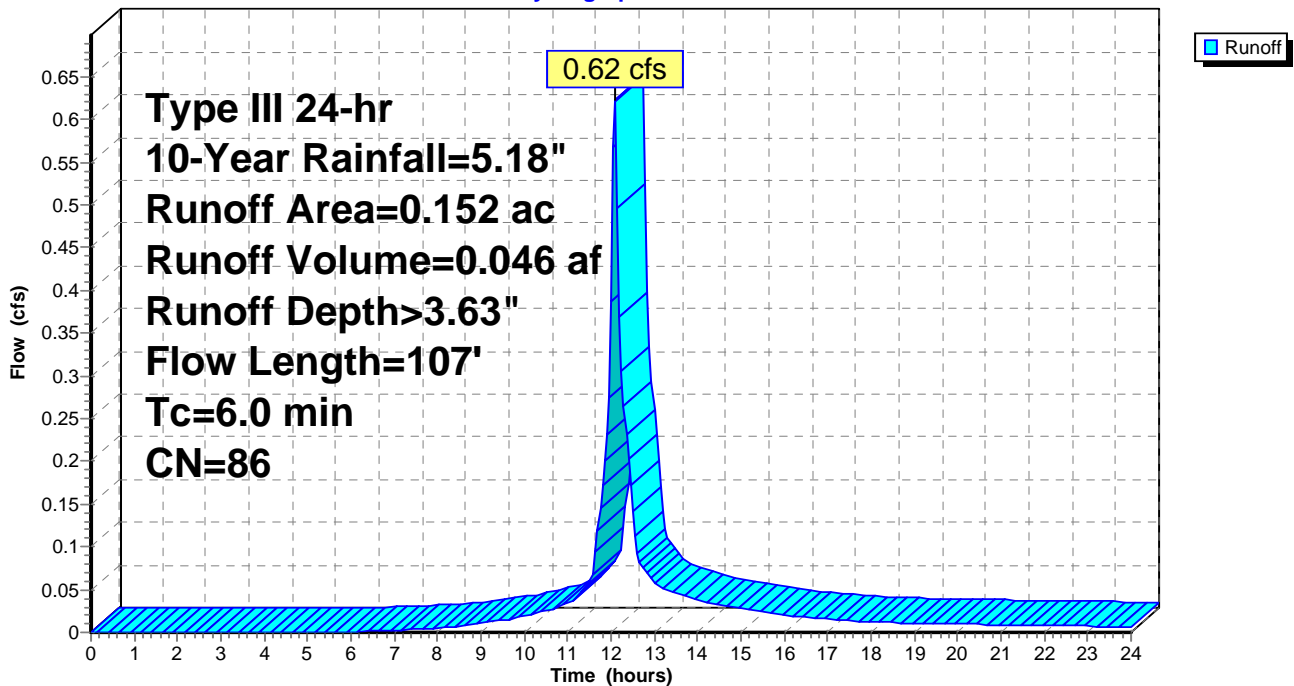
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
0.051	98	Water Surface, 0% imp, HSG C
0.101	80	>75% Grass cover, Good, HSG D
0.152	86	Weighted Average
0.152		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	50	0.1000	0.20		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	57	0.1754	2.93		Shallow Concentrated Flow, Woods Short Grass Pasture Kv= 7.0 fps
4.5	107	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 21S: DA 2F

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Type III 24-hr 10-Year Rainfall=5.18"

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Summary for Subcatchment 22S: DA 2H

Runoff = 9.48 cfs @ 12.14 hrs, Volume= 0.786 af, Depth> 3.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10-Year Rainfall=5.18"

Area (ac)	CN	Description
* 0.431	98	Paved parking, HSG C, North
* 0.010	80	>75% Grass cover, Good, HSG D, North
0.313	80	>75% Grass cover, Good, HSG D
* 0.550	98	Paved parking, HSG C, South
0.360	80	>75% Grass cover, Good, HSG D
0.748	70	Woods, Good, HSG C
0.336	80	>75% Grass cover, Good, HSG D
2.748	84	Weighted Average
1.767		64.30% Pervious Area
0.981		35.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.3	50	0.1000	0.13		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
1.7	190	0.1316	1.81		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	81	0.3333	4.04		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
1.7	355	0.0310	3.57		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
10.0	676	Total			

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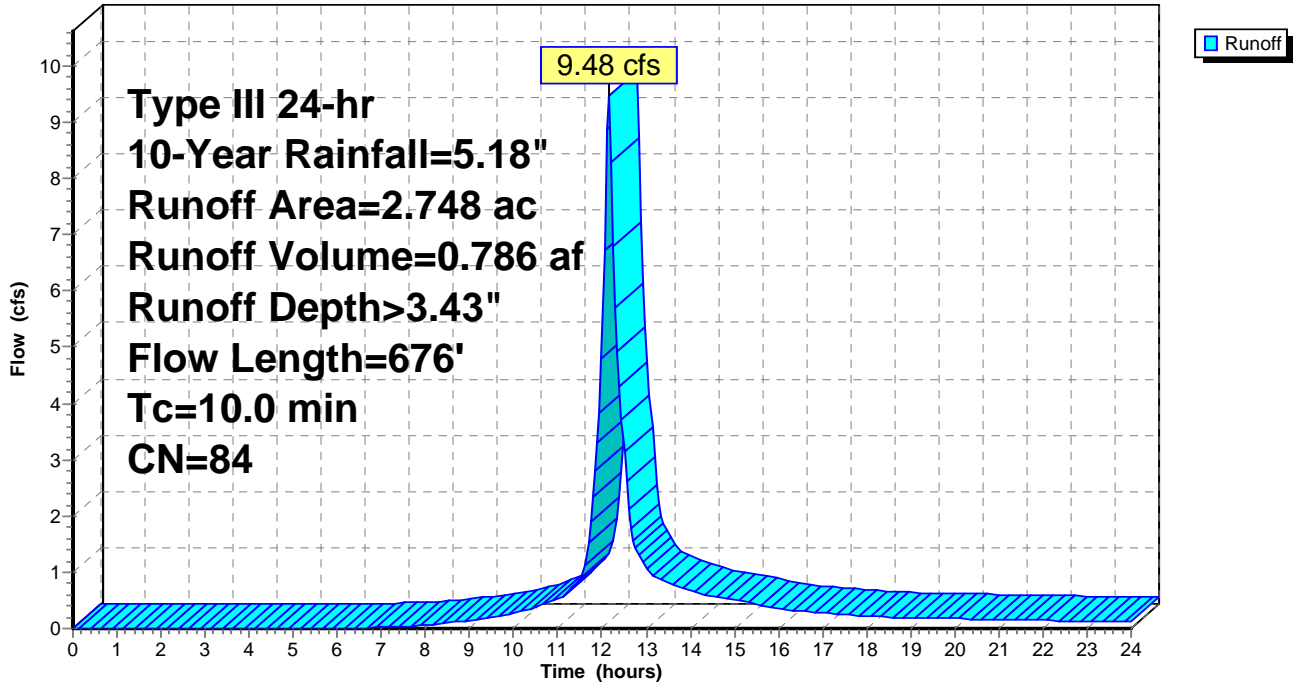
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Subcatchment 22S: DA 2H

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Summary for Pond 15P: Apartments Phase II Stormwater Basin 2

Inflow Area = 3.175 ac, 31.02% Impervious, Inflow Depth > 3.35" for 10-Year event
 Inflow = 10.08 cfs @ 12.16 hrs, Volume= 0.885 af
 Outflow = 8.47 cfs @ 12.25 hrs, Volume= 0.877 af, Atten= 16%, Lag= 5.3 min
 Primary = 8.47 cfs @ 12.25 hrs, Volume= 0.877 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 567.00' Surf.Area= 2,390 sf Storage= 1,777 cf
 Peak Elev= 568.73' @ 12.25 hrs Surf.Area= 3,241 sf Storage= 6,631 cf (4,854 cf above start)
 Flood Elev= 569.70' Surf.Area= 3,741 sf Storage= 10,022 cf (8,245 cf above start)

Plug-Flow detention time= 56.5 min calculated for 0.836 af (94% of inflow)
 Center-of-Mass det. time= 14.8 min (830.4 - 815.6)

Volume	Invert	Avail.Storage	Storage Description
#1	566.00'	11,168 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
566.00	1,164	0	0
567.00	2,390	1,777	1,777
568.00	2,867	2,629	4,406
570.00	3,895	6,762	11,168

Device	Routing	Invert	Outlet Devices
#1	Primary	566.00'	18.0" Round 18" HDPE L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 566.00' / 564.27' S= 0.0254 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	567.00'	6.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#3	Device 1	567.50'	12.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	568.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	569.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=8.46 cfs @ 12.25 hrs HW=568.73' TW=565.23' (Dynamic Tailwater)

- 1=18" HDPE (Passes 8.46 cfs of 11.97 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 2.30 cfs @ 5.85 fps)
- 3=Orifice/Grate (Orifice Controls 3.23 cfs @ 4.11 fps)
- 4=Orifice/Grate (Orifice Controls 2.94 cfs @ 2.91 fps)
- 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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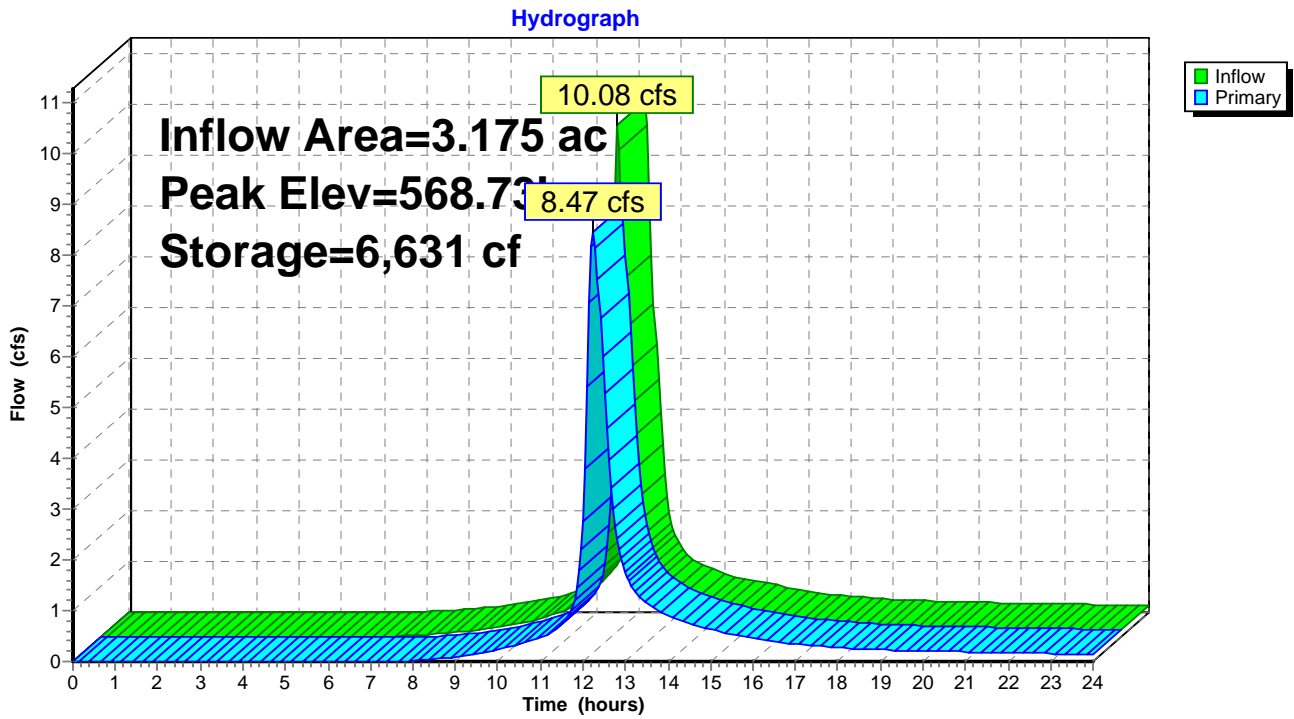
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Pond 15P: Apartments Phase II Stormwater Basin 2



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Summary for Pond 20P: Apartments Phase II Stormwater Basin 1

Inflow Area = 7.013 ac, 32.94% Impervious, Inflow Depth > 3.44" for 10-Year event
 Inflow = 20.47 cfs @ 12.16 hrs, Volume= 2.011 af
 Outflow = 11.01 cfs @ 12.46 hrs, Volume= 1.967 af, Atten= 46%, Lag= 17.7 min
 Primary = 11.01 cfs @ 12.46 hrs, Volume= 1.967 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 555.00' Surf.Area= 6,117 sf Storage= 5,401 cf
 Peak Elev= 557.90' @ 12.46 hrs Surf.Area= 9,427 sf Storage= 28,390 cf (22,989 cf above start)
 Flood Elev= 559.40' Surf.Area= 11,019 sf Storage= 43,681 cf (38,280 cf above start)

Plug-Flow detention time= 96.2 min calculated for 1.843 af (92% of inflow)
 Center-of-Mass det. time= 39.7 min (856.9 - 817.2)

Volume	Invert	Avail.Storage	Storage Description
#1	554.00'	50,485 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
554.00	4,686	0	0
556.00	7,547	12,233	12,233
558.00	9,522	17,069	29,302
560.00	11,661	21,183	50,485

Device	Routing	Invert	Outlet Devices
#1	Primary	554.00'	18.0" Round 18" HDPE L= 102.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 554.00' / 552.00' S= 0.0196 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	555.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	556.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	557.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	558.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=11.00 cfs @ 12.46 hrs HW=557.90' TW=0.00' (Dynamic Tailwater)

- 1=18" HDPE (Passes 11.00 cfs of 15.11 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 4.14 cfs @ 7.59 fps)
- 3=Orifice/Grate (Orifice Controls 3.20 cfs @ 5.87 fps)
- 4=Orifice/Grate (Orifice Controls 3.66 cfs @ 3.35 fps)
- 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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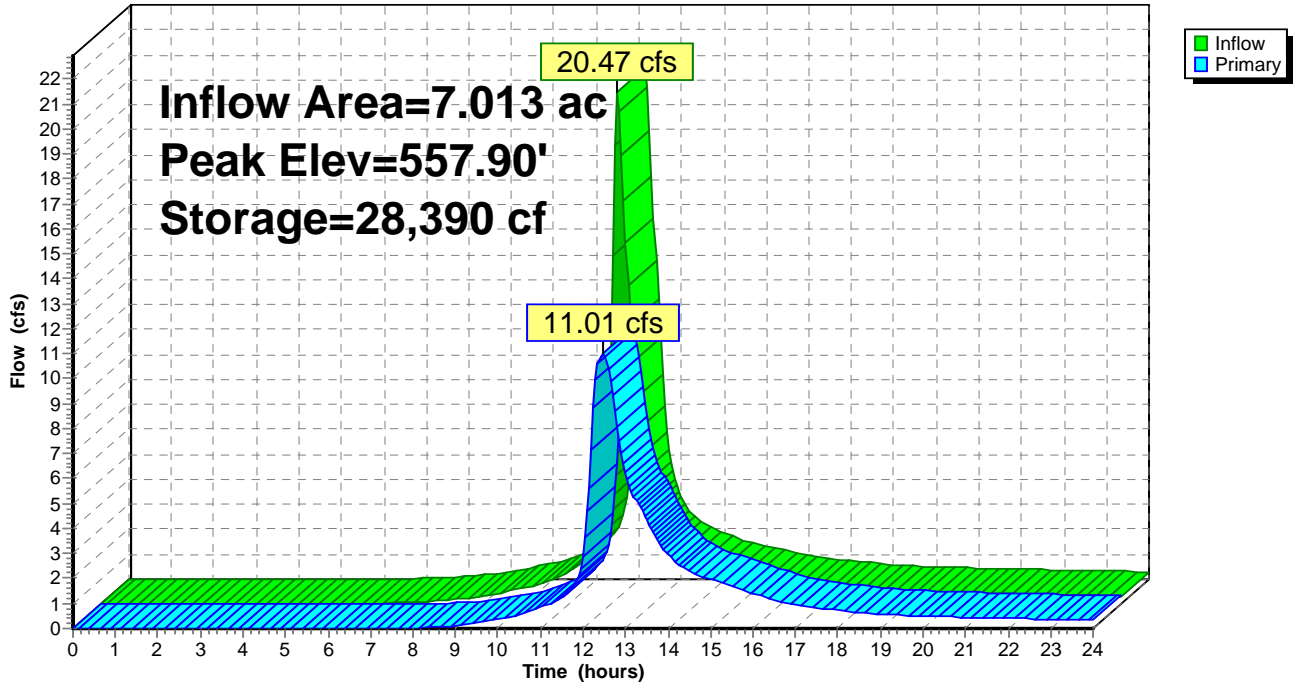
Type III 24-hr 10-Year Rainfall=5.18"

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Pond 20P: Apartments Phase II Stormwater Basin 1

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Summary for Pond 21P: DMH #2

Inflow Area = 3.711 ac, 35.81% Impervious, Inflow Depth > 3.45" for 10-Year event
 Inflow = 10.22 cfs @ 12.22 hrs, Volume= 1.067 af
 Outflow = 10.22 cfs @ 12.22 hrs, Volume= 1.067 af, Atten= 0%, Lag= 0.0 min
 Primary = 10.22 cfs @ 12.22 hrs, Volume= 1.067 af

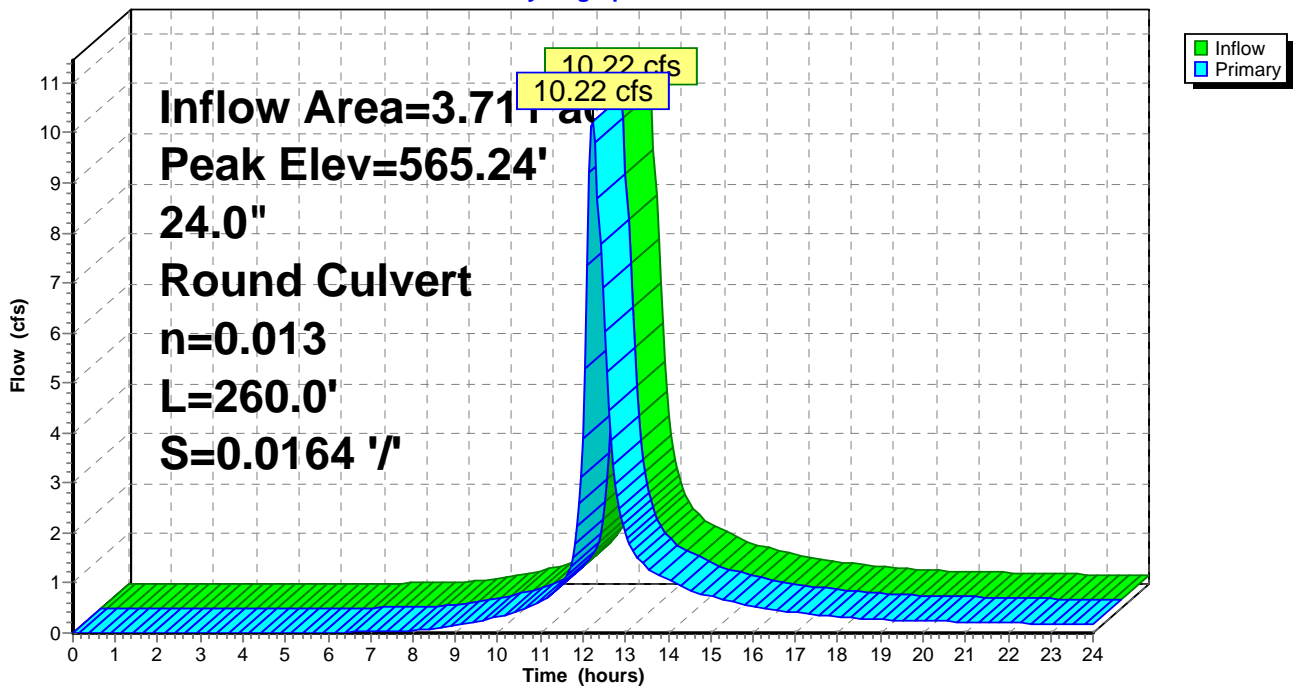
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 565.24' @ 12.22 hrs
 Flood Elev= 569.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	563.77'	24.0" Round Culvert L= 260.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 563.77' / 559.50' S= 0.0164 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=10.11 cfs @ 12.22 hrs HW=565.23' TW=558.36' (Dynamic Tailwater)
 ←1=Culvert (Inlet Controls 10.11 cfs @ 4.11 fps)

Pond 21P: DMH #2

Hydrograph



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Summary for Pond 22P: FE #2A

Inflow Area = 6.459 ac, 35.76% Impervious, Inflow Depth > 3.44" for 10-Year event
 Inflow = 18.88 cfs @ 12.17 hrs, Volume= 1.852 af
 Outflow = 18.88 cfs @ 12.17 hrs, Volume= 1.852 af, Atten= 0%, Lag= 0.0 min
 Primary = 18.88 cfs @ 12.17 hrs, Volume= 1.852 af

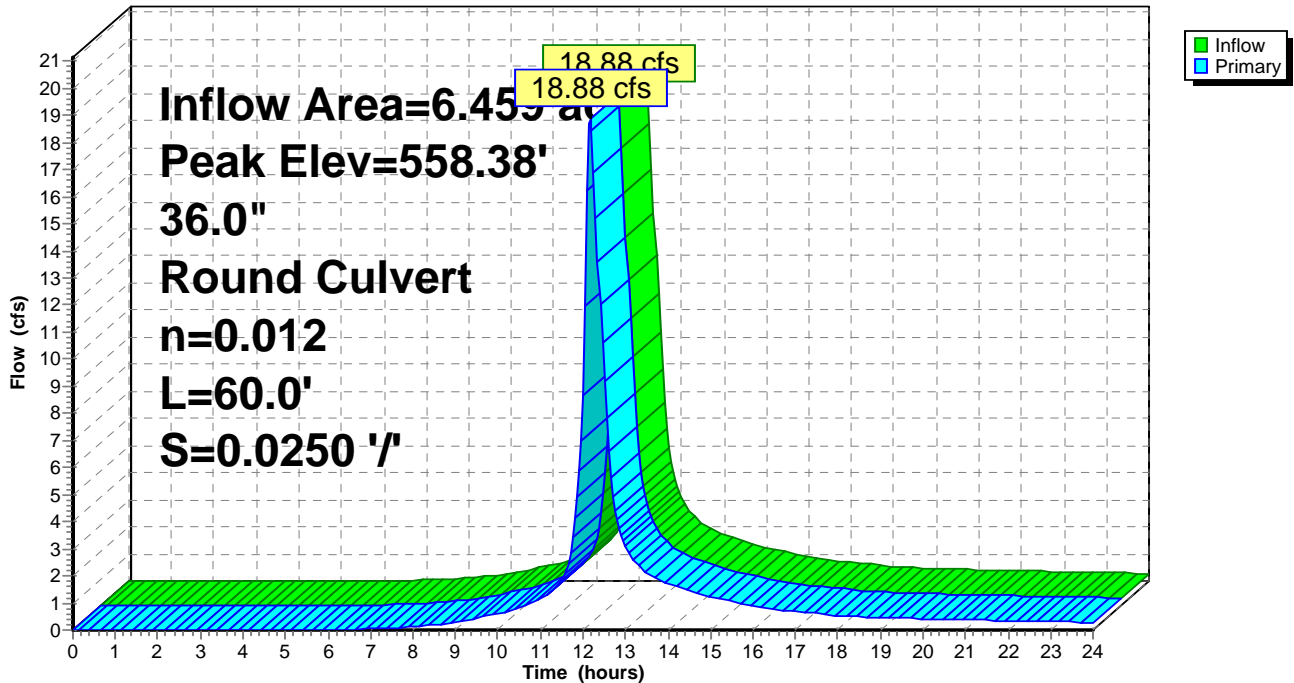
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 558.38' @ 12.28 hrs
 Flood Elev= 564.47'

Device	Routing	Invert	Outlet Devices
#1	Primary	556.50'	36.0" Round Culvert L= 60.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 556.50' / 555.00' S= 0.0250 '/ Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 7.07 sf

Primary OutFlow Max=18.61 cfs @ 12.17 hrs HW=558.29' TW=557.20' (Dynamic Tailwater)
 ←1=Culvert (Outlet Controls 18.61 cfs @ 6.07 fps)

Pond 22P: FE #2A

Hydrograph



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Type III 24-hr 10-Year Rainfall=5.18"

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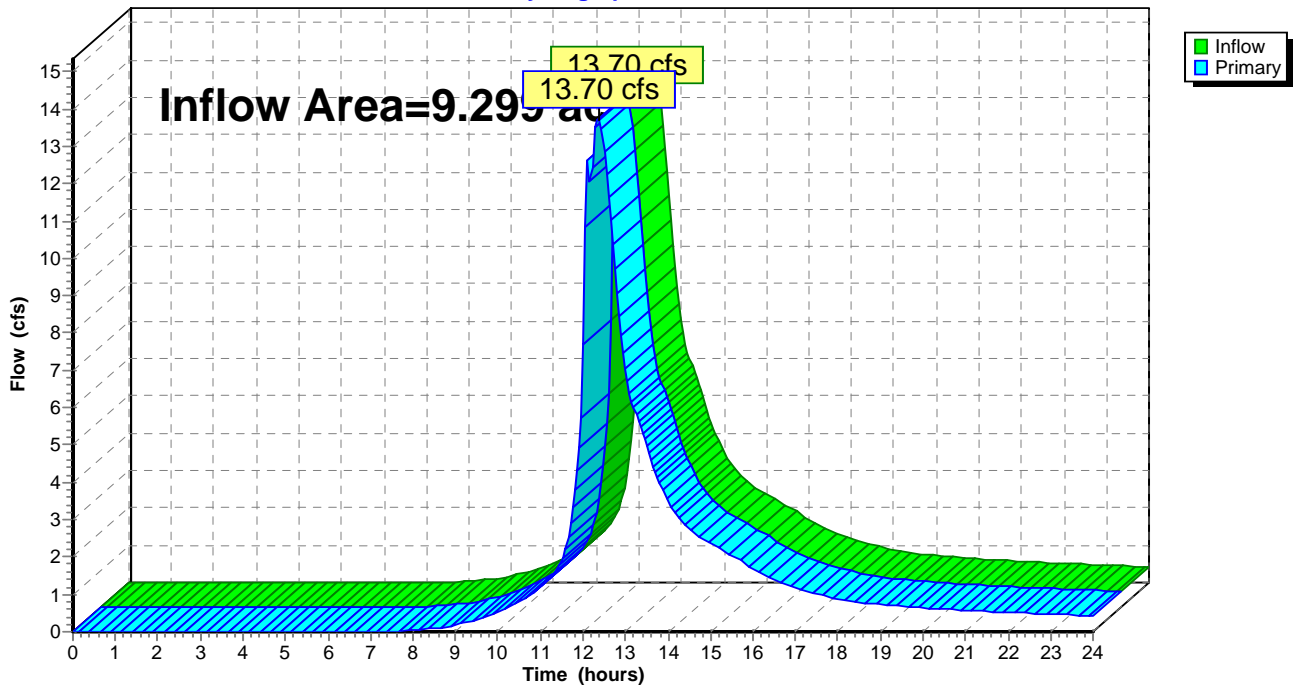
Summary for Link 20L: Off-Site

Inflow Area = 9.299 ac, 30.95% Impervious, Inflow Depth > 3.29" for 10-Year event
Inflow = 13.70 cfs @ 12.36 hrs, Volume= 2.548 af
Primary = 13.70 cfs @ 12.36 hrs, Volume= 2.548 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 20L: Off-Site

Hydrograph



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Type III 24-hr 25-Year Rainfall=6.30"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 15S: DA 2E Runoff Area=3.023 ac 32.58% Impervious Runoff Depth>4.36"
Flow Length=671' Tc=12.0 min CN=83 Runoff=12.50 cfs 1.099 af

Subcatchment 16S: DA 2G Runoff Area=0.554 ac 0.00% Impervious Runoff Depth>4.47"
Flow Length=110' Tc=6.0 min CN=84 Runoff=2.80 cfs 0.207 af

Subcatchment 17S: DA 2J Runoff Area=2.286 ac 24.85% Impervious Runoff Depth>4.05"
Flow Length=240' Tc=6.0 min CN=80 Runoff=10.57 cfs 0.771 af

Subcatchment 18S: DA 2I Runoff Area=0.536 ac 64.18% Impervious Runoff Depth>5.36"
Flow Length=230' Slope=0.0200 '/' Tc=11.0 min CN=92 Runoff=2.66 cfs 0.239 af

Subcatchment 21S: DA 2F Runoff Area=0.152 ac 0.00% Impervious Runoff Depth>4.69"
Flow Length=107' Tc=6.0 min CN=86 Runoff=0.80 cfs 0.059 af

Subcatchment 22S: DA 2H Runoff Area=2.748 ac 35.70% Impervious Runoff Depth>4.47"
Flow Length=676' Tc=10.0 min CN=84 Runoff=12.25 cfs 1.024 af

Pond 15P: Apartments Phase II Stormwater Peak Elev=569.05' Storage=7,690 cf Inflow=13.09 cfs 1.158 af
Outflow=11.03 cfs 1.149 af

Pond 20P: Apartments Phase II Peak Elev=558.35' Storage=32,709 cf Inflow=26.37 cfs 2.619 af
Outflow=16.15 cfs 2.569 af

Pond 21P: DMH #2 Peak Elev=565.52' Inflow=13.08 cfs 1.388 af
24.0" Round Culvert n=0.013 L=260.0' S=0.0164 '/' Outflow=13.08 cfs 1.388 af

Pond 22P: FE #2A Peak Elev=558.86' Inflow=24.25 cfs 2.412 af
36.0" Round Culvert n=0.012 L=60.0' S=0.0250 '/' Outflow=24.25 cfs 2.412 af

Link 20L: Off-Site Inflow=20.53 cfs 3.341 af
Primary=20.53 cfs 3.341 af

Total Runoff Area = 9.299 ac Runoff Volume = 3.400 af Average Runoff Depth = 4.39"
69.05% Pervious = 6.421 ac 30.95% Impervious = 2.878 ac

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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 15S: DA 2E

Runoff = 12.50 cfs @ 12.16 hrs, Volume= 1.099 af, Depth> 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
* 0.985	98	Paved parking, HSG C, South
0.455	80	>75% Grass cover, Good, HSG D
0.917	70	Woods, Good, HSG C
0.666	80	>75% Grass cover, Good, HSG D
3.023	83	Weighted Average
2.038		67.42% Pervious Area
0.985		32.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	50	0.0600	0.11		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
3.3	417	0.1799	2.12		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	40	0.1000	2.21		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
0.7	164	0.0421	4.17		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
12.0	671	Total			

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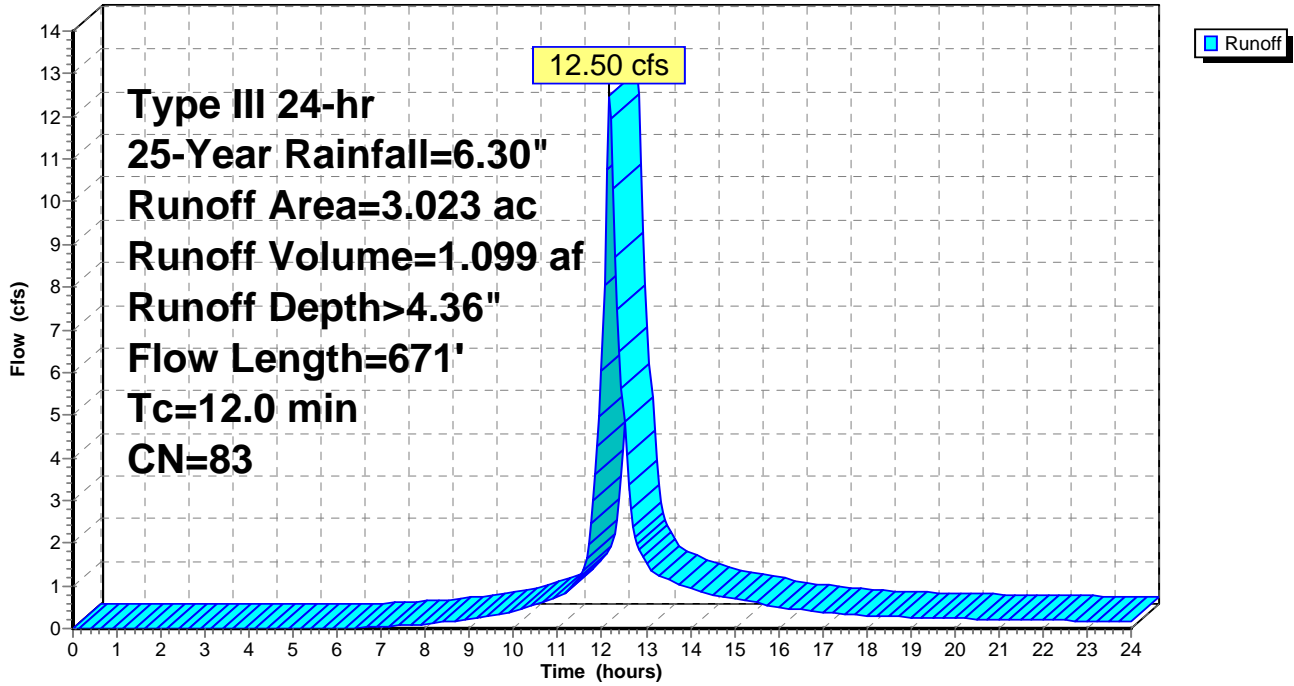
Type III 24-hr 25-Year Rainfall=6.30"

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Subcatchment 15S: DA 2E

Hydrograph



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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 16S: DA 2G

Runoff = 2.80 cfs @ 12.09 hrs, Volume= 0.207 af, Depth> 4.47"

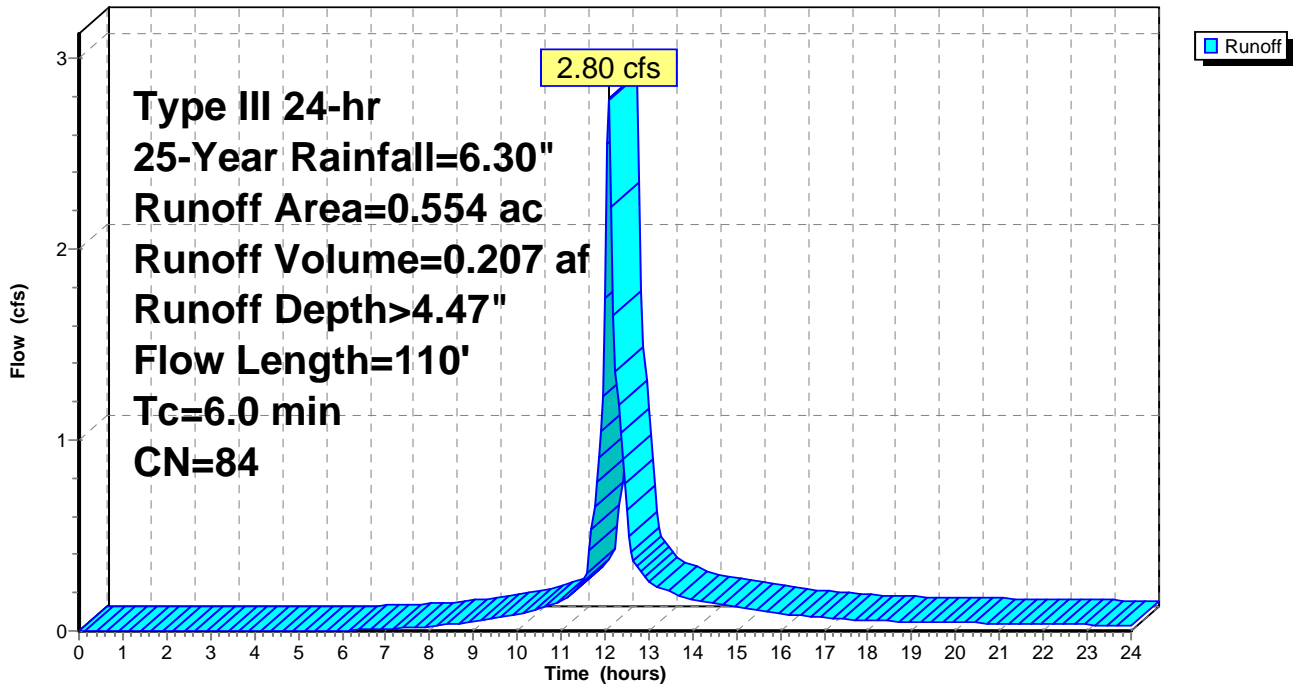
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
0.135	98	Water Surface, 0% imp, HSG C
0.017	80	>75% Grass cover, Good, HSG D
0.229	80	>75% Grass cover, Good, HSG D
0.157	80	>75% Grass cover, Good, HSG D
0.016	80	>75% Grass cover, Good, HSG D
0.554	84	Weighted Average
0.554		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.5	50	0.0500	0.15		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.2	60	0.3500	4.14		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
5.7	110	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 16S: DA 2G

Hydrograph



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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 17S: DA 2J

Runoff = 10.57 cfs @ 12.09 hrs, Volume= 0.771 af, Depth> 4.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
0.412	80	>75% Grass cover, Good, HSG D
0.061	98	Paved parking, HSG C
0.032	74	>75% Grass cover, Good, HSG C
0.140	98	Paved parking, HSG C
0.721	74	>75% Grass cover, Good, HSG C
* 0.184	98	Two single Family Houses and Paved Driveways
0.183	98	Paved parking, HSG C
0.524	70	Woods, Good, HSG C
0.029	74	>75% Grass cover, Good, HSG C
2.286	80	Weighted Average
1.718		75.15% Pervious Area
0.568		24.85% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.3	24	0.1000	0.17		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	26	0.0500	1.56		Sheet Flow, Paved/Gravel Smooth surfaces n= 0.011 P2= 3.37"
0.3	85	0.0824	4.62		Shallow Concentrated Flow, Gravel Unpaved Kv= 16.1 fps
0.7	105	0.1333	2.56		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
3.6	240	Total, Increased to minimum Tc = 6.0 min			

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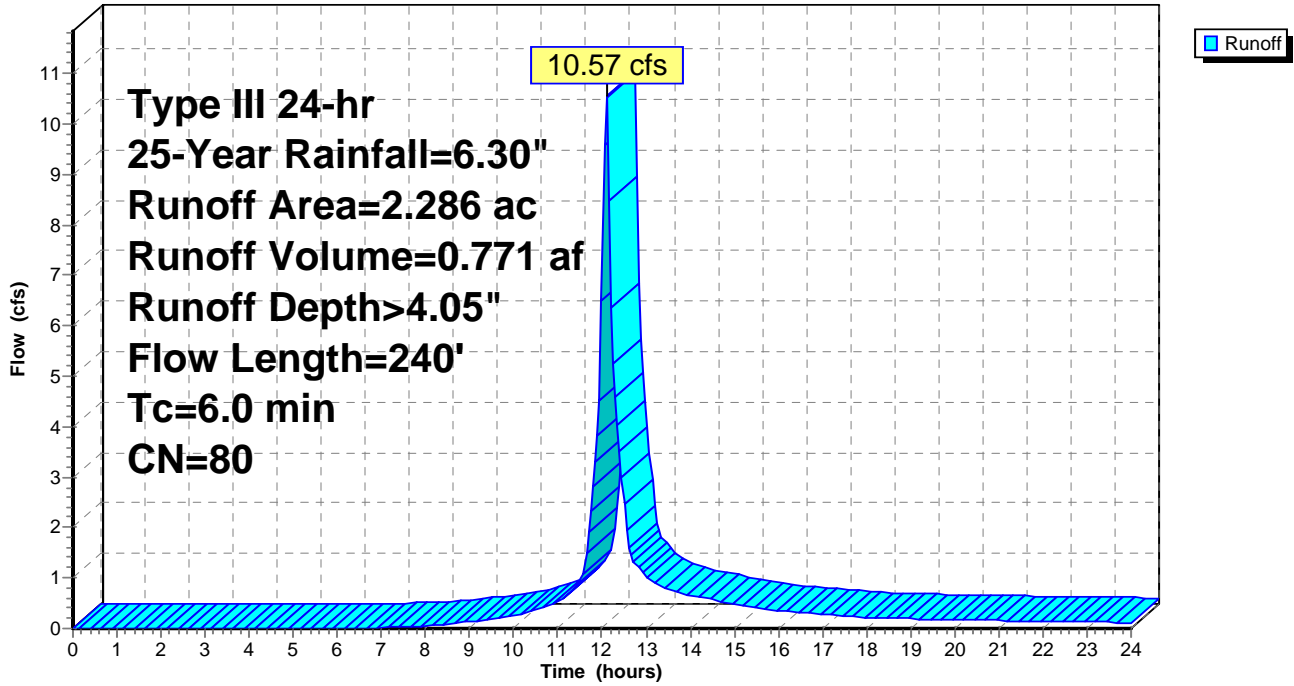
Type III 24-hr 25-Year Rainfall=6.30"

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Subcatchment 17S: DA 2J

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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 18S: DA 2I

Runoff = 2.66 cfs @ 12.15 hrs, Volume= 0.239 af, Depth> 5.36"

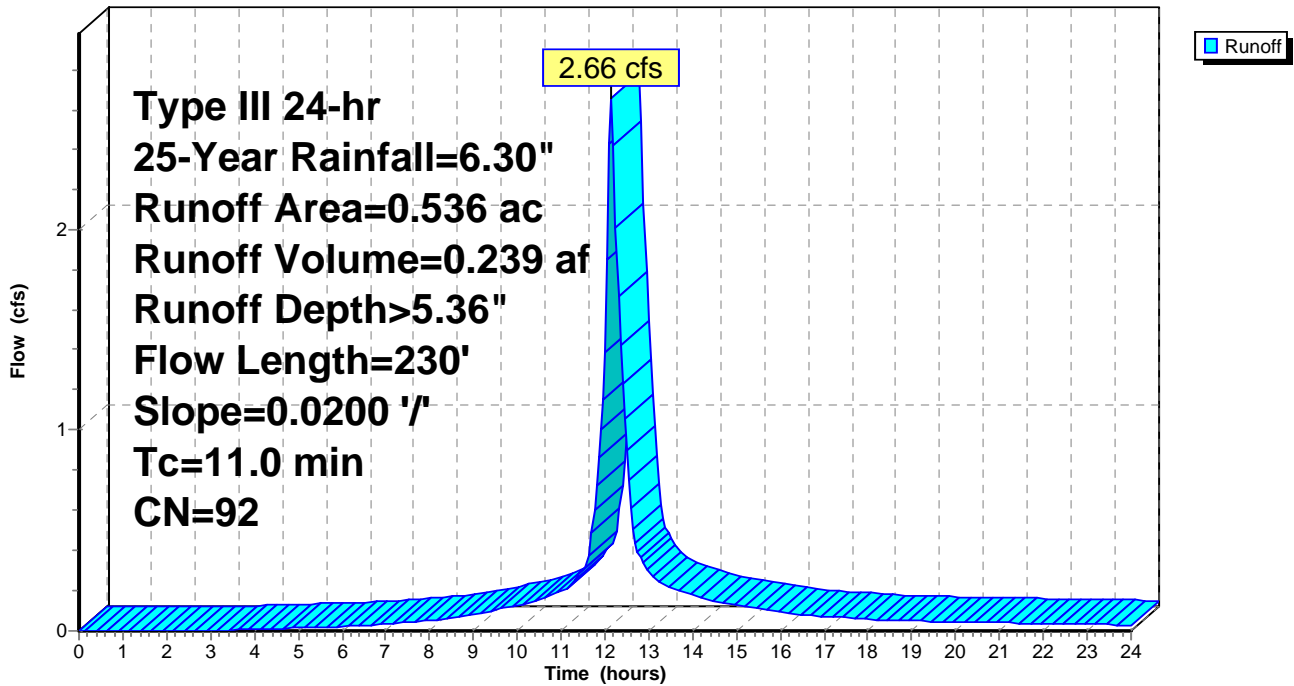
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
* 0.344	98	Paved parking, HSG C, North
0.192	80	>75% Grass cover, Good, HSG D
0.536	92	Weighted Average
0.192		35.82% Pervious Area
0.344		64.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0200	0.10		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
3.0	180	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
11.0	230	Total			

Subcatchment 18S: DA 2I

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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 21S: DA 2F

Runoff = 0.80 cfs @ 12.09 hrs, Volume= 0.059 af, Depth> 4.69"

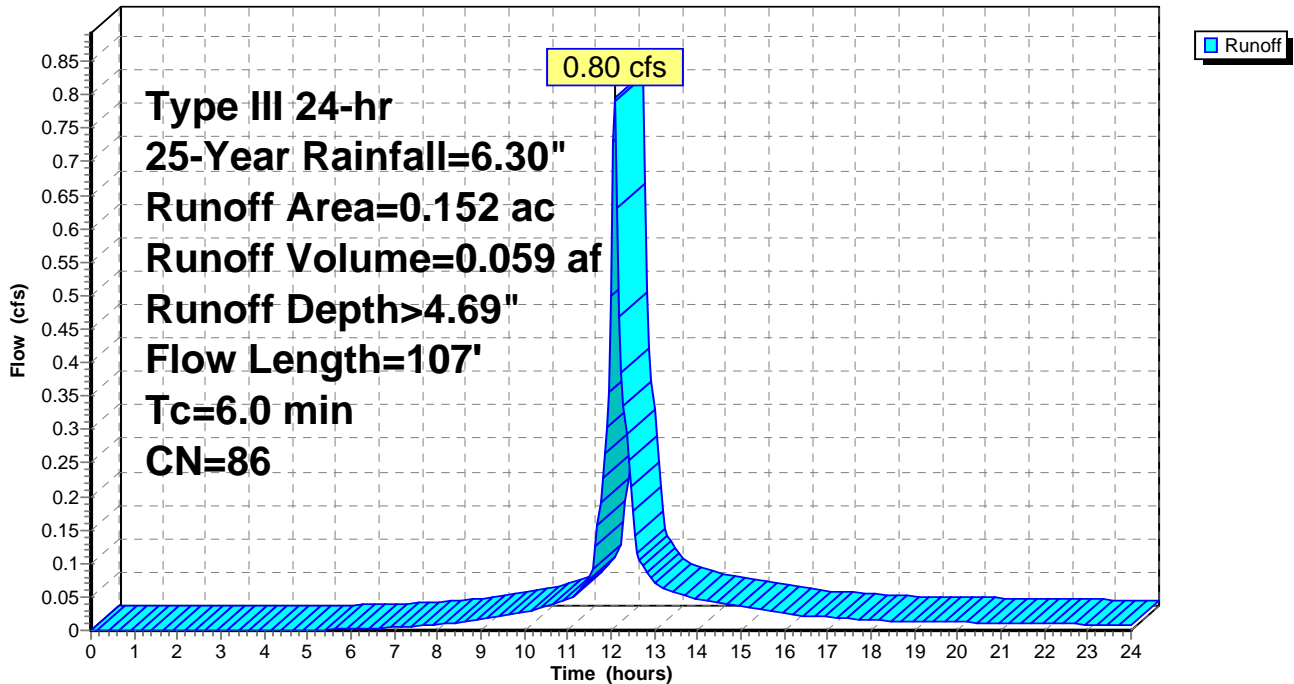
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
0.051	98	Water Surface, 0% imp, HSG C
0.101	80	>75% Grass cover, Good, HSG D
0.152	86	Weighted Average
0.152		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	50	0.1000	0.20		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	57	0.1754	2.93		Shallow Concentrated Flow, Woods Short Grass Pasture Kv= 7.0 fps
4.5	107	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 21S: DA 2F

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Type III 24-hr 25-Year Rainfall=6.30"

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Summary for Subcatchment 22S: DA 2H

Runoff = 12.25 cfs @ 12.14 hrs, Volume= 1.024 af, Depth> 4.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 25-Year Rainfall=6.30"

Area (ac)	CN	Description
* 0.431	98	Paved parking, HSG C, North
* 0.010	80	>75% Grass cover, Good, HSG D, North
0.313	80	>75% Grass cover, Good, HSG D
* 0.550	98	Paved parking, HSG C, South
0.360	80	>75% Grass cover, Good, HSG D
0.748	70	Woods, Good, HSG C
0.336	80	>75% Grass cover, Good, HSG D
2.748	84	Weighted Average
1.767		64.30% Pervious Area
0.981		35.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.3	50	0.1000	0.13		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
1.7	190	0.1316	1.81		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	81	0.3333	4.04		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
1.7	355	0.0310	3.57		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
10.0	676	Total			

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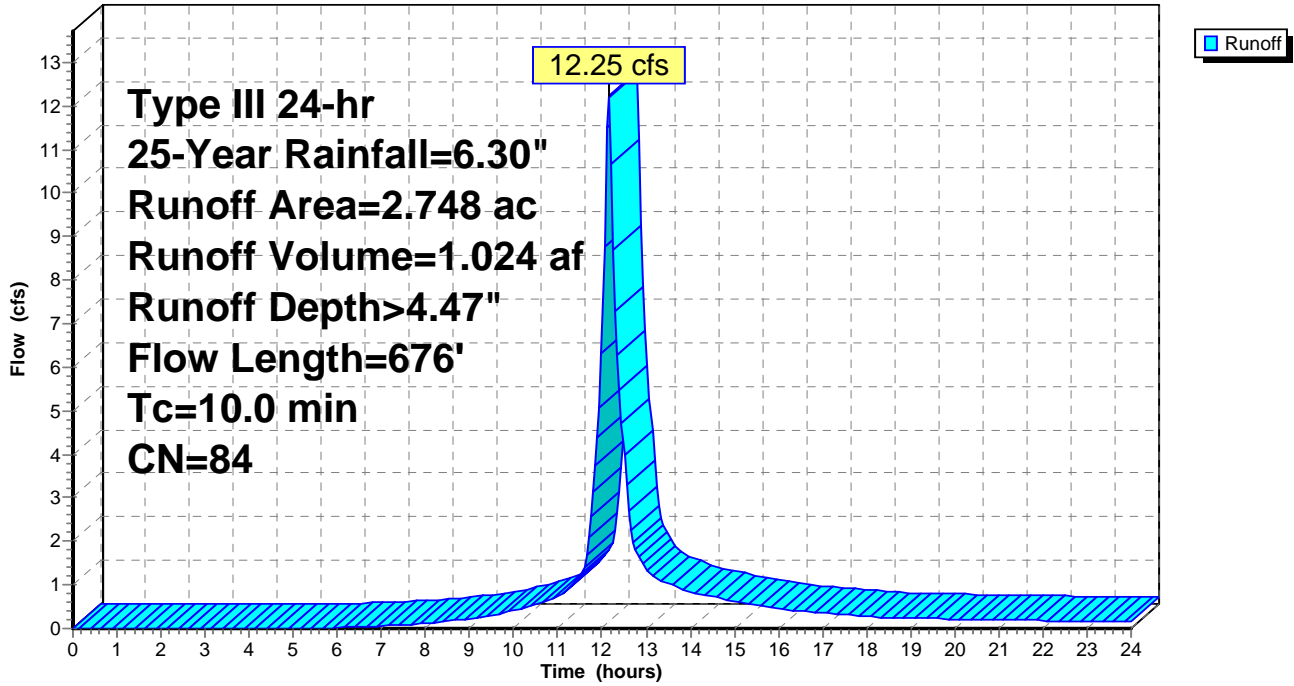
Type III 24-hr 25-Year Rainfall=6.30"

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Subcatchment 22S: DA 2H

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Summary for Pond 15P: Apartments Phase II Stormwater Basin 2

Inflow Area = 3.175 ac, 31.02% Impervious, Inflow Depth > 4.38" for 25-Year event
 Inflow = 13.09 cfs @ 12.16 hrs, Volume= 1.158 af
 Outflow = 11.03 cfs @ 12.25 hrs, Volume= 1.149 af, Atten= 16%, Lag= 5.4 min
 Primary = 11.03 cfs @ 12.25 hrs, Volume= 1.149 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 567.00' Surf.Area= 2,390 sf Storage= 1,777 cf
 Peak Elev= 569.05' @ 12.25 hrs Surf.Area= 3,405 sf Storage= 7,690 cf (5,913 cf above start)
 Flood Elev= 569.70' Surf.Area= 3,741 sf Storage= 10,022 cf (8,245 cf above start)

Plug-Flow detention time= 48.5 min calculated for 1.108 af (96% of inflow)
 Center-of-Mass det. time= 13.9 min (821.9 - 808.1)

Volume	Invert	Avail.Storage	Storage Description
#1	566.00'	11,168 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
566.00	1,164	0	0
567.00	2,390	1,777	1,777
568.00	2,867	2,629	4,406
570.00	3,895	6,762	11,168

Device	Routing	Invert	Outlet Devices
#1	Primary	566.00'	18.0" Round 18" HDPE L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 566.00' / 564.27' S= 0.0254 1/8" Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	567.00'	6.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#3	Device 1	567.50'	12.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	568.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	569.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=11.02 cfs @ 12.25 hrs HW=569.05' TW=565.51' (Dynamic Tailwater)

- 1=18" HDPE (Passes 11.02 cfs of 12.89 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 2.53 cfs @ 6.45 fps)
- 3=Orifice/Grate (Orifice Controls 3.87 cfs @ 4.93 fps)
- 4=Orifice/Grate (Orifice Controls 4.17 cfs @ 3.82 fps)
- 5=Broad-Crested Rectangular Weir (Weir Controls 0.45 cfs @ 0.60 fps)

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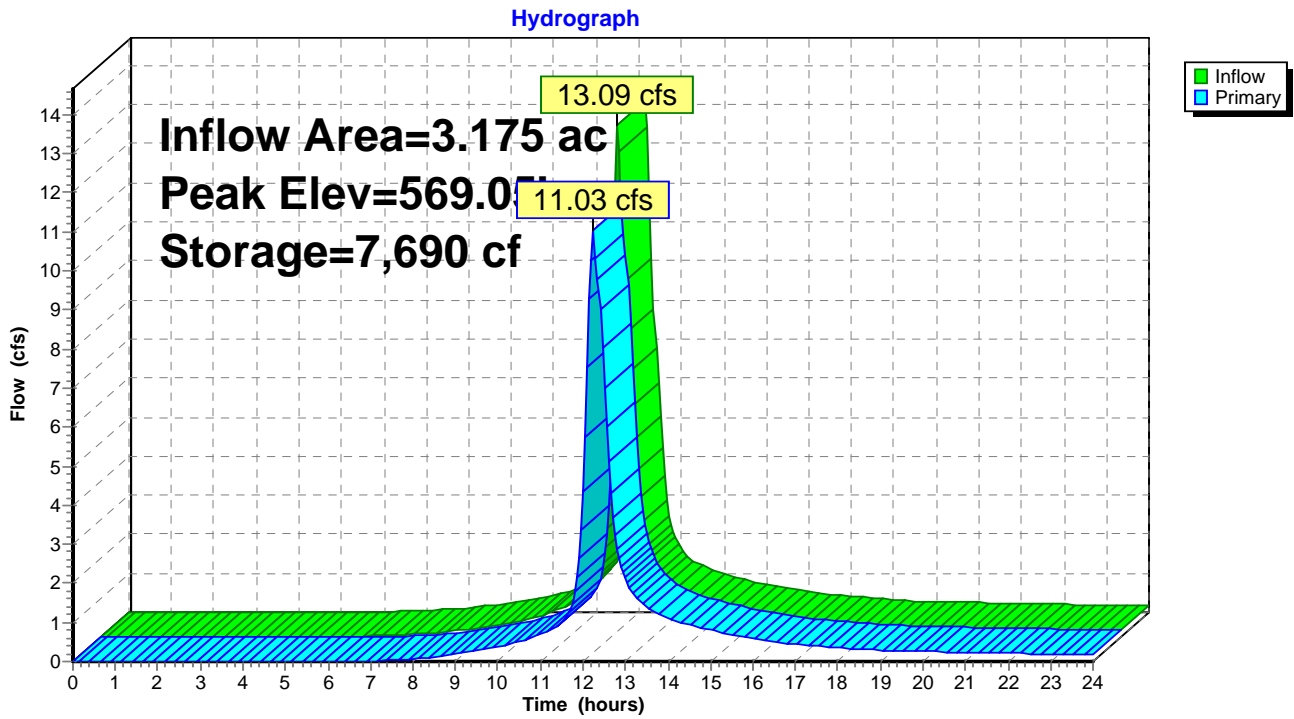
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Type III 24-hr 25-Year Rainfall=6.30"

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Pond 15P: Apartments Phase II Stormwater Basin 2



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Summary for Pond 20P: Apartments Phase II Stormwater Basin 1

Inflow Area = 7.013 ac, 32.94% Impervious, Inflow Depth > 4.48" for 25-Year event
 Inflow = 26.37 cfs @ 12.16 hrs, Volume= 2.619 af
 Outflow = 16.15 cfs @ 12.41 hrs, Volume= 2.569 af, Atten= 39%, Lag= 15.3 min
 Primary = 16.15 cfs @ 12.41 hrs, Volume= 2.569 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 555.00' Surf.Area= 6,117 sf Storage= 5,401 cf
 Peak Elev= 558.35' @ 12.41 hrs Surf.Area= 9,897 sf Storage= 32,709 cf (27,307 cf above start)
 Flood Elev= 559.40' Surf.Area= 11,019 sf Storage= 43,681 cf (38,280 cf above start)

Plug-Flow detention time= 84.2 min calculated for 2.440 af (93% of inflow)
 Center-of-Mass det. time= 36.9 min (846.5 - 809.6)

Volume	Invert	Avail.Storage	Storage Description
#1	554.00'	50,485 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
554.00	4,686	0	0
556.00	7,547	12,233	12,233
558.00	9,522	17,069	29,302
560.00	11,661	21,183	50,485

Device	Routing	Invert	Outlet Devices
#1	Primary	554.00'	18.0" Round 18" HDPE L= 102.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 554.00' / 552.00' S= 0.0196 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	555.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	556.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	557.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	558.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=16.14 cfs @ 12.41 hrs HW=558.35' TW=0.00' (Dynamic Tailwater)

- 1=18" HDPE (Inlet Controls 16.14 cfs @ 9.13 fps)
- 2=Orifice/Grate (Passes < 4.50 cfs potential flow)
- 3=Orifice/Grate (Passes < 3.65 cfs potential flow)
- 4=Orifice/Grate (Passes < 5.07 cfs potential flow)
- 5=Broad-Crested Rectangular Weir (Passes < 9.48 cfs potential flow)

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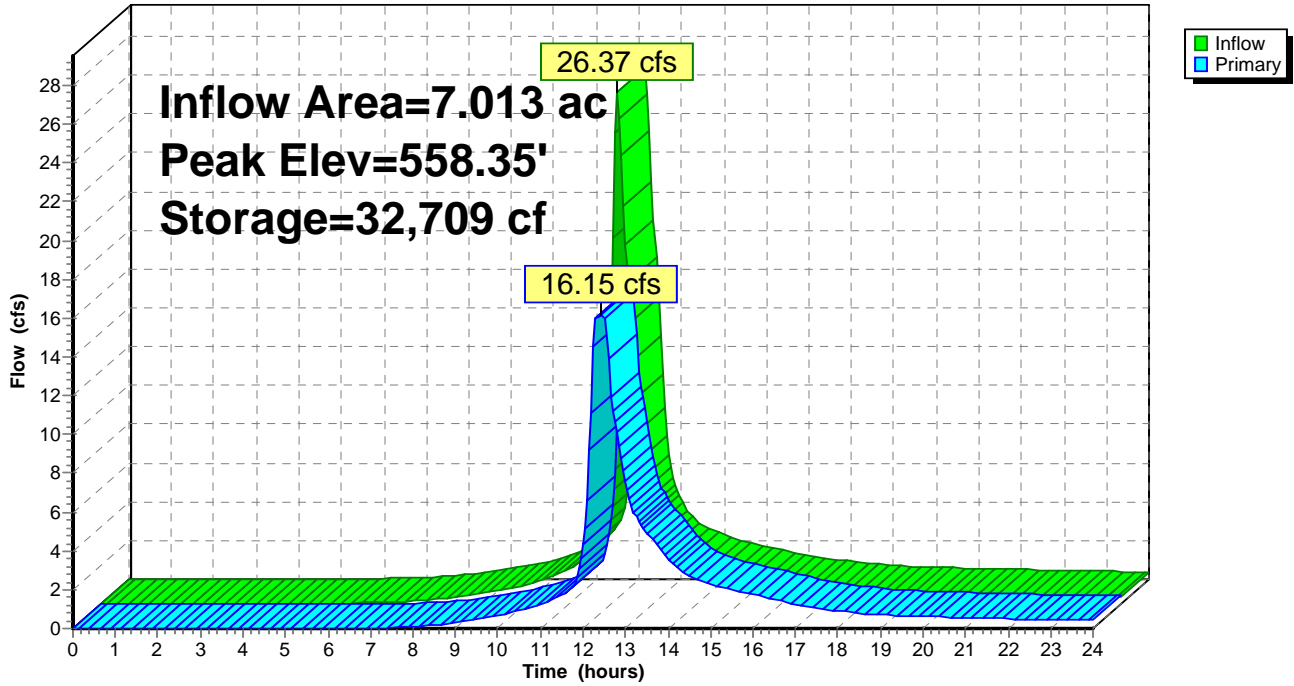
Type III 24-hr 25-Year Rainfall=6.30"

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Pond 20P: Apartments Phase II Stormwater Basin 1

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Summary for Pond 21P: DMH #2

Inflow Area = 3.711 ac, 35.81% Impervious, Inflow Depth > 4.49" for 25-Year event
Inflow = 13.08 cfs @ 12.24 hrs, Volume= 1.388 af
Outflow = 13.08 cfs @ 12.24 hrs, Volume= 1.388 af, Atten= 0%, Lag= 0.0 min
Primary = 13.08 cfs @ 12.24 hrs, Volume= 1.388 af

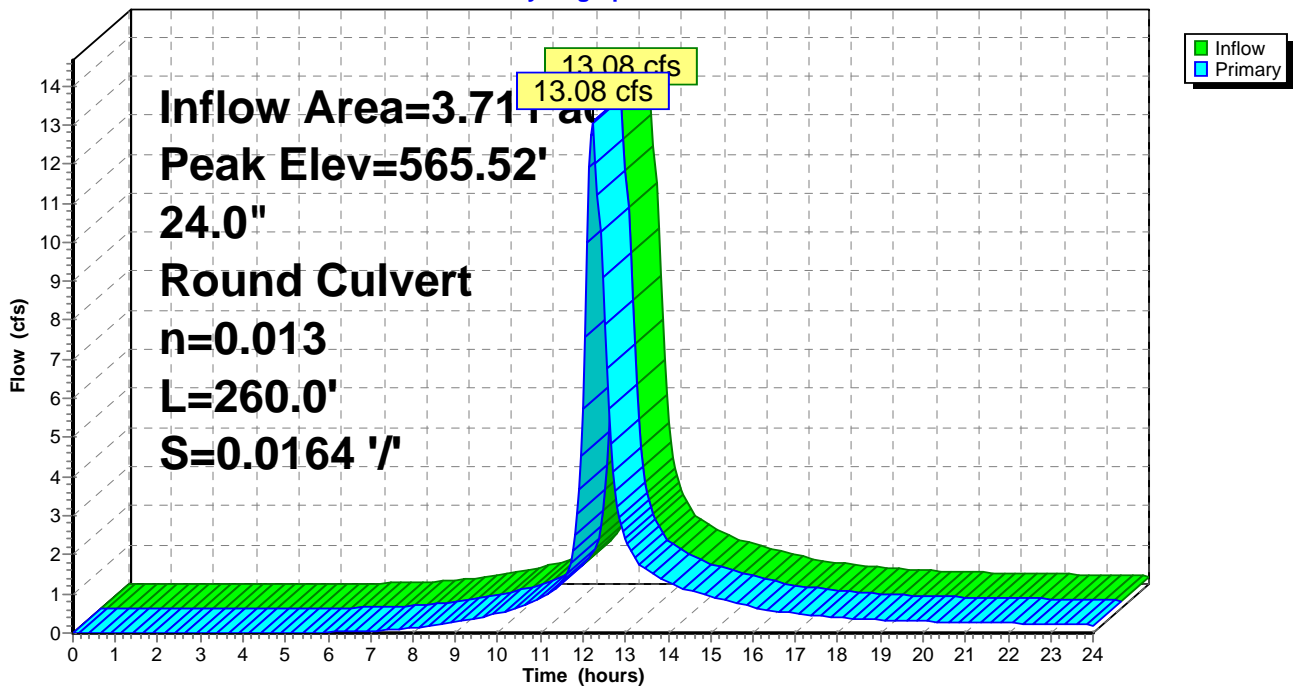
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 565.52' @ 12.24 hrs
Flood Elev= 569.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	563.77'	24.0" Round Culvert L= 260.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 563.77' / 559.50' S= 0.0164 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=12.95 cfs @ 12.24 hrs HW=565.50' TW=558.84' (Dynamic Tailwater)
↑1=Culvert (Inlet Controls 12.95 cfs @ 4.48 fps)

Pond 21P: DMH #2

Hydrograph



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Summary for Pond 22P: FE #2A

Inflow Area = 6.459 ac, 35.76% Impervious, Inflow Depth > 4.48" for 25-Year event
 Inflow = 24.25 cfs @ 12.16 hrs, Volume= 2.412 af
 Outflow = 24.25 cfs @ 12.16 hrs, Volume= 2.412 af, Atten= 0%, Lag= 0.0 min
 Primary = 24.25 cfs @ 12.16 hrs, Volume= 2.412 af

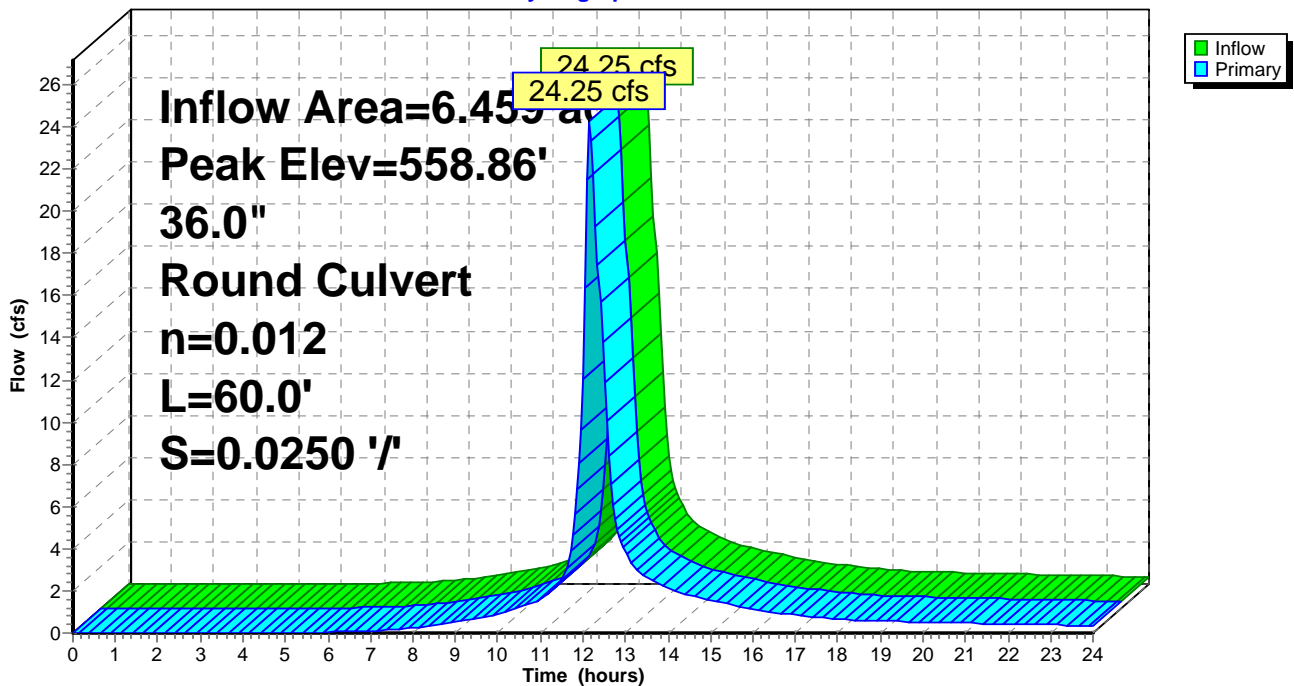
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 558.86' @ 12.26 hrs
 Flood Elev= 564.47'

Device	Routing	Invert	Outlet Devices
#1	Primary	556.50'	36.0" Round Culvert L= 60.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 556.50' / 555.00' S= 0.0250 '/ Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 7.07 sf

Primary OutFlow Max=23.97 cfs @ 12.16 hrs HW=558.72' TW=557.71' (Dynamic Tailwater)
 ←1=Culvert (Outlet Controls 23.97 cfs @ 5.95 fps)

Pond 22P: FE #2A

Hydrograph



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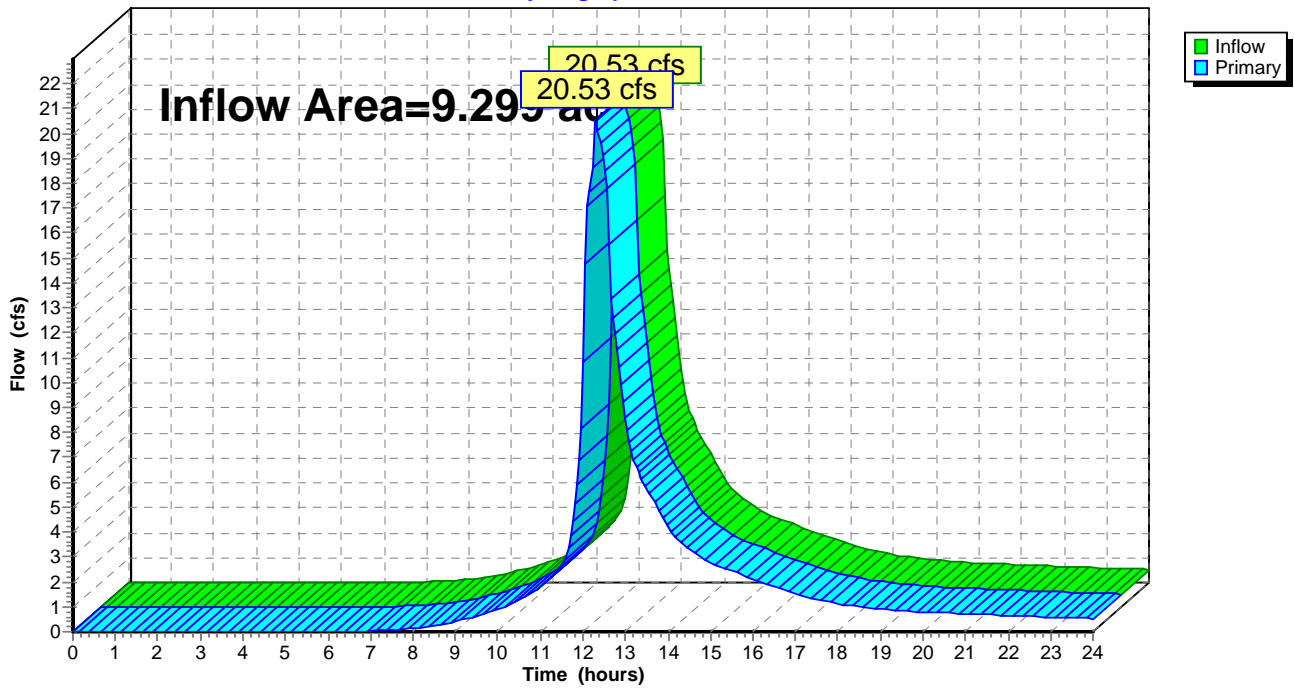
Summary for Link 20L: Off-Site

Inflow Area = 9.299 ac, 30.95% Impervious, Inflow Depth > 4.31" for 25-Year event
Inflow = 20.53 cfs @ 12.31 hrs, Volume= 3.341 af
Primary = 20.53 cfs @ 12.31 hrs, Volume= 3.341 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 20L: Off-Site

Hydrograph



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Type III 24-hr 50-Year Rainfall=7.14"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 15S: DA 2E Runoff Area=3.023 ac 32.58% Impervious Runoff Depth>5.15"
Flow Length=671' Tc=12.0 min CN=83 Runoff=14.67 cfs 1.298 af

Subcatchment 16S: DA 2G Runoff Area=0.554 ac 0.00% Impervious Runoff Depth>5.27"
Flow Length=110' Tc=6.0 min CN=84 Runoff=3.27 cfs 0.243 af

Subcatchment 17S: DA 2J Runoff Area=2.286 ac 24.85% Impervious Runoff Depth>4.82"
Flow Length=240' Tc=6.0 min CN=80 Runoff=12.52 cfs 0.918 af

Subcatchment 18S: DA 2I Runoff Area=0.536 ac 64.18% Impervious Runoff Depth>6.18"
Flow Length=230' Slope=0.0200 '/ Tc=11.0 min CN=92 Runoff=3.04 cfs 0.276 af

Subcatchment 21S: DA 2F Runoff Area=0.152 ac 0.00% Impervious Runoff Depth>5.50"
Flow Length=107' Tc=6.0 min CN=86 Runoff=0.93 cfs 0.070 af

Subcatchment 22S: DA 2H Runoff Area=2.748 ac 35.70% Impervious Runoff Depth>5.27"
Flow Length=676' Tc=10.0 min CN=84 Runoff=14.32 cfs 1.206 af

Pond 15P: Apartments Phase II Stormwater Peak Elev=569.20' Storage=8,233 cf Inflow=15.36 cfs 1.367 af
Outflow=13.37 cfs 1.357 af

Pond 20P: Apartments Phase II Peak Elev=558.85' Storage=37,754 cf Inflow=30.88 cfs 3.082 af
Outflow=17.22 cfs 3.029 af

Pond 21P: DMH #2 Peak Elev=565.92' Inflow=16.19 cfs 1.633 af
24.0" Round Culvert n=0.013 L=260.0' S=0.0164 '/ Outflow=16.19 cfs 1.633 af

Pond 22P: FE #2A Peak Elev=559.26' Inflow=28.70 cfs 2.839 af
36.0" Round Culvert n=0.012 L=60.0' S=0.0250 '/ Outflow=28.70 cfs 2.839 af

Link 20L: Off-Site Inflow=23.57 cfs 3.947 af
Primary=23.57 cfs 3.947 af

Total Runoff Area = 9.299 ac Runoff Volume = 4.011 af Average Runoff Depth = 5.18"
69.05% Pervious = 6.421 ac 30.95% Impervious = 2.878 ac

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Summary for Subcatchment 15S: DA 2E

Runoff = 14.67 cfs @ 12.16 hrs, Volume= 1.298 af, Depth> 5.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
* 0.985	98	Paved parking, HSG C, South
0.455	80	>75% Grass cover, Good, HSG D
0.917	70	Woods, Good, HSG C
0.666	80	>75% Grass cover, Good, HSG D
3.023	83	Weighted Average
2.038		67.42% Pervious Area
0.985		32.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	50	0.0600	0.11		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
3.3	417	0.1799	2.12		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	40	0.1000	2.21		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
0.7	164	0.0421	4.17		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
12.0	671	Total			

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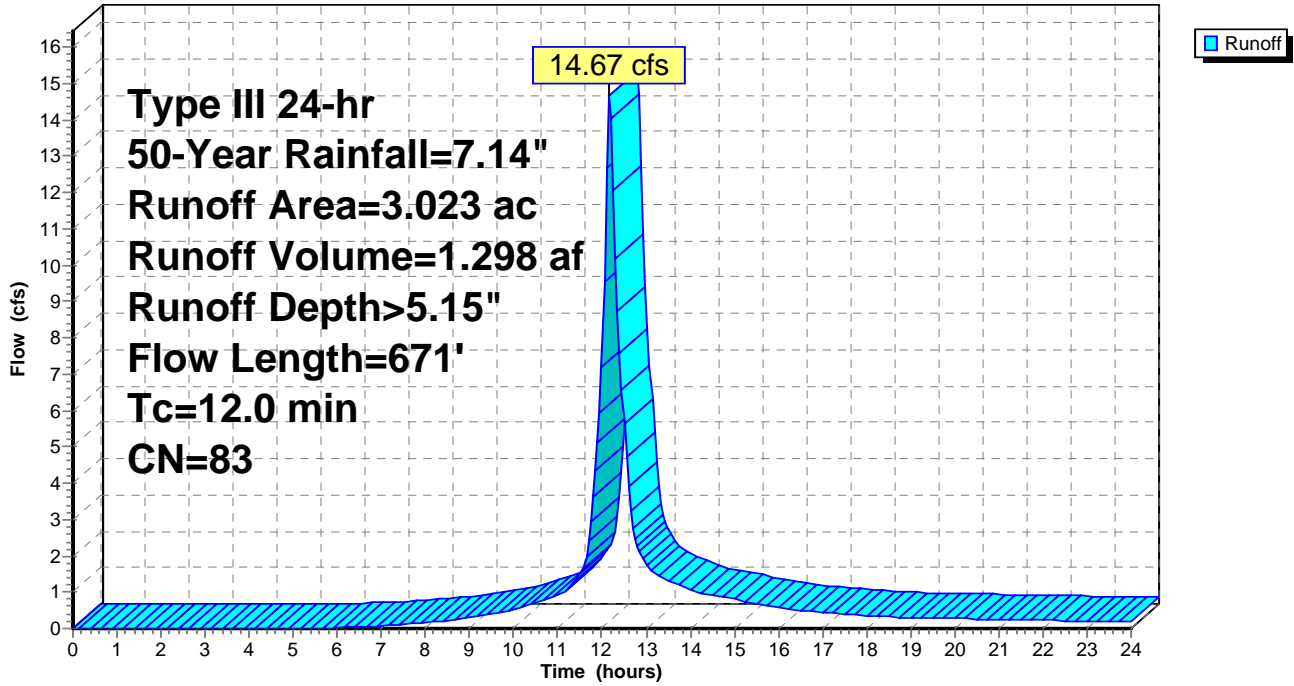
Type III 24-hr 50-Year Rainfall=7.14"

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Subcatchment 15S: DA 2E

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Summary for Subcatchment 16S: DA 2G

Runoff = 3.27 cfs @ 12.09 hrs, Volume= 0.243 af, Depth> 5.27"

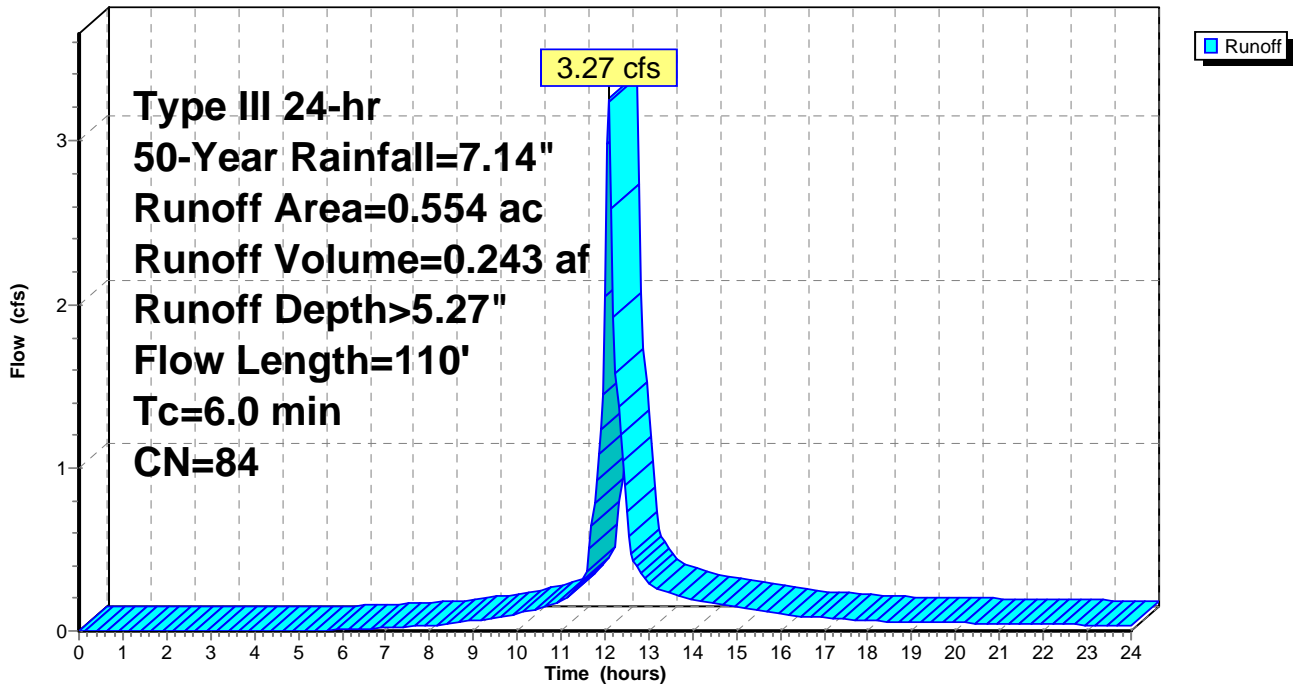
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
0.135	98	Water Surface, 0% imp, HSG C
0.017	80	>75% Grass cover, Good, HSG D
0.229	80	>75% Grass cover, Good, HSG D
0.157	80	>75% Grass cover, Good, HSG D
0.016	80	>75% Grass cover, Good, HSG D
0.554	84	Weighted Average
0.554		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.5	50	0.0500	0.15		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.2	60	0.3500	4.14		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
5.7	110	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 16S: DA 2G

Hydrograph



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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Subcatchment 17S: DA 2J

Runoff = 12.52 cfs @ 12.09 hrs, Volume= 0.918 af, Depth> 4.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
0.412	80	>75% Grass cover, Good, HSG D
0.061	98	Paved parking, HSG C
0.032	74	>75% Grass cover, Good, HSG C
0.140	98	Paved parking, HSG C
0.721	74	>75% Grass cover, Good, HSG C
* 0.184	98	Two single Family Houses and Paved Driveways
0.183	98	Paved parking, HSG C
0.524	70	Woods, Good, HSG C
0.029	74	>75% Grass cover, Good, HSG C
2.286	80	Weighted Average
1.718		75.15% Pervious Area
0.568		24.85% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.3	24	0.1000	0.17		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	26	0.0500	1.56		Sheet Flow, Paved/Gravel Smooth surfaces n= 0.011 P2= 3.37"
0.3	85	0.0824	4.62		Shallow Concentrated Flow, Gravel Unpaved Kv= 16.1 fps
0.7	105	0.1333	2.56		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
3.6	240	Total, Increased to minimum Tc = 6.0 min			

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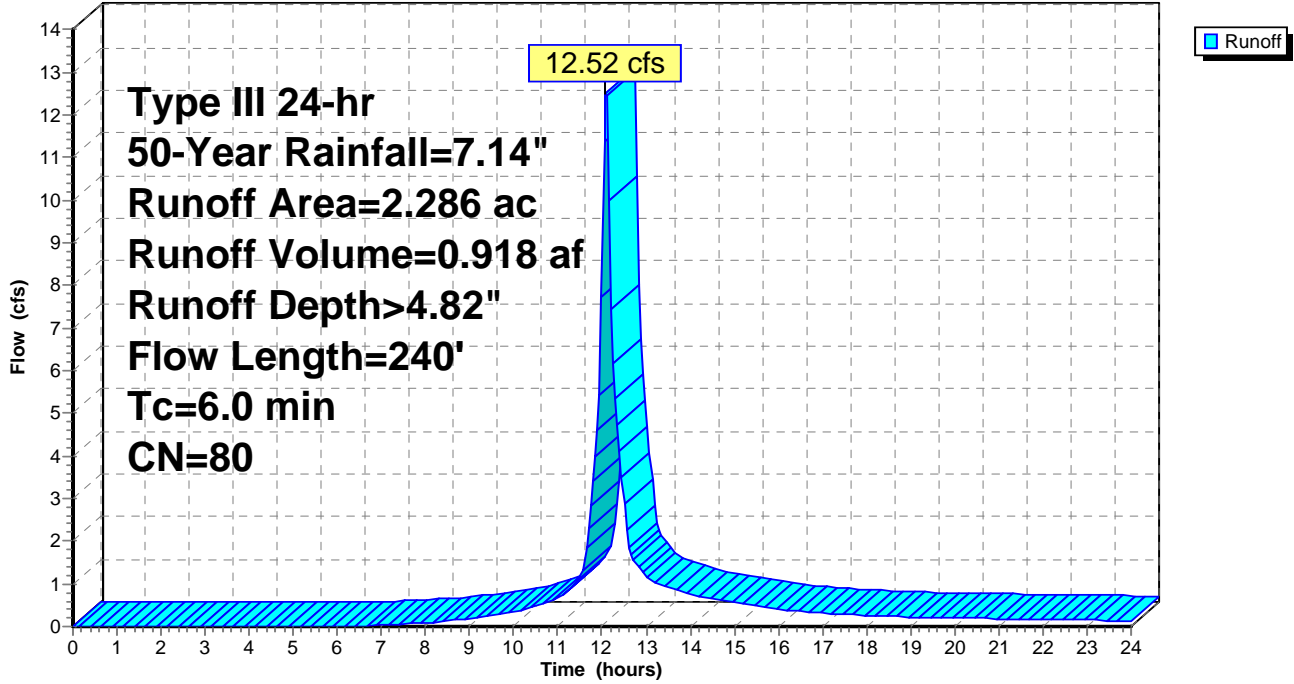
Type III 24-hr 50-Year Rainfall=7.14"

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Subcatchment 17S: DA 2J

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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Subcatchment 18S: DA 2I

Runoff = 3.04 cfs @ 12.15 hrs, Volume= 0.276 af, Depth> 6.18"

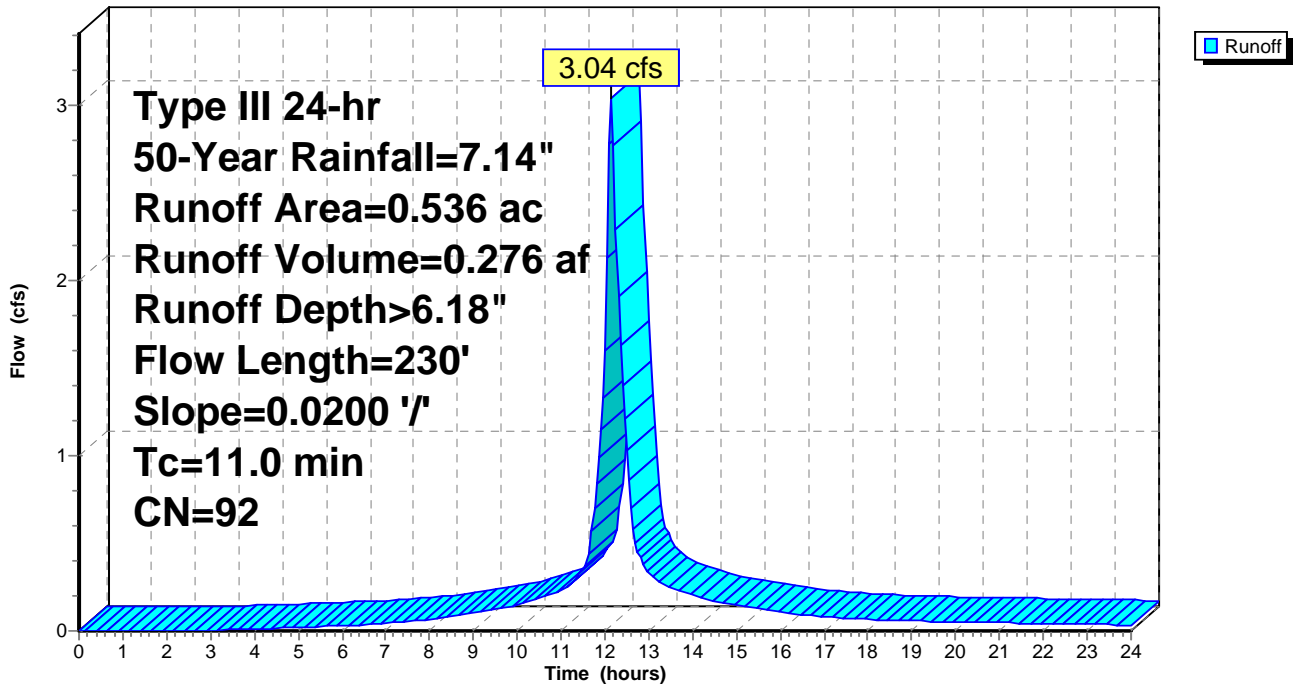
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
* 0.344	98	Paved parking, HSG C, North
0.192	80	>75% Grass cover, Good, HSG D
0.536	92	Weighted Average
0.192		35.82% Pervious Area
0.344		64.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0200	0.10		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
3.0	180	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
11.0	230	Total			

Subcatchment 18S: DA 2I

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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Subcatchment 21S: DA 2F

Runoff = 0.93 cfs @ 12.09 hrs, Volume= 0.070 af, Depth> 5.50"

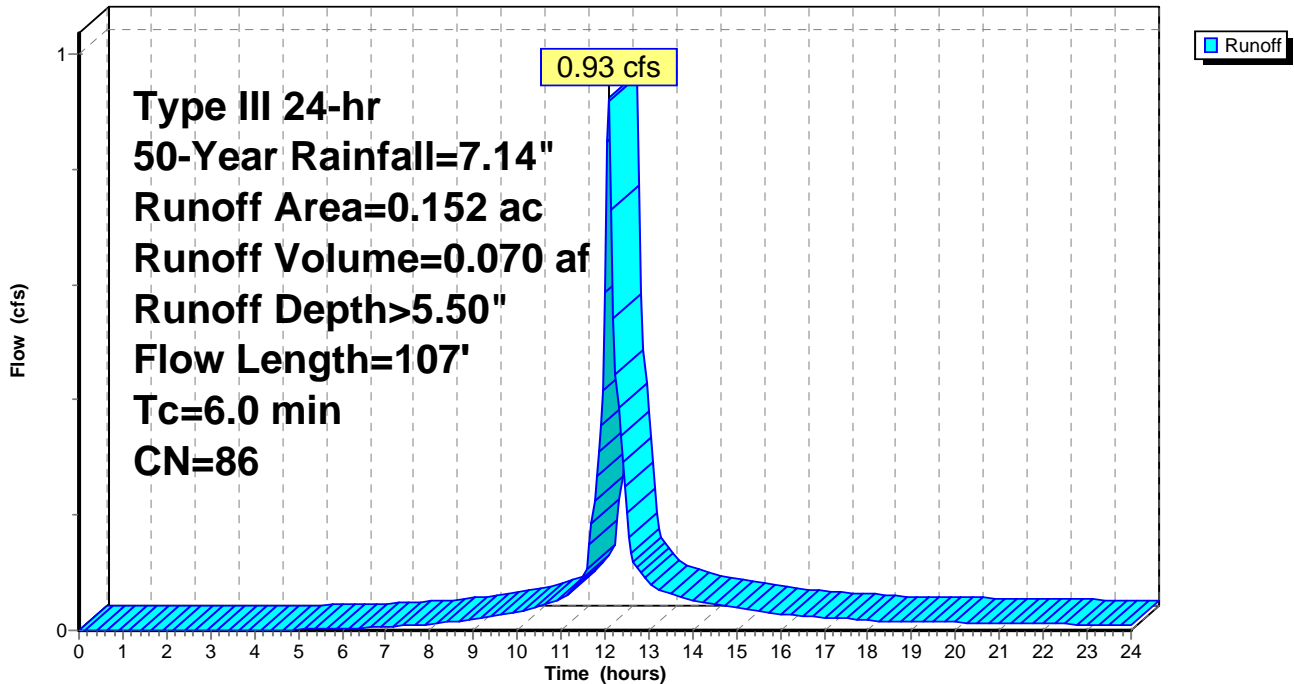
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
0.051	98	Water Surface, 0% imp, HSG C
0.101	80	>75% Grass cover, Good, HSG D
0.152	86	Weighted Average
0.152		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	50	0.1000	0.20		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	57	0.1754	2.93		Shallow Concentrated Flow, Woods Short Grass Pasture Kv= 7.0 fps
4.5	107	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 21S: DA 2F

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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Subcatchment 22S: DA 2H

Runoff = 14.32 cfs @ 12.14 hrs, Volume= 1.206 af, Depth> 5.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 50-Year Rainfall=7.14"

Area (ac)	CN	Description
* 0.431	98	Paved parking, HSG C, North
* 0.010	80	>75% Grass cover, Good, HSG D, North
0.313	80	>75% Grass cover, Good, HSG D
* 0.550	98	Paved parking, HSG C, South
0.360	80	>75% Grass cover, Good, HSG D
0.748	70	Woods, Good, HSG C
0.336	80	>75% Grass cover, Good, HSG D
2.748	84	Weighted Average
1.767		64.30% Pervious Area
0.981		35.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.3	50	0.1000	0.13		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
1.7	190	0.1316	1.81		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	81	0.3333	4.04		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
1.7	355	0.0310	3.57		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
10.0	676	Total			

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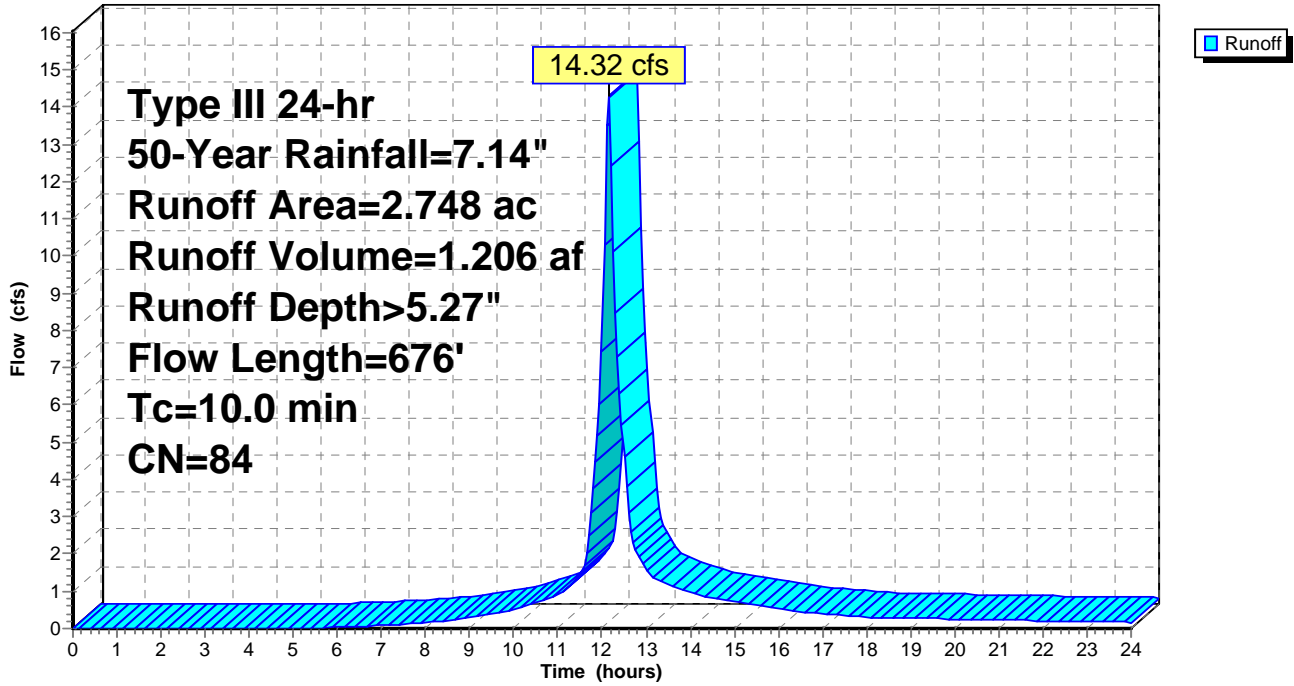
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Subcatchment 22S: DA 2H

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Summary for Pond 15P: Apartments Phase II Stormwater Basin 2

Inflow Area = 3.175 ac, 31.02% Impervious, Inflow Depth > 5.17" for 50-Year event
 Inflow = 15.36 cfs @ 12.16 hrs, Volume= 1.367 af
 Outflow = 13.37 cfs @ 12.23 hrs, Volume= 1.357 af, Atten= 13%, Lag= 4.1 min
 Primary = 13.37 cfs @ 12.23 hrs, Volume= 1.357 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 567.00' Surf.Area= 2,390 sf Storage= 1,777 cf
 Peak Elev= 569.20' @ 12.23 hrs Surf.Area= 3,486 sf Storage= 8,233 cf (6,456 cf above start)
 Flood Elev= 569.70' Surf.Area= 3,741 sf Storage= 10,022 cf (8,245 cf above start)

Plug-Flow detention time= 43.9 min calculated for 1.313 af (96% of inflow)
 Center-of-Mass det. time= 13.3 min (816.8 - 803.5)

Volume	Invert	Avail.Storage	Storage Description
#1	566.00'	11,168 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
566.00	1,164	0	0
567.00	2,390	1,777	1,777
568.00	2,867	2,629	4,406
570.00	3,895	6,762	11,168

Device	Routing	Invert	Outlet Devices
#1	Primary	566.00'	18.0" Round 18" HDPE L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 566.00' / 564.27' S= 0.0254 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	567.00'	6.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#3	Device 1	567.50'	12.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	568.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	569.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=13.30 cfs @ 12.23 hrs HW=569.19' TW=565.86' (Dynamic Tailwater)

- 1=18" HDPE (Inlet Controls 13.30 cfs @ 7.53 fps)
- 2=Orifice/Grate (Passes < 2.64 cfs potential flow)
- 3=Orifice/Grate (Passes < 4.13 cfs potential flow)
- 4=Orifice/Grate (Passes < 4.63 cfs potential flow)
- 5=Broad-Crested Rectangular Weir (Passes < 3.81 cfs potential flow)

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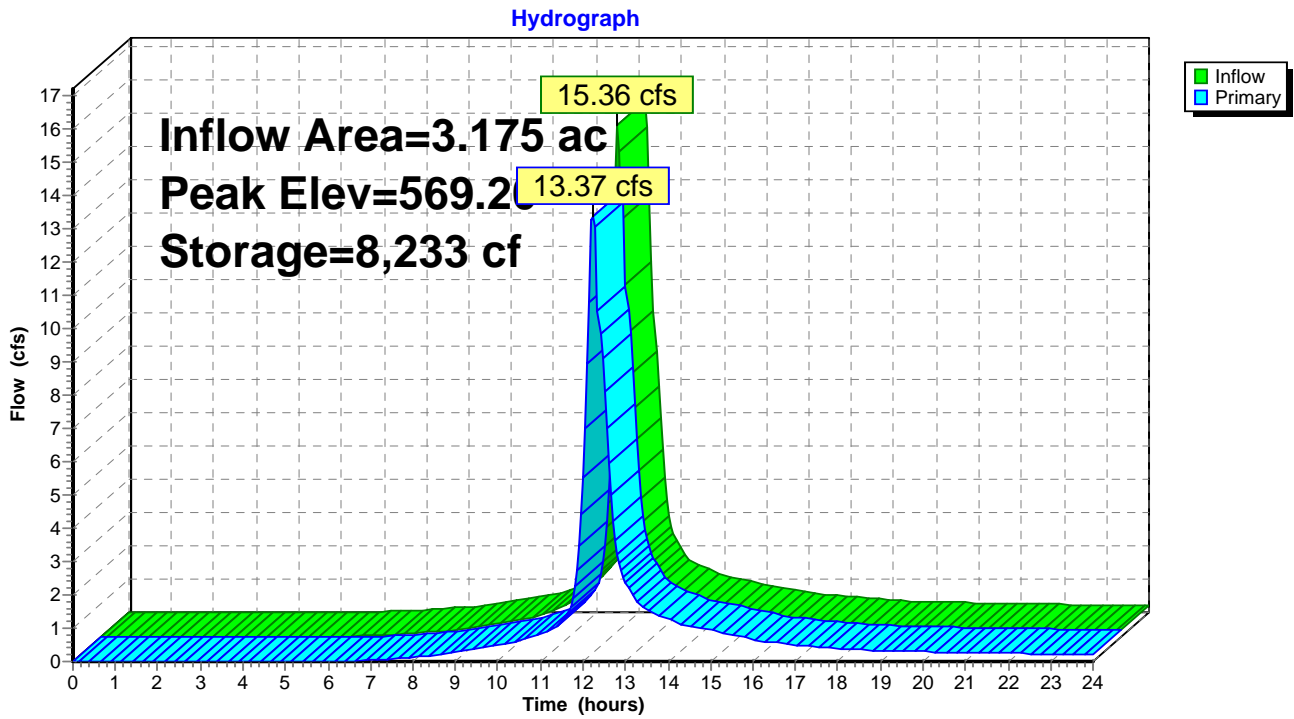
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Type III 24-hr 50-Year Rainfall=7.14"

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Pond 15P: Apartments Phase II Stormwater Basin 2



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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Pond 20P: Apartments Phase II Stormwater Basin 1

Inflow Area = 7.013 ac, 32.94% Impervious, Inflow Depth > 5.27" for 50-Year event
 Inflow = 30.88 cfs @ 12.17 hrs, Volume= 3.082 af
 Outflow = 17.22 cfs @ 12.44 hrs, Volume= 3.029 af, Atten= 44%, Lag= 16.0 min
 Primary = 17.22 cfs @ 12.44 hrs, Volume= 3.029 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 555.00' Surf.Area= 6,117 sf Storage= 5,401 cf
 Peak Elev= 558.85' @ 12.44 hrs Surf.Area= 10,428 sf Storage= 37,754 cf (32,353 cf above start)
 Flood Elev= 559.40' Surf.Area= 11,019 sf Storage= 43,681 cf (38,280 cf above start)

Plug-Flow detention time= 79.1 min calculated for 2.905 af (94% of inflow)
 Center-of-Mass det. time= 36.1 min (841.0 - 804.9)

Volume	Invert	Avail.Storage	Storage Description
#1	554.00'	50,485 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
554.00	4,686	0	0
556.00	7,547	12,233	12,233
558.00	9,522	17,069	29,302
560.00	11,661	21,183	50,485

Device	Routing	Invert	Outlet Devices
#1	Primary	554.00'	18.0" Round 18" HDPE L= 102.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 554.00' / 552.00' S= 0.0196 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	555.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	556.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	557.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	558.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=17.22 cfs @ 12.44 hrs HW=558.84' TW=0.00' (Dynamic Tailwater)

- 1=18" HDPE (Inlet Controls 17.22 cfs @ 9.74 fps)
- 2=Orifice/Grate (Passes < 4.86 cfs potential flow)
- 3=Orifice/Grate (Passes < 4.09 cfs potential flow)
- 4=Orifice/Grate (Passes < 6.27 cfs potential flow)
- 5=Broad-Crested Rectangular Weir (Passes < 40.97 cfs potential flow)

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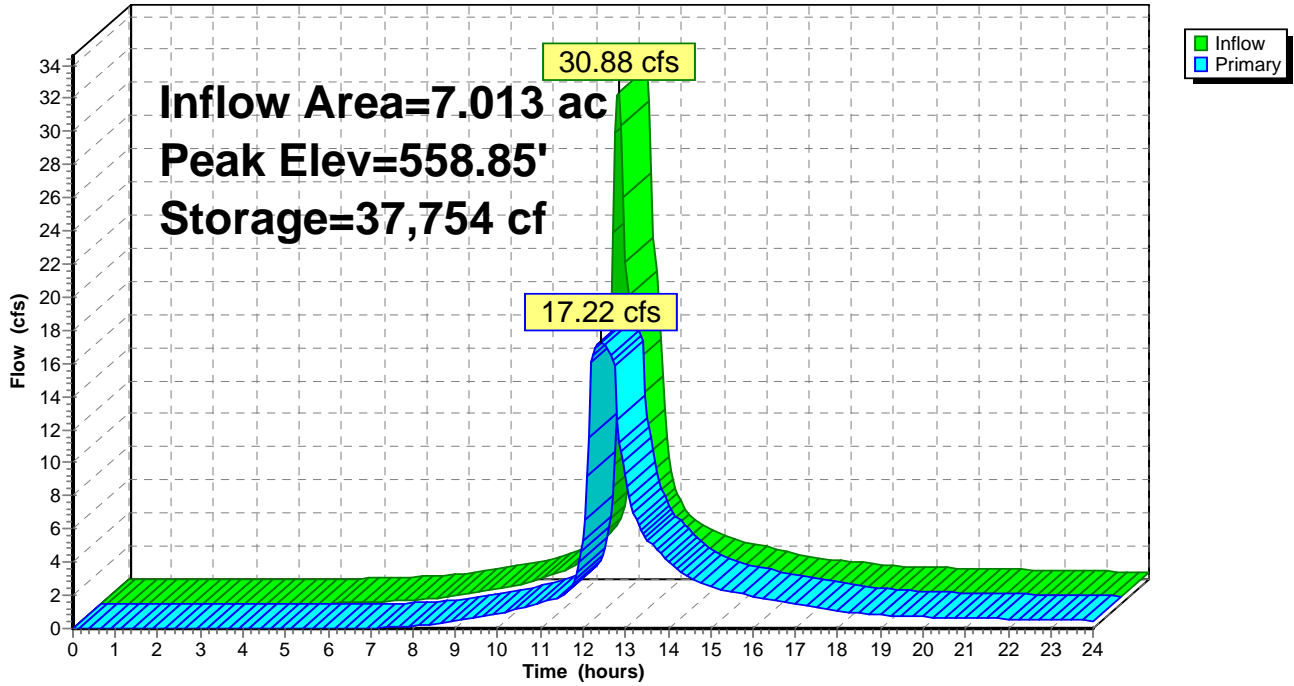
Type III 24-hr 50-Year Rainfall=7.14"

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Pond 20P: Apartments Phase II Stormwater Basin 1

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Summary for Pond 21P: DMH #2

Inflow Area = 3.711 ac, 35.81% Impervious, Inflow Depth > 5.28" for 50-Year event
 Inflow = 16.19 cfs @ 12.22 hrs, Volume= 1.633 af
 Outflow = 16.19 cfs @ 12.22 hrs, Volume= 1.633 af, Atten= 0%, Lag= 0.0 min
 Primary = 16.19 cfs @ 12.22 hrs, Volume= 1.633 af

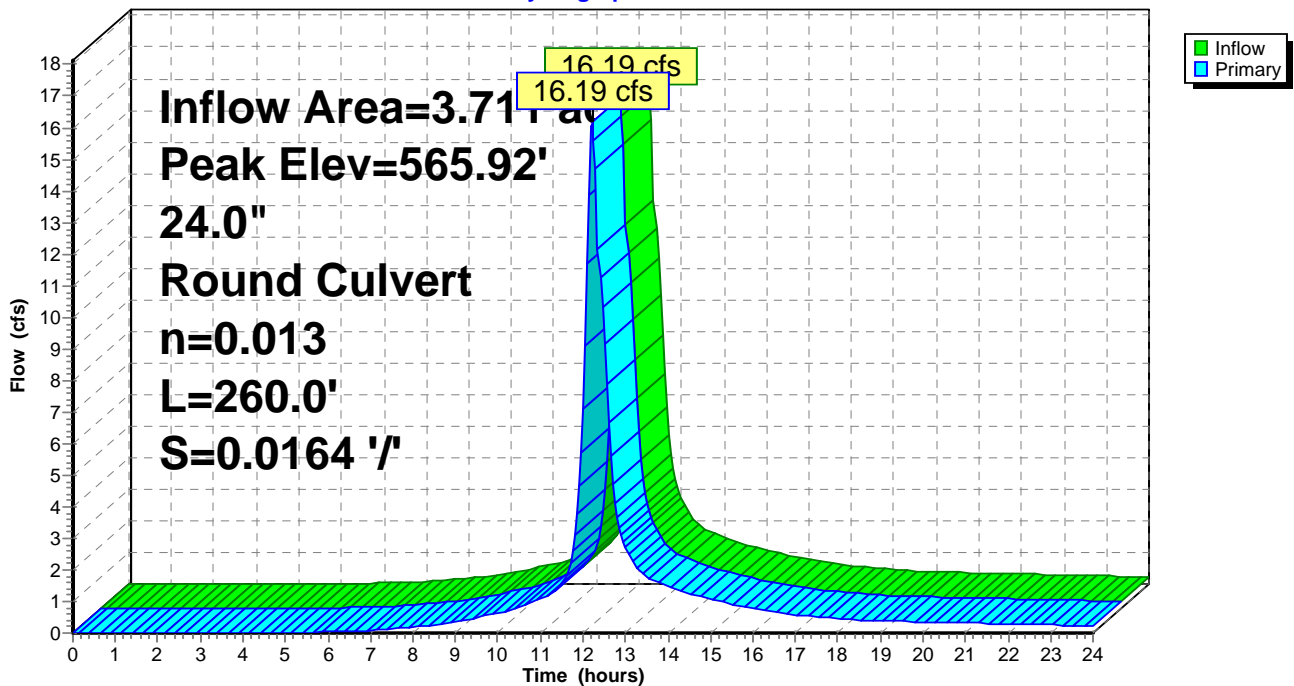
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 565.92' @ 12.22 hrs
 Flood Elev= 569.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	563.77'	24.0" Round Culvert L= 260.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 563.77' / 559.50' S= 0.0164 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=15.90 cfs @ 12.22 hrs HW=565.87' TW=559.21' (Dynamic Tailwater)
 ←1=Culvert (Inlet Controls 15.90 cfs @ 5.06 fps)

Pond 21P: DMH #2

Hydrograph



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Type III 24-hr 50-Year Rainfall=7.14"

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Summary for Pond 22P: FE #2A

Inflow Area = 6.459 ac, 35.76% Impervious, Inflow Depth > 5.27" for 50-Year event
 Inflow = 28.70 cfs @ 12.18 hrs, Volume= 2.839 af
 Outflow = 28.70 cfs @ 12.18 hrs, Volume= 2.839 af, Atten= 0%, Lag= 0.0 min
 Primary = 28.70 cfs @ 12.18 hrs, Volume= 2.839 af

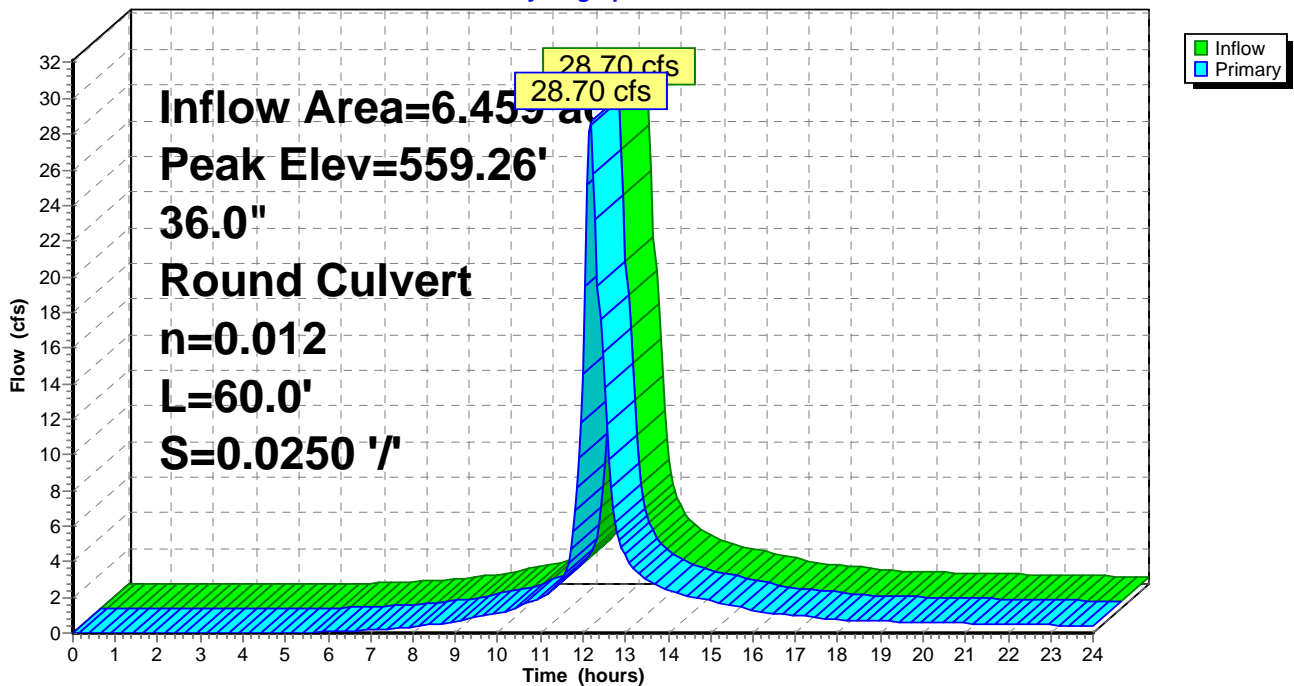
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Peak Elev= 559.26' @ 12.29 hrs
 Flood Elev= 564.47'

Device	Routing	Invert	Outlet Devices
#1	Primary	556.50'	36.0" Round Culvert L= 60.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 556.50' / 555.00' S= 0.0250 '/ Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 7.07 sf

Primary OutFlow Max=28.40 cfs @ 12.18 hrs HW=559.12' TW=558.19' (Dynamic Tailwater)
 ←1=Culvert (Outlet Controls 28.40 cfs @ 5.78 fps)

Pond 22P: FE #2A

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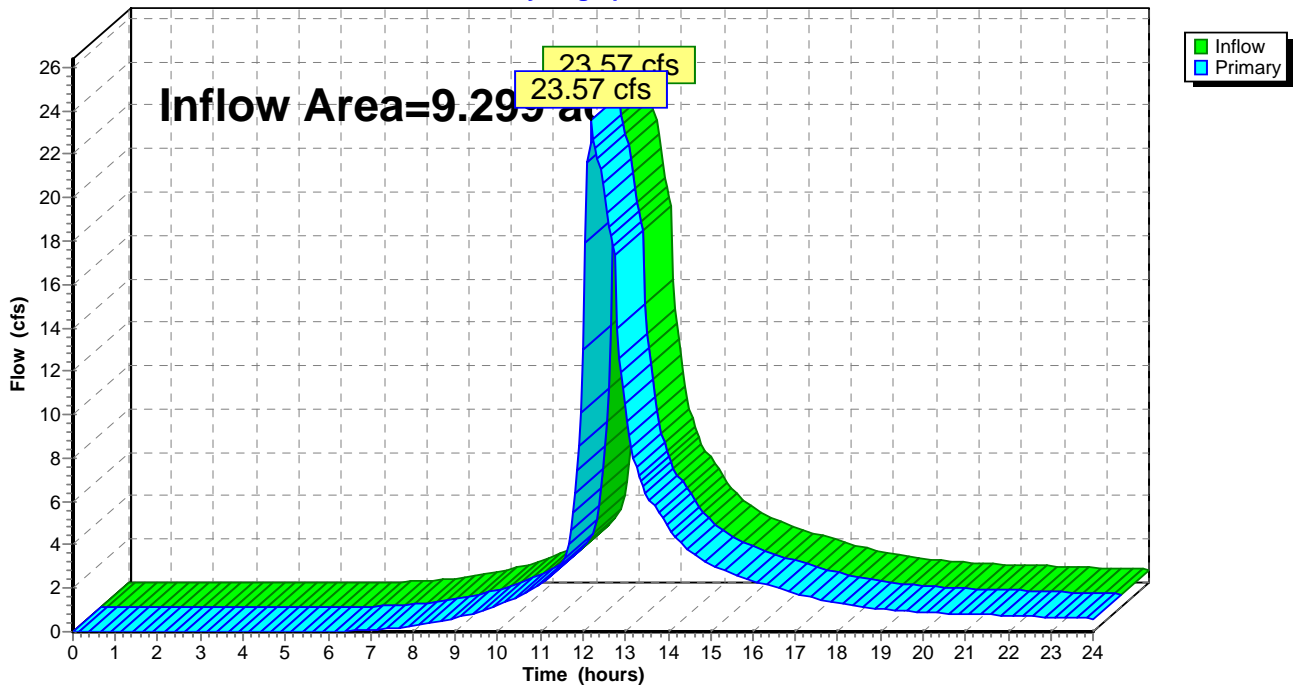
Summary for Link 20L: Off-Site

Inflow Area = 9.299 ac, 30.95% Impervious, Inflow Depth > 5.09" for 50-Year event
Inflow = 23.57 cfs @ 12.21 hrs, Volume= 3.947 af
Primary = 23.57 cfs @ 12.21 hrs, Volume= 3.947 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 20L: Off-Site

Hydrograph



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Type III 24-hr 100-Year Rainfall=8.04"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 2
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 15S: DA 2E Runoff Area=3.023 ac 32.58% Impervious Runoff Depth>6.00"
Flow Length=671' Tc=12.0 min CN=83 Runoff=17.00 cfs 1.513 af

Subcatchment 16S: DA 2G Runoff Area=0.554 ac 0.00% Impervious Runoff Depth>6.13"
Flow Length=110' Tc=6.0 min CN=84 Runoff=3.77 cfs 0.283 af

Subcatchment 17S: DA 2J Runoff Area=2.286 ac 24.85% Impervious Runoff Depth>5.66"
Flow Length=240' Tc=6.0 min CN=80 Runoff=14.61 cfs 1.078 af

Subcatchment 18S: DA 2I Runoff Area=0.536 ac 64.18% Impervious Runoff Depth>7.07"
Flow Length=230' Slope=0.0200 '/' Tc=11.0 min CN=92 Runoff=3.46 cfs 0.316 af

Subcatchment 21S: DA 2F Runoff Area=0.152 ac 0.00% Impervious Runoff Depth>6.37"
Flow Length=107' Tc=6.0 min CN=86 Runoff=1.06 cfs 0.081 af

Subcatchment 22S: DA 2H Runoff Area=2.748 ac 35.70% Impervious Runoff Depth>6.13"
Flow Length=676' Tc=10.0 min CN=84 Runoff=16.54 cfs 1.403 af

Pond 15P: Apartments Phase II Stormwater Peak Elev=569.50' Storage=9,270 cf Inflow=17.79 cfs 1.593 af
Outflow=14.10 cfs 1.582 af

Pond 20P: Apartments Phase II Peak Elev=559.41' Storage=43,789 cf Inflow=36.32 cfs 3.584 af
Outflow=18.37 cfs 3.527 af

Pond 21P: DMH #2 Peak Elev=566.04' Inflow=17.02 cfs 1.898 af
24.0" Round Culvert n=0.013 L=260.0' S=0.0164 '/' Outflow=17.02 cfs 1.898 af

Pond 22P: FE #2A Peak Elev=559.79' Inflow=33.44 cfs 3.301 af
36.0" Round Culvert n=0.012 L=60.0' S=0.0250 '/' Outflow=33.44 cfs 3.301 af

Link 20L: Off-Site Inflow=27.76 cfs 4.605 af
Primary=27.76 cfs 4.605 af

Total Runoff Area = 9.299 ac Runoff Volume = 4.673 af Average Runoff Depth = 6.03"
69.05% Pervious = 6.421 ac 30.95% Impervious = 2.878 ac

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Type III 24-hr 100-Year Rainfall=8.04"

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Summary for Subcatchment 15S: DA 2E

Runoff = 17.00 cfs @ 12.16 hrs, Volume= 1.513 af, Depth> 6.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
* 0.985	98	Paved parking, HSG C, South
0.455	80	>75% Grass cover, Good, HSG D
0.917	70	Woods, Good, HSG C
0.666	80	>75% Grass cover, Good, HSG D
3.023	83	Weighted Average
2.038		67.42% Pervious Area
0.985		32.58% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	50	0.0600	0.11		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
3.3	417	0.1799	2.12		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	40	0.1000	2.21		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
0.7	164	0.0421	4.17		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
12.0	671	Total			

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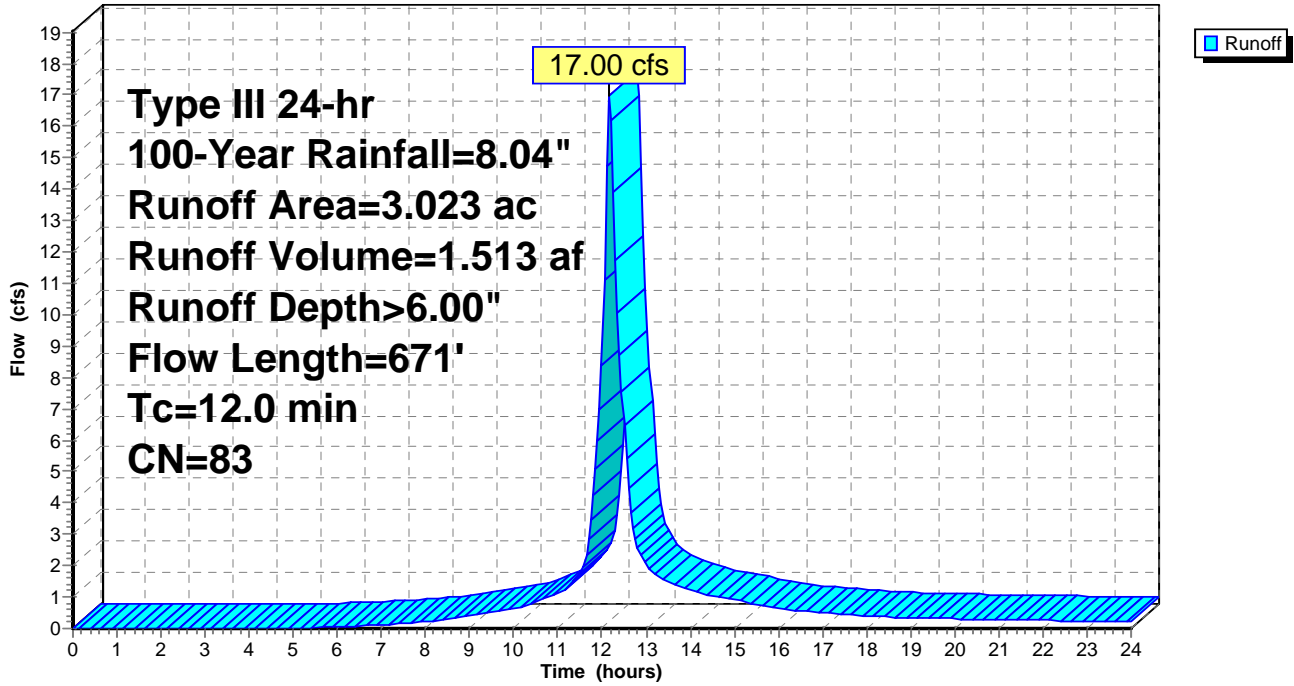
Type III 24-hr 100-Year Rainfall=8.04"

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Subcatchment 15S: DA 2E

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Type III 24-hr 100-Year Rainfall=8.04"

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Summary for Subcatchment 16S: DA 2G

Runoff = 3.77 cfs @ 12.09 hrs, Volume= 0.283 af, Depth> 6.13"

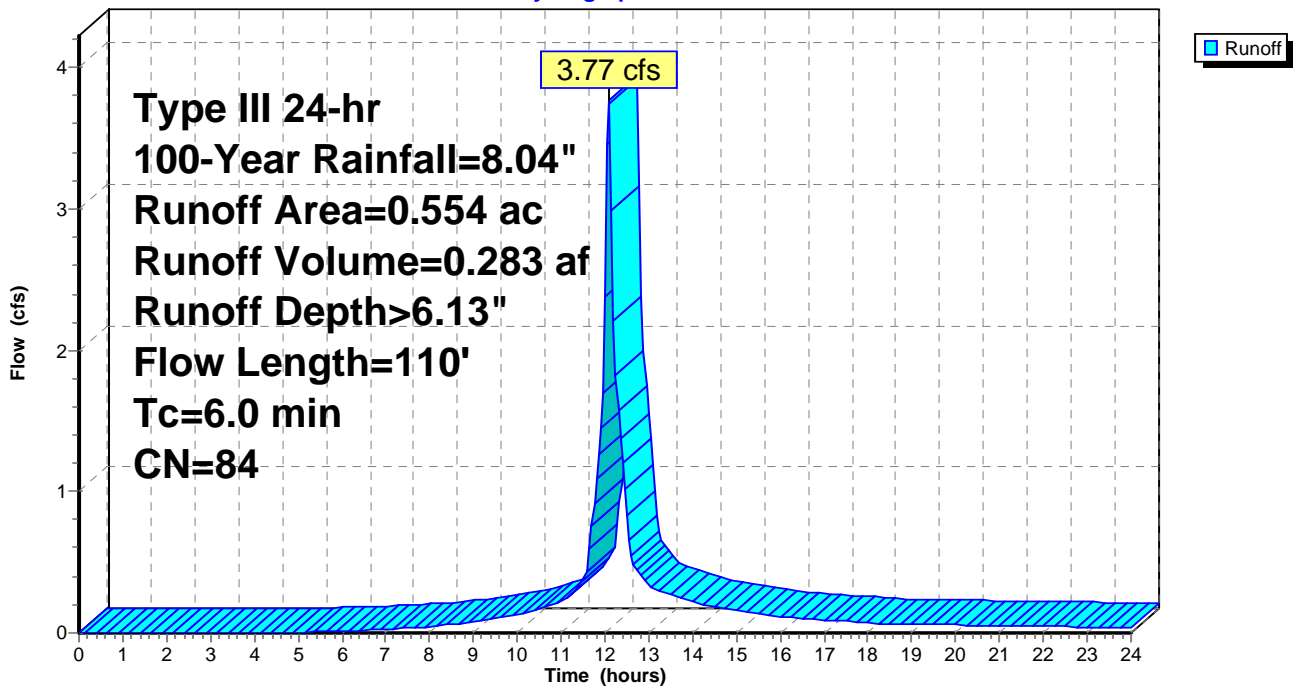
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
0.135	98	Water Surface, 0% imp, HSG C
0.017	80	>75% Grass cover, Good, HSG D
0.229	80	>75% Grass cover, Good, HSG D
0.157	80	>75% Grass cover, Good, HSG D
0.016	80	>75% Grass cover, Good, HSG D
0.554	84	Weighted Average
0.554		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.5	50	0.0500	0.15		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.2	60	0.3500	4.14		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
5.7	110	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 16S: DA 2G

Hydrograph



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Summary for Subcatchment 17S: DA 2J

Runoff = 14.61 cfs @ 12.09 hrs, Volume= 1.078 af, Depth> 5.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
0.412	80	>75% Grass cover, Good, HSG D
0.061	98	Paved parking, HSG C
0.032	74	>75% Grass cover, Good, HSG C
0.140	98	Paved parking, HSG C
0.721	74	>75% Grass cover, Good, HSG C
* 0.184	98	Two single Family Houses and Paved Driveways
0.183	98	Paved parking, HSG C
0.524	70	Woods, Good, HSG C
0.029	74	>75% Grass cover, Good, HSG C
2.286	80	Weighted Average
1.718		75.15% Pervious Area
0.568		24.85% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.3	24	0.1000	0.17		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	26	0.0500	1.56		Sheet Flow, Paved/Gravel Smooth surfaces n= 0.011 P2= 3.37"
0.3	85	0.0824	4.62		Shallow Concentrated Flow, Gravel Unpaved Kv= 16.1 fps
0.7	105	0.1333	2.56		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
3.6	240	Total, Increased to minimum Tc = 6.0 min			

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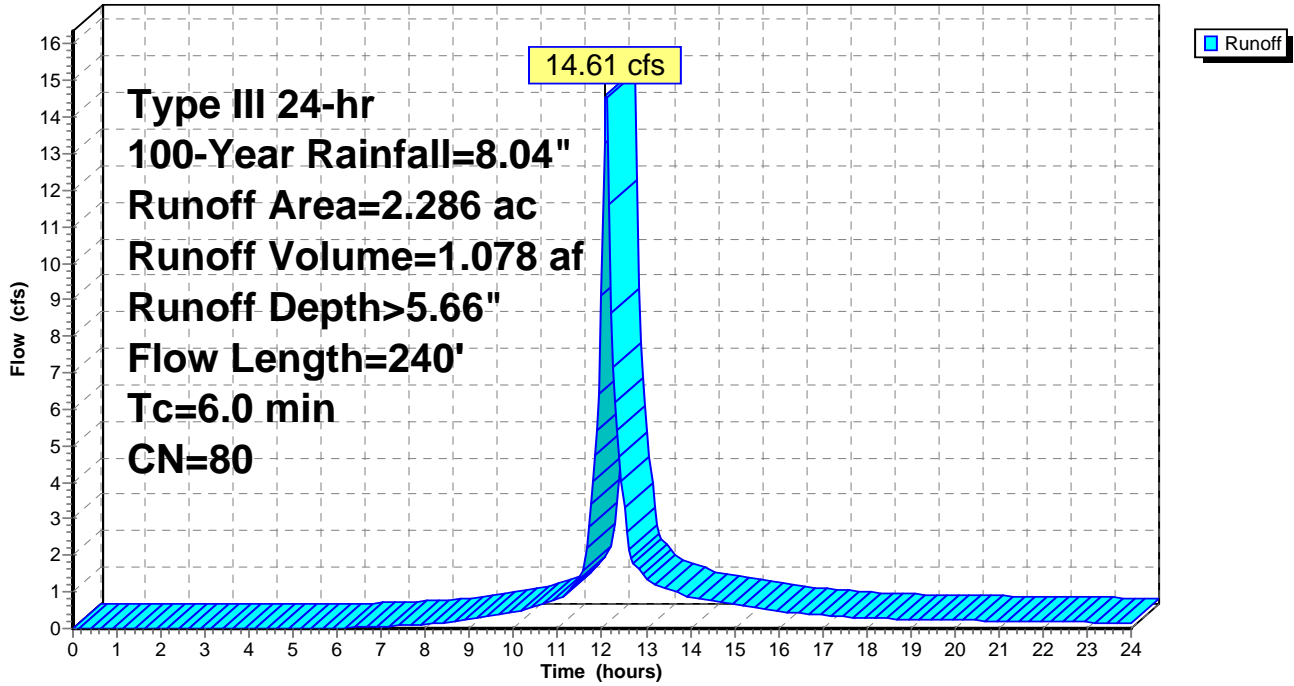
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Subcatchment 17S: DA 2J

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Summary for Subcatchment 18S: DA 2I

Runoff = 3.46 cfs @ 12.15 hrs, Volume= 0.316 af, Depth> 7.07"

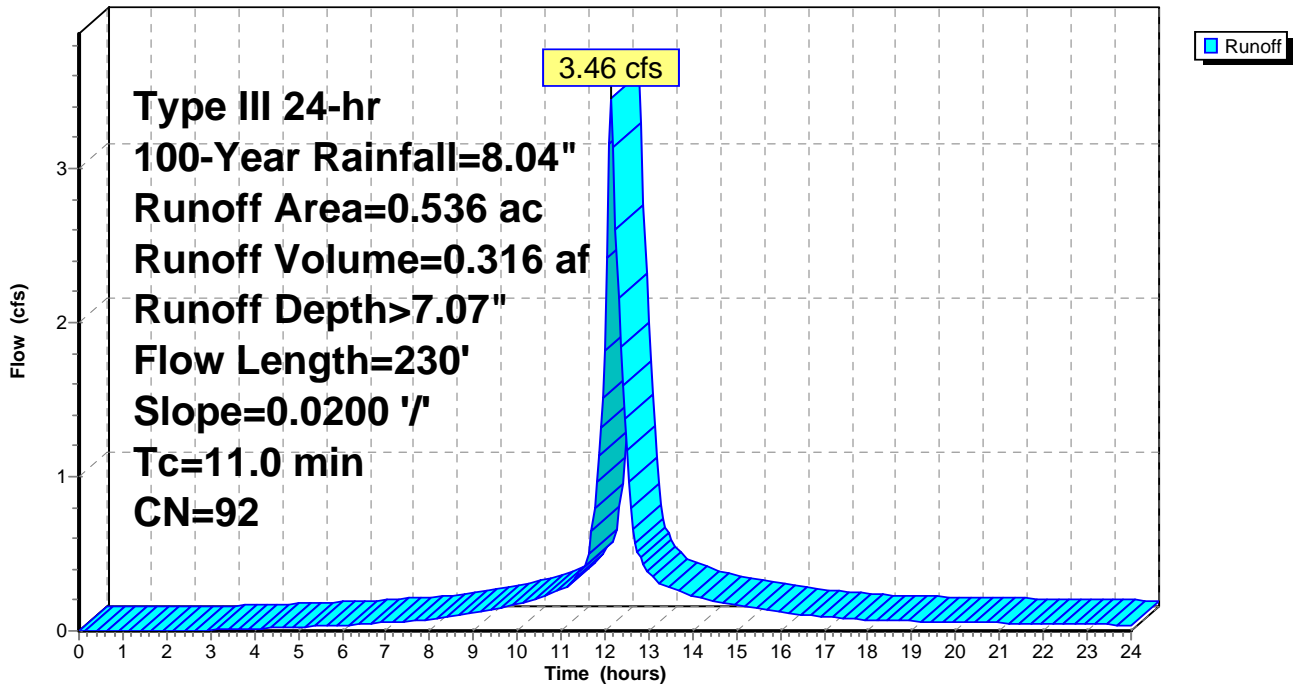
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
* 0.344	98	Paved parking, HSG C, North
0.192	80	>75% Grass cover, Good, HSG D
0.536	92	Weighted Average
0.192		35.82% Pervious Area
0.344		64.18% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.0	50	0.0200	0.10		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
3.0	180	0.0200	0.99		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
11.0	230	Total			

Subcatchment 18S: DA 2I

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Summary for Subcatchment 21S: DA 2F

Runoff = 1.06 cfs @ 12.09 hrs, Volume= 0.081 af, Depth> 6.37"

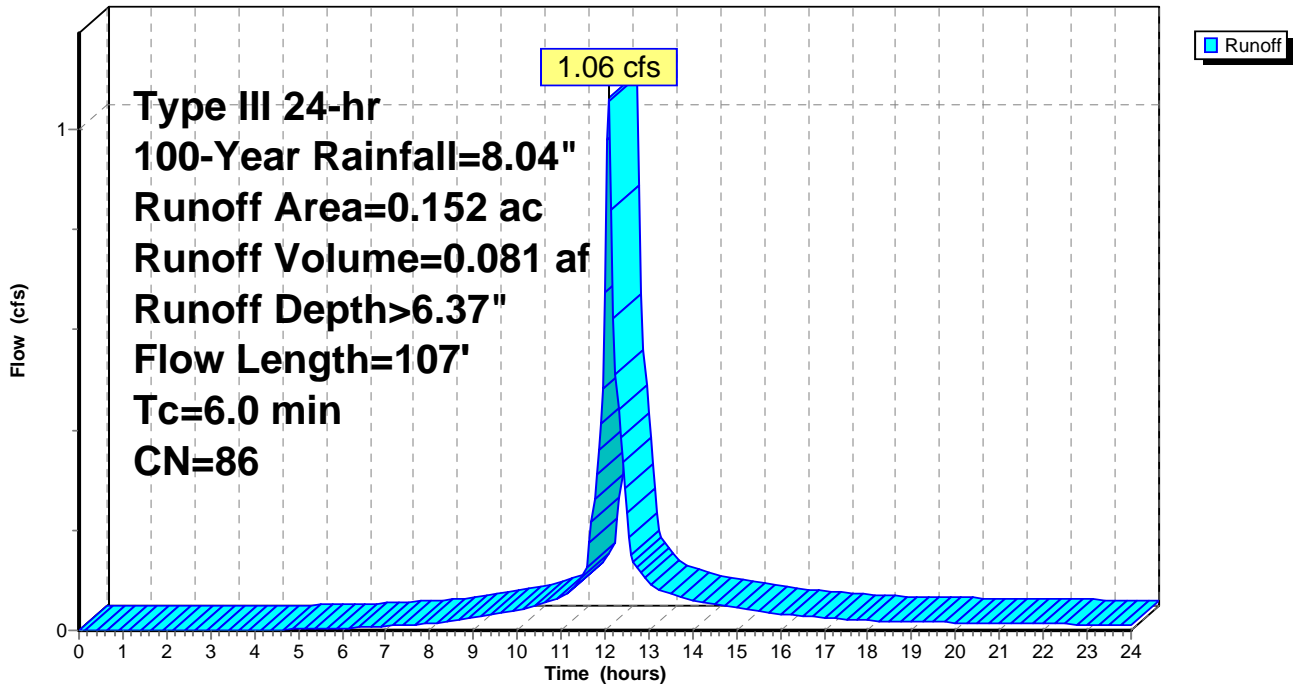
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
0.051	98	Water Surface, 0% imp, HSG C
0.101	80	>75% Grass cover, Good, HSG D
0.152	86	Weighted Average
0.152		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	50	0.1000	0.20		Sheet Flow, Grass Grass: Dense n= 0.240 P2= 3.37"
0.3	57	0.1754	2.93		Shallow Concentrated Flow, Woods Short Grass Pasture Kv= 7.0 fps
4.5	107	Total, Increased to minimum Tc = 6.0 min			

Subcatchment 21S: DA 2F

Hydrograph



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Type III 24-hr 100-Year Rainfall=8.04"

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Summary for Subcatchment 22S: DA 2H

Runoff = 16.54 cfs @ 12.14 hrs, Volume= 1.403 af, Depth> 6.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 100-Year Rainfall=8.04"

Area (ac)	CN	Description
* 0.431	98	Paved parking, HSG C, North
* 0.010	80	>75% Grass cover, Good, HSG D, North
0.313	80	>75% Grass cover, Good, HSG D
* 0.550	98	Paved parking, HSG C, South
0.360	80	>75% Grass cover, Good, HSG D
0.748	70	Woods, Good, HSG C
0.336	80	>75% Grass cover, Good, HSG D
2.748	84	Weighted Average
1.767		64.30% Pervious Area
0.981		35.70% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.3	50	0.1000	0.13		Sheet Flow, Woods Woods: Light underbrush n= 0.400 P2= 3.37"
1.7	190	0.1316	1.81		Shallow Concentrated Flow, Woods Woodland Kv= 5.0 fps
0.3	81	0.3333	4.04		Shallow Concentrated Flow, Grass Short Grass Pasture Kv= 7.0 fps
1.7	355	0.0310	3.57		Shallow Concentrated Flow, Paved Paved Kv= 20.3 fps
10.0	676	Total			

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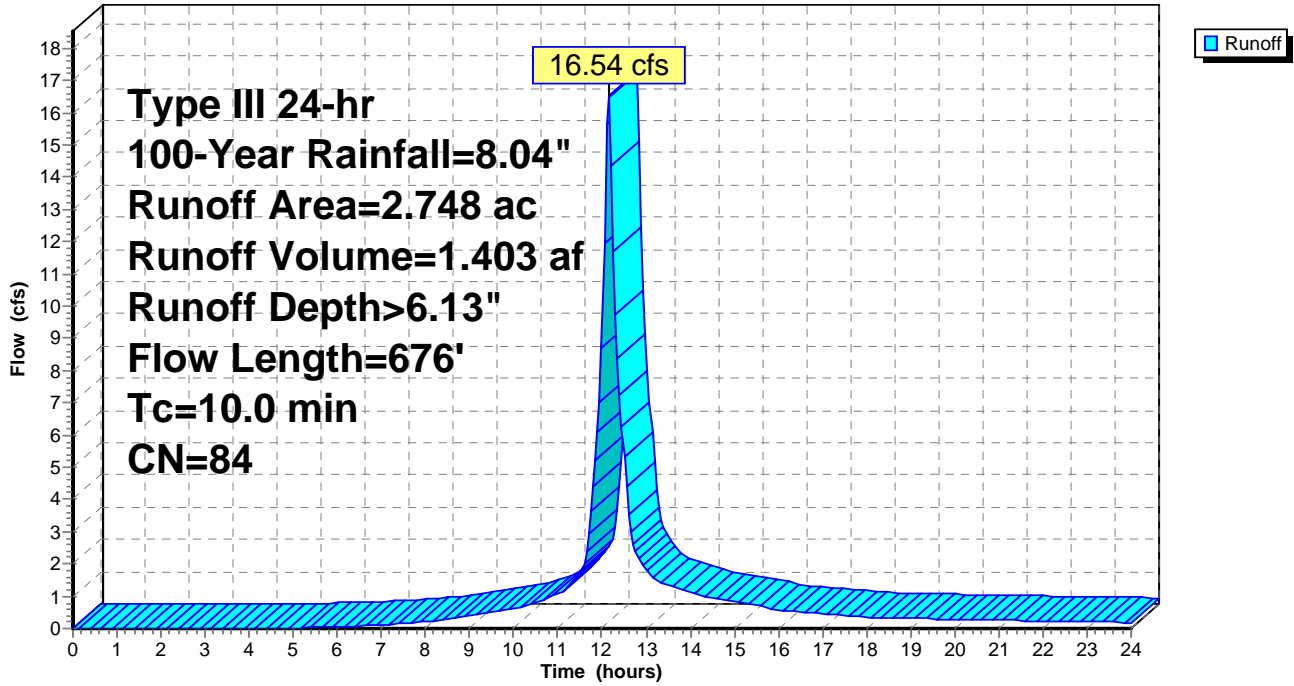
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Subcatchment 22S: DA 2H

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Summary for Pond 15P: Apartments Phase II Stormwater Basin 2

Inflow Area = 3.175 ac, 31.02% Impervious, Inflow Depth > 6.02" for 100-Year event
 Inflow = 17.79 cfs @ 12.16 hrs, Volume= 1.593 af
 Outflow = 14.10 cfs @ 12.26 hrs, Volume= 1.582 af, Atten= 21%, Lag= 6.0 min
 Primary = 14.10 cfs @ 12.26 hrs, Volume= 1.582 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 567.00' Surf.Area= 2,390 sf Storage= 1,777 cf
 Peak Elev= 569.50' @ 12.26 hrs Surf.Area= 3,636 sf Storage= 9,270 cf (7,493 cf above start)
 Flood Elev= 569.70' Surf.Area= 3,741 sf Storage= 10,022 cf (8,245 cf above start)

Plug-Flow detention time= 40.7 min calculated for 1.541 af (97% of inflow)
 Center-of-Mass det. time= 12.9 min (812.2 - 799.2)

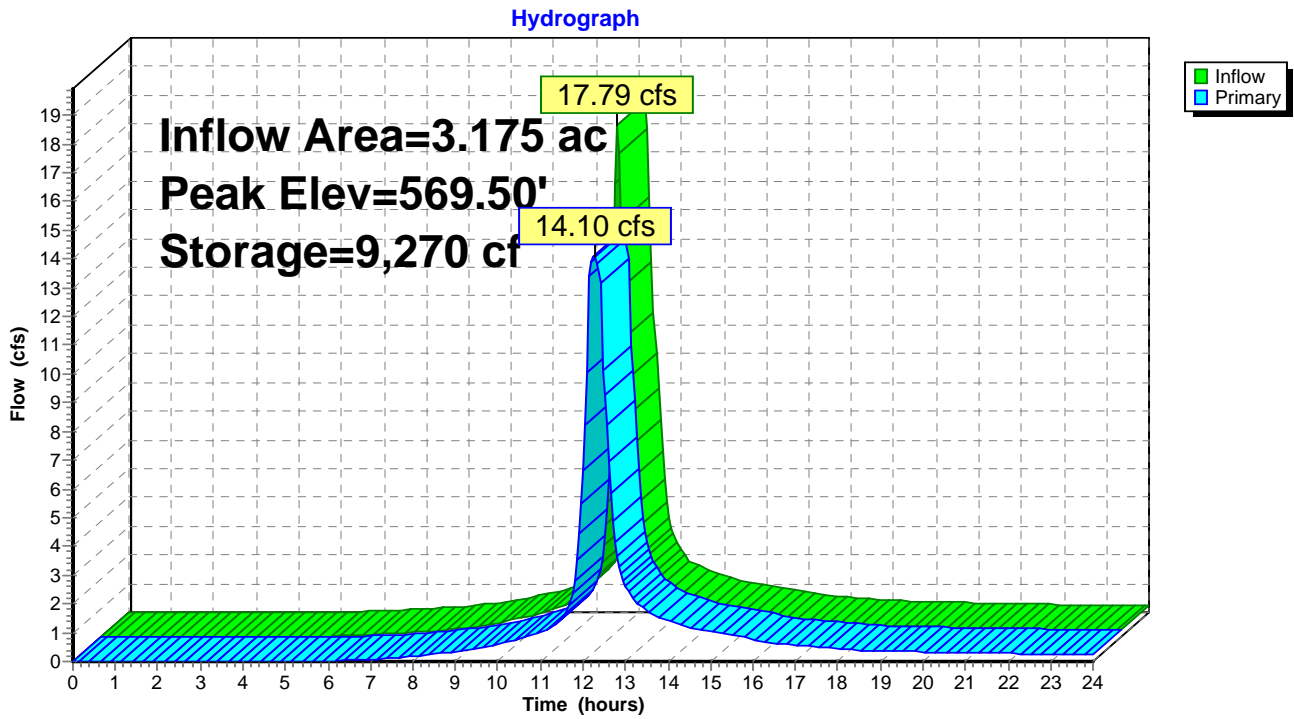
Volume	Invert	Avail.Storage	Storage Description
#1	566.00'	11,168 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
566.00	1,164	0	0
567.00	2,390	1,777	1,777
568.00	2,867	2,629	4,406
570.00	3,895	6,762	11,168

Device	Routing	Invert	Outlet Devices
#1	Primary	566.00'	18.0" Round 18" HDPE L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 566.00' / 564.27' S= 0.0254 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	567.00'	6.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#3	Device 1	567.50'	12.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	568.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	569.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=14.08 cfs @ 12.26 hrs HW=569.49' TW=565.97' (Dynamic Tailwater)

- 1=18" HDPE (Inlet Controls 14.08 cfs @ 7.97 fps)
- 2=Orifice/Grate (Passes < 2.83 cfs potential flow)
- 3=Orifice/Grate (Passes < 4.61 cfs potential flow)
- 4=Orifice/Grate (Passes < 5.43 cfs potential flow)
- 5=Broad-Crested Rectangular Weir (Passes < 16.25 cfs potential flow)

Pond 15P: Apartments Phase II Stormwater Basin 2



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Type III 24-hr 100-Year Rainfall=8.04"

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Summary for Pond 20P: Apartments Phase II Stormwater Basin 1

[58] Hint: Peaked 0.01' above defined flood level

Inflow Area = 7.013 ac, 32.94% Impervious, Inflow Depth > 6.13" for 100-Year event
 Inflow = 36.32 cfs @ 12.15 hrs, Volume= 3.584 af
 Outflow = 18.37 cfs @ 12.46 hrs, Volume= 3.527 af, Atten= 49%, Lag= 18.7 min
 Primary = 18.37 cfs @ 12.46 hrs, Volume= 3.527 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
 Starting Elev= 555.00' Surf.Area= 6,117 sf Storage= 5,401 cf
 Peak Elev= 559.41' @ 12.46 hrs Surf.Area= 11,030 sf Storage= 43,789 cf (38,388 cf above start)
 Flood Elev= 559.40' Surf.Area= 11,019 sf Storage= 43,681 cf (38,280 cf above start)

Plug-Flow detention time= 74.7 min calculated for 3.396 af (95% of inflow)
 Center-of-Mass det. time= 36.0 min (836.7 - 800.7)

Volume	Invert	Avail.Storage	Storage Description
#1	554.00'	50,485 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
554.00	4,686	0	0
556.00	7,547	12,233	12,233
558.00	9,522	17,069	29,302
560.00	11,661	21,183	50,485

Device	Routing	Invert	Outlet Devices
#1	Primary	554.00'	18.0" Round 18" HDPE L= 102.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 554.00' / 552.00' S= 0.0196 1/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	555.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	556.00'	10.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Device 1	557.00'	10.0" Vert. Orifice/Grate X 2.00 C= 0.600 Limited to weir flow at low heads
#5	Device 1	558.00'	16.0' long x 0.5' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=18.36 cfs @ 12.46 hrs HW=559.40' TW=0.00' (Dynamic Tailwater)

- 1=18" HDPE (Inlet Controls 18.36 cfs @ 10.39 fps)
- 2=Orifice/Grate (Passes < 5.24 cfs potential flow)
- 3=Orifice/Grate (Passes < 4.54 cfs potential flow)
- 4=Orifice/Grate (Passes < 7.40 cfs potential flow)
- 5=Broad-Crested Rectangular Weir (Passes < 88.39 cfs potential flow)

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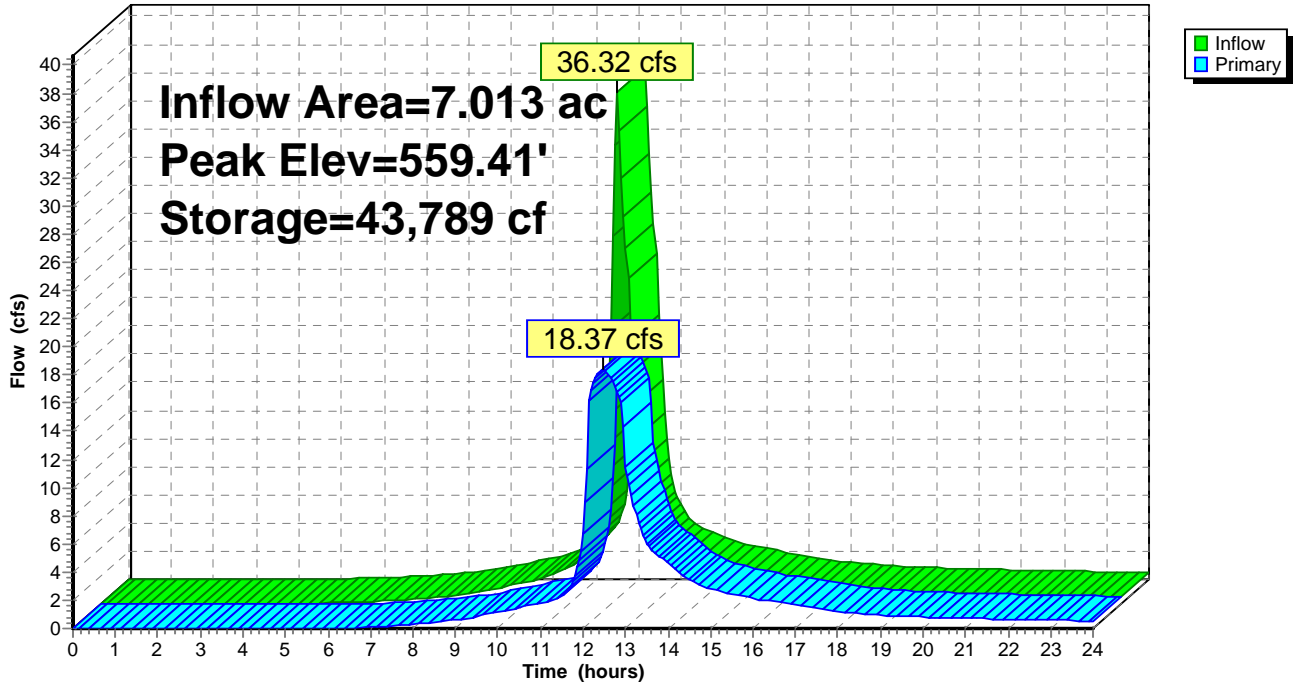
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Pond 20P: Apartments Phase II Stormwater Basin 1

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Summary for Pond 21P: DMH #2

Inflow Area = 3.711 ac, 35.81% Impervious, Inflow Depth > 6.14" for 100-Year event
Inflow = 17.02 cfs @ 12.19 hrs, Volume= 1.898 af
Outflow = 17.02 cfs @ 12.19 hrs, Volume= 1.898 af, Atten= 0%, Lag= 0.0 min
Primary = 17.02 cfs @ 12.19 hrs, Volume= 1.898 af

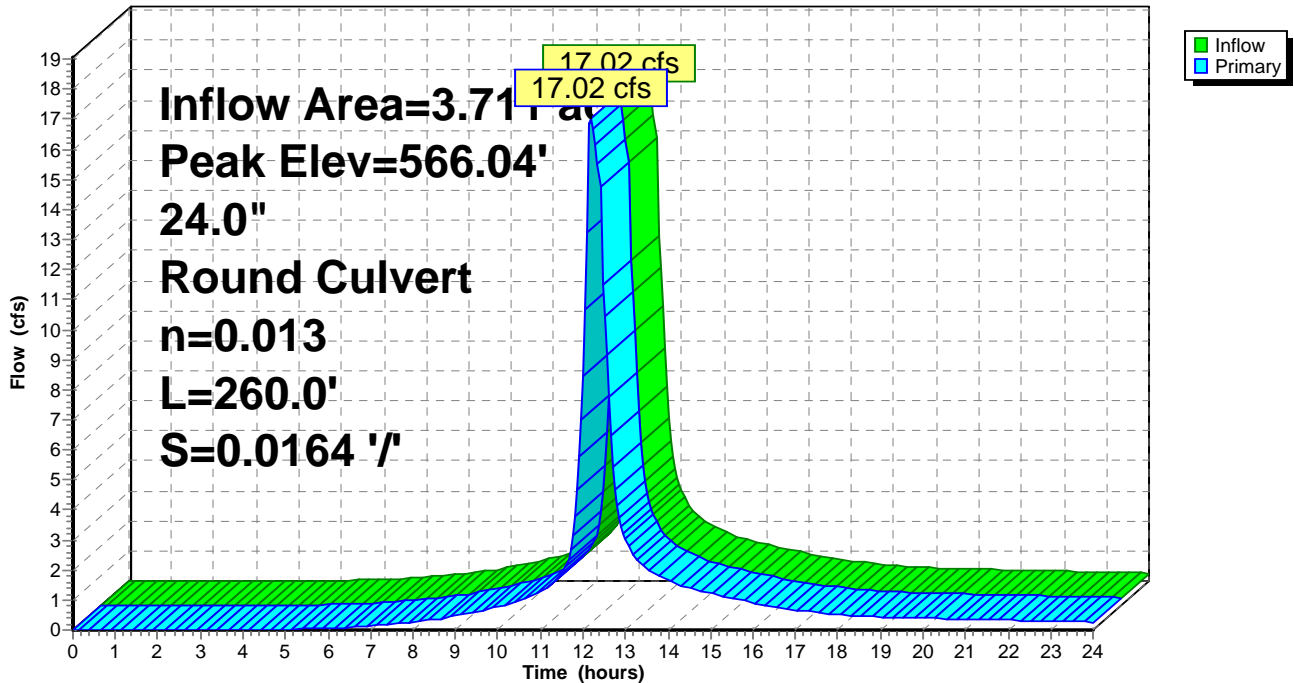
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 566.04' @ 12.19 hrs
Flood Elev= 569.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	563.77'	24.0" Round Culvert L= 260.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 563.77' / 559.50' S= 0.0164 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=16.99 cfs @ 12.19 hrs HW=566.03' TW=559.51' (Dynamic Tailwater)
↑**1=Culvert** (Inlet Controls 16.99 cfs @ 5.41 fps)

Pond 21P: DMH #2

Hydrograph



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Summary for Pond 22P: FE #2A

Inflow Area = 6.459 ac, 35.76% Impervious, Inflow Depth > 6.13" for 100-Year event
Inflow = 33.44 cfs @ 12.16 hrs, Volume= 3.301 af
Outflow = 33.44 cfs @ 12.16 hrs, Volume= 3.301 af, Atten= 0%, Lag= 0.0 min
Primary = 33.44 cfs @ 12.16 hrs, Volume= 3.301 af

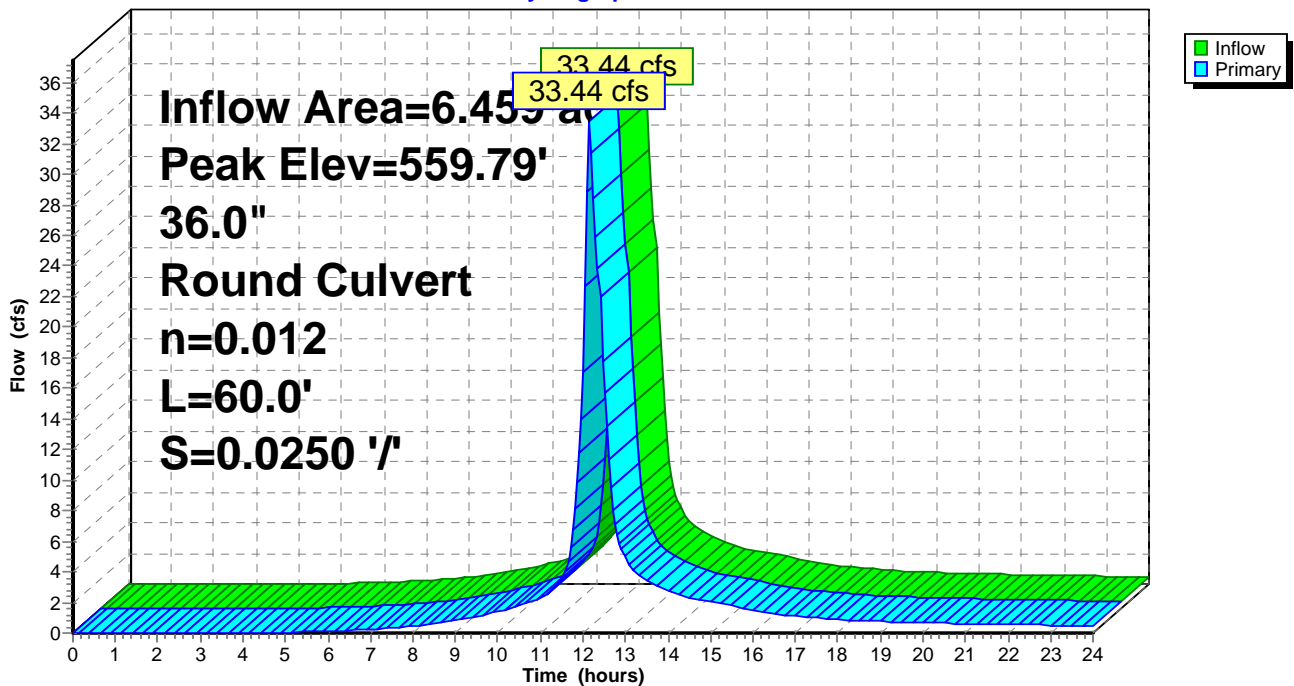
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 2
Peak Elev= 559.79' @ 12.38 hrs
Flood Elev= 564.47'

Device	Routing	Invert	Outlet Devices
#1	Primary	556.50'	36.0" Round Culvert L= 60.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 556.50' / 555.00' S= 0.0250 '/ Cc= 0.900 n= 0.012 Corrugated PP, smooth interior, Flow Area= 7.07 sf

Primary OutFlow Max=33.07 cfs @ 12.16 hrs HW=559.41' TW=558.41' (Dynamic Tailwater)
↑1=Culvert (Outlet Controls 33.07 cfs @ 6.00 fps)

Pond 22P: FE #2A

Hydrograph



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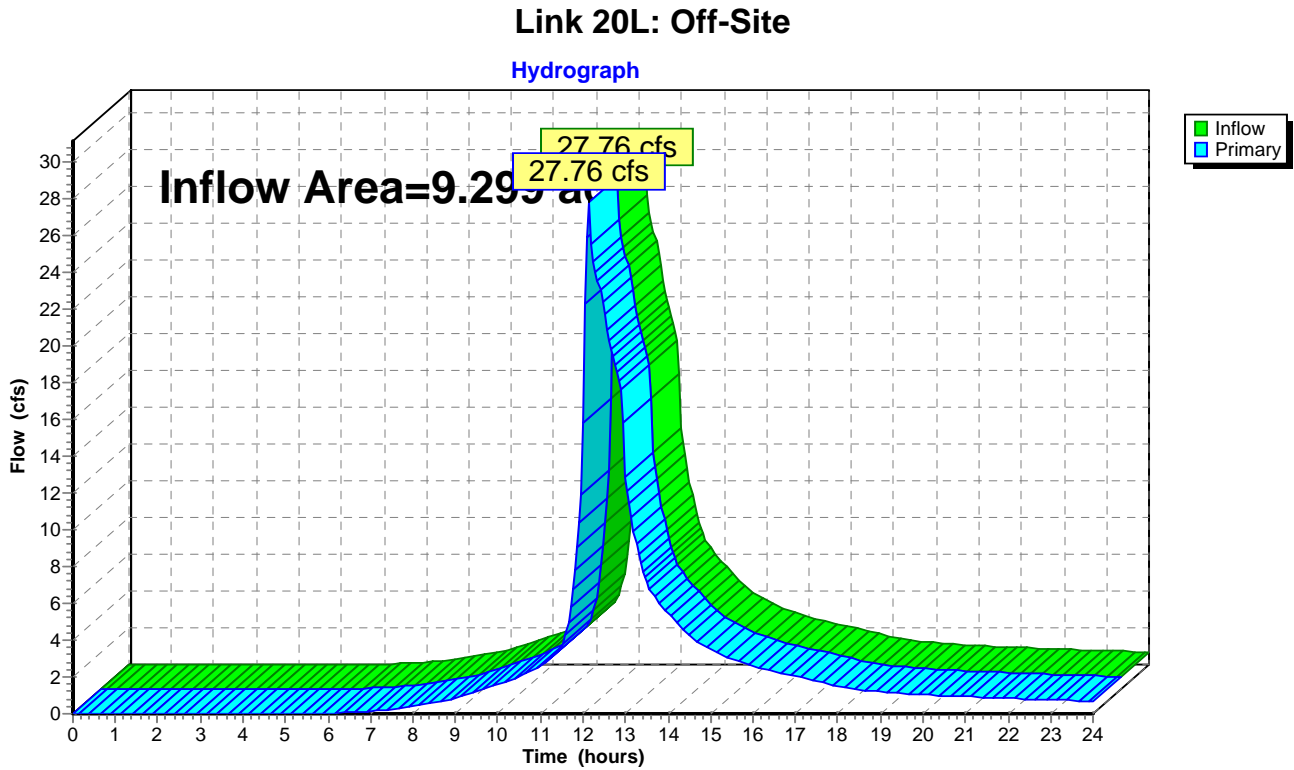
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Summary for Link 20L: Off-Site

Inflow Area = 9.299 ac, 30.95% Impervious, Inflow Depth > 5.94" for 100-Year event
Inflow = 27.76 cfs @ 12.15 hrs, Volume= 4.605 af
Primary = 27.76 cfs @ 12.15 hrs, Volume= 4.605 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs



Appendix C

Supporting Stormwater Calculations

Appendix C
Pipe Sizing Calculations

Manning's Equation for Open Channel Flow

$$Q = \frac{1.49}{n} AR^{2/3} S^{1/2}$$

Maximum pipe capacities for the trunk line drains are presented below as compared to the peak flow rates calculated using the Rational Method for the contributing watersheds or the HydroCAD modeling results as applicable. Pipes are sized with capacity for the 10-year design storm minimum in accordance with the recommendations of the CT DOT Drainage Manual for curb and gutter systems.

DMH 6 to DMH 2 (18-inch HDPE at S=0.015)

Q=	12.90 CFS	Flow Rate
n=	0.013	Roughness Coefficient
A=	1.77 SF	Area of Pipe
R=	0.375 FT	Hydraulic Radius = A/P
S=	0.015 FT/FT	Pipe Slope
r=	0.75 FT	Pipe Radius
P=	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	8.97 CFS
(10-year flow from DA 2H)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

DMH 7 to DMH-6 (18-inch HDPE at S=0.015)

Q=	12.90 CFS	Flow Rate
n=	0.013	Roughness Coefficient
A=	1.77 SF	Area of Pipe
R=	0.375 FT	Hydraulic Radius = A/P
S=	0.015 FT/FT	Pipe Slope
r=	0.75 FT	Pipe Radius
P=	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	8.97 CFS
(10-year flow from DA 2H)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 1 to DMH 7 (15-inch HDPE at S = 0.060)

Q=	15.87 CFS	Flow Rate
n=	0.013	Roughness Coefficient
A=	1.23 SF	Area of Pipe
R=	0.3125 FT	Hydraulic Radius = A/P
S=	0.06 FT/FT	Pipe Slope
r=	0.625 FT	Pipe Radius
P=	3.93 FT	Pipe Perimeter

Design Flow Rate

Q=	8.97 CFS
(10-year flow from DA 2H)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 2 to CB 1 (15-inch HDPE at S = 0.072)

Q=	17.38 CFS	Flow Rate
n=	0.013	Roughness Coefficient
A=	1.23 SF	Area of Pipe
R=	0.3125 FT	Hydraulic Radius = A/P
S=	0.072 FT/FT	Pipe Slope
r=	0.625 FT	Pipe Radius
P=	3.93 FT	Pipe Perimeter

Design Flow Rate

Q=	8.97 CFS
(10-year flow from DA 2H)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

Appendix C
Pipe Sizing Calculations

CB 3 to CB 2 (15-inch HDPE at S = 0.061)

Q= 16.00 CFS Flow Rate
n= 0.013 Roughness Coefficient
A= 1.23 SF Area of Pipe
R= 0.3125 FT Hydraulic Radius = *A*/*P*
S= 0.061 FT/FT Pipe Slope
r= 0.625 FT Pipe Radius
P= 3.93 FT Pipe Perimeter

Design Flow Rate

Q= 9.42 CFS

(10-year flow from DA 2H)

CAPACITY FOR 10-YEAR EVENT (MIN)

CB 4 to CB 3 (15-inch HDPE at S = 0.013)

Q= 7.39 CFS Flow Rate
n= 0.013 Roughness Coefficient
A= 1.23 SF Area of Pipe
R= 0.3125 FT Hydraulic Radius = *A*/*P*
S= 0.013 FT/FT Pipe Slope
r= 0.625 FT Pipe Radius
P= 3.93 FT Pipe Perimeter

Design Flow Rate

C_f= 1

C= 0.95

I= 5.42 in/hour

A= 0.16 acre

Q= 0.8 CFS

CAPACITY FOR 10-YEAR EVENT (MIN)

CB 5 to CB 3 (15-inch HDPE at S = 0.059)

Q= 15.73 CFS Flow Rate
n= 0.013 Roughness Coefficient
A= 1.23 SF Area of Pipe
R= 0.3125 FT Hydraulic Radius = *A*/*P*
S= 0.059 FT/FT Pipe Slope
r= 0.625 FT Pipe Radius
P= 3.93 FT Pipe Perimeter

Design Flow Rate

Q= 9.42 CFS

(10-year flow from DA 2H)

CAPACITY FOR 10-YEAR EVENT (MIN)

CB 6 to CB 5 (15-inch HDPE at S = 0.025)

Q= 10.24 CFS Flow Rate
n= 0.013 Roughness Coefficient
A= 1.23 SF Area of Pipe
R= 0.3125 FT Hydraulic Radius = *A*/*P*
S= 0.025 FT/FT Pipe Slope
r= 0.625 FT Pipe Radius
P= 3.93 FT Pipe Perimeter

Design Flow Rate

Q= 9.42 CFS

(10-year flow from DA 2H)

CAPACITY FOR 10-YEAR EVENT (MIN)

CB 7 to CB 6 (15-inch HDPE at S = 0.037)

Q= 12.46 CFS Flow Rate
n= 0.013 Roughness Coefficient
A= 1.23 SF Area of Pipe
R= 0.3125 FT Hydraulic Radius = *A*/*P*
S= 0.037 FT/FT Pipe Slope
r= 0.625 FT Pipe Radius
P= 3.93 FT Pipe Perimeter

Design Flow Rate

Q= 9.42 CFS

(10-year flow from DA 2H)

CAPACITY FOR 10-YEAR EVENT (MIN)

Appendix C
Pipe Sizing Calculations

CB 8 to DMH 5 (15-inch HDPE at S = 0.074)

Q=	17.62 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.23 SF	Area of Pipe
<i>R</i> =	0.3125 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.074 FT/FT	Pipe Slope
<i>r</i> =	0.625 FT	Pipe Radius
<i>P</i> =	3.93 FT	Pipe Perimeter

Design Flow Rate

Q=	2.02 CFS
(10-year flow from DA 2I)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 9 to CB 8 (15-inch HDPE at S = 0.020)

Q=	9.16 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.23 SF	Area of Pipe
<i>R</i> =	0.3125 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.02 FT/FT	Pipe Slope
<i>r</i> =	0.625 FT	Pipe Radius
<i>P</i> =	3.93 FT	Pipe Perimeter

Design Flow Rate

Q=	2.02 CFS
(10-year flow from DA 2I)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

DMH 8 to Outlet (18-inch HDPE at S = 0.023)

Q=	15.97 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.77 SF	Area of Pipe
<i>R</i> =	0.375 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.023 FT/FT	Pipe Slope
<i>r</i> =	0.75 FT	Pipe Radius
<i>P</i> =	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	9.16 CFS
(10-year flow from DA 2E)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 10 to DMH 8 (18-inch HDPE at S = 0.019)

Q=	14.52 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.77 SF	Area of Pipe
<i>R</i> =	0.375 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.019 FT/FT	Pipe Slope
<i>r</i> =	0.75 FT	Pipe Radius
<i>P</i> =	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	9.16 CFS
(10-year flow from DA 2E)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 11 to CB 10 (18-inch HDPE at S = 0.027)

Q=	17.31 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.77 SF	Area of Pipe
<i>R</i> =	0.375 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.027 FT/FT	Pipe Slope
<i>r</i> =	0.75 FT	Pipe Radius
<i>P</i> =	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	9.16 CFS
(10-year flow from DA 2E)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

Appendix C
Pipe Sizing Calculations

CB 12 to CB 11 (18-inch HDPE at S = 0.010)

Q=	10.53 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.77 SF	Area of Pipe
<i>R</i> =	0.375 FT	Hydraulic Radius = A/P
<i>S</i> =	0.01 FT/FT	Pipe Slope
<i>r</i> =	0.75 FT	Pipe Radius
<i>P</i> =	4.71 FT	Pipe Perimeter

Design Flow Rate

Q=	9.16 CFS
(10-year flow from DA 2E)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 13 to CB 12 (15-inch HDPE at S = 0.014)

Q=	7.66 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.23 SF	Area of Pipe
<i>R</i> =	0.3125 FT	Hydraulic Radius = A/P
<i>S</i> =	0.014 FT/FT	Pipe Slope
<i>r</i> =	0.625 FT	Pipe Radius
<i>P</i> =	3.93 FT	Pipe Perimeter

Design Flow Rate

<i>C_f</i> =	1
<i>C</i> =	0.95
<i>I</i> =	5.42 in/hour
<i>A</i> =	0.44 acre
Q=	2.3 CFS
CAPACITY FOR 10-YEAR EVENT (MIN)	

CB 14 to CB 13 (15-inch HDPE at S = 0.009)

Q=	6.14 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	1.23 SF	Area of Pipe
<i>R</i> =	0.3125 FT	Hydraulic Radius = A/P
<i>S</i> =	0.009 FT/FT	Pipe Slope
<i>r</i> =	0.625 FT	Pipe Radius
<i>P</i> =	3.93 FT	Pipe Perimeter

Design Flow Rate

<i>C_f</i> =	1
<i>C</i> =	0.95
<i>I</i> =	5.42 in/hour
<i>A</i> =	0.44 acre
Q=	2.3 CFS
CAPACITY FOR 10-YEAR EVENT (MIN)	

DMH 3 to DMH 2 (24-inch HDPE at S = 0.012)

Q=	24.85 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	3.14 SF	Area of Pipe
<i>R</i> =	0.5 FT	Hydraulic Radius = A/P
<i>S</i> =	0.012 FT/FT	Pipe Slope
<i>r</i> =	1 FT	Pipe Radius
<i>P</i> =	6.28 FT	Pipe Perimeter

Design Flow Rate

Q=	11.05 CFS
(10-year flow from DA 2I and Stormwater Basin 2)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

DMH 4 to DMH 3 (24-inch HDPE at S = 0.016)

Q=	28.69 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	3.14 SF	Area of Pipe
<i>R</i> =	0.5 FT	Hydraulic Radius = A/P
<i>S</i> =	0.016 FT/FT	Pipe Slope
<i>r</i> =	1 FT	Pipe Radius
<i>P</i> =	6.28 FT	Pipe Perimeter

Design Flow Rate

Q=	11.05 CFS
(10-year flow from DA 2I and Stormwater Basin 2)	
CAPACITY FOR 10-YEAR EVENT (MIN)	

Appendix C
Pipe Sizing Calculations

DMH 5 to DMH 4 (24-inch HDPE at S = 0.016)

Q=	28.69 CFS	Flow Rate
<i>n</i> =	0.013	Roughness Coefficient
<i>A</i> =	3.14 SF	Area of Pipe
<i>R</i> =	0.5 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.016 FT/FT	Pipe Slope
<i>r</i> =	1 FT	Pipe Radius
<i>P</i> =	6.28 FT	Pipe Perimeter

Design Flow Rate

Q=	11.05 CFS
(10-year flow from DA 2I and Stormwater Basin 2)	

CAPACITY FOR 10-YEAR EVENT (MIN)

Roof Drainage* (8-inch PVC at S = 0.02 minimum)

Q=	1.97 CFS	Flow Rate
<i>n</i> =	0.011	Roughness Coefficient
<i>A</i> =	0.34 SF	Area of Pipe
<i>R</i> =	0.165 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.02 FT/FT	Pipe Slope
<i>r</i> =	0.33 FT	Pipe Radius
<i>P</i> =	2.07 FT	Pipe Perimeter

Design Flow Rate

<i>C_f</i> =	1
<i>C</i> =	0.95
<i>I</i> =	5.42 in/hour
<i>A</i> =	0.318 acre
Q=	1.6 CFS

**CAPACITY FOR 10-YEAR EVENT (MIN)
FOR TWO BUILDINGS**

Roof Drainage* (8-inch PVC at S = 0.01 minimum)

Q=	1.39 CFS	Flow Rate
<i>n</i> =	0.011	Roughness Coefficient
<i>A</i> =	0.34 SF	Area of Pipe
<i>R</i> =	0.165 FT	Hydraulic Radius = <i>A</i> / <i>P</i>
<i>S</i> =	0.01 FT/FT	Pipe Slope
<i>r</i> =	0.33 FT	Pipe Radius
<i>P</i> =	2.07 FT	Pipe Perimeter

Design Flow Rate

<i>C_f</i> =	1
<i>C</i> =	0.95
<i>I</i> =	5.42 in/hour
<i>A</i> =	0.159 acre
Q=	0.8 CFS

**CAPACITY FOR 10-YEAR EVENT (MIN)
FOR ONE BUILDING**

**2015 International Plumbing Code specifies a rainfall intensity of 2.75 inches/hour for roof drain sizing. Proposed sizing is conservative.*

Appendix C

Rip Rap Apron Sizing Calculations

Per 2002 CT DEEP Soil Erosion and Sediment Control Guidelines

Stormwater Basin 1 Inlet

Q= 24.3 CFS 25-year storm
D= 36.00 in Pipe Diameter
 $L_a = 31.93$ FT Length of Apron = $(1.7Q/D^{(3/2)})+8D$
W= 21.8 FT Width = $3D+0.4L_a$
Width at Pipe End = 6 FT

$D_{50} = 0.27$ FT $D_{50} = (0.02/TW)*(Q/D)^{(4/3)}$
Use modified riprap TW=0.4D

Stormwater Basin 2 Inlet

Q= 13.1 CFS 25-year storm
D= 18.00 in Pipe Diameter
 $L_a = 24.11$ FT Length of Apron = $(1.7Q/D^{(3/2)})+8D$
W= 14.1 FT Width = $3D+0.4L_a$
Width at Pipe End = 3 FT

$D_{50} = 0.60$ FT $D_{50} = (0.02/TW)*(Q/D)^{(4/3)}$
Use modified riprap TW=0.4D

Appendix C

Water Quality Volume Calculations

Water Quality Volume - Apartments Phase 2

$$WQV = (1")(R)(A)/12$$

WQV = Water Quality Volume (acre-feet)

$$R = \text{Runoff Co-Efficient} = 0.005 + 0.009(I)$$

I = Impervious Area (%)

A = Site Area (acres)

Water Quality Volume for Contributing Area to Stormwater Basin 1 (DA 2E, DA 2F, DA 2G, 2H, DA 2I)

IA= 2.31 acres

I = 33.00 %

R = 0.30

A = 7.00 acres

WQV = 0.18 acre-feet

= **7,673.84 cubic feet**

Sediment Forebay Volume

Bottom Area = 155 SF

Top Area = 975 SF

Depth = 4 FT

Volume = 2,260 CF

% Stored = 29.45%

Constructed Stormwater Wetlands Volume

Bottom Area = 4,688 SF

Top Area = 6,655 SF

Depth = 1 FT

Volume = 5,672 CF

% Stored = 73.91%

Retention Provided = 7,932 CF

% Provided = 103.36%

Appendix C

Water Quality Volume Calculations

Water Quality Volume for Contributing Area to Stormwater Basin 2 (DA 2E and DA 2F)

IA= 0.99 acres

I = 30.03 %

R = 0.28

A = 3.28 acres

WQV = 0.08 acre-feet

= **3,277.53 cubic feet**

Sediment Forebay Volume

Bottom Area = 36 SF

Top Area = 722 SF

Depth = 4 FT

Volume = 1,516 CF

% Stored = 46.25%

Constructed Stormwater Wetlands Volume

Bottom Area = 1,164 SF

Top Area = 2,390 SF

Depth = 1 FT

Volume = 1,777 CF

% Stored = 54.22%

Retention Provided = 3,293 CF

% Provided = 100.47%

Appendix C

Groundwater Recharge Volume Calculations

Groundwater Recharge Volume - Apartments Phase 2

$$GRV = (D)(A)(I)/12$$

GRV = Groundwater Recharge Volume (acre-feet)

D = Depth of runoff to be recharged (inches)

A = Site Area (acres)

I = Post-development site imperviousness

D= 0.10 inches HSG C (Table 7-4 of the DEEP Water Quality Manual)

A = 7.00 acres

IA = 2.55 acres

I = 0.36

GRV = 0.02 acre-feet

= **925.65** cubic feet

Appendix C

Temporary Sediment Trap Sizing Calculations

Temporary Sediment Traps sized for 134 cubic yards of storage per acre of contributing area.

Temporary Sediment Trap 1

Contributing area =	2.4 acres
Required storage =	322 cubic yards
	8,683 cubic feet
Bottom of excavation =	549.00
Emergency spillway =	553.00
Storage provided =	8,994 cubic feet
	138.80 cubic yards per acre

Temporary Sediment Trap 2

Contributing area =	3.34 acres
Required storage =	448 cubic yards
	12,084 cubic feet
Bottom of excavation =	558.00
Emergency spillway =	562.00
Storage provided =	13,280 cubic feet
	147.26 cubic yards per acre

Temporary Sediment Trap 3

Contributing area =	0.25 acres
Required storage =	34 cubic yards
	905 cubic feet
Bottom of excavation =	558.00
Emergency spillway =	561.00
Storage provided =	1,037 cubic feet
	153.63 cubic yards per acre



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<http://www.trinkausengineering.com>

January 9, 2021

Pollutant loading analysis:

A pollutant renovation analysis was done for the two proposed stormwater basins to demonstrate the reductions in non-point source runoff which will be achieved by the two extended detention shallow wetland systems.

The Scheuler Equation was used to calculate the pollutant loads for the Water Quality Storm Event (1"/24-hours) for Total Suspended Solids (TSS), Total Nitrogen (TN), Total Phosphorous (TP), Zinc (Zn), Total Petroleum Hydrocarbons (TPH), and Dissolved Inorganic Nitrogen (DIN) for the proposed apartment complex.

Table #1 shows the loads which will be directed to Basin #2 (upper basin) and how is directed to Basin #1. Table #2 shows the reductions for Basin #1 for those areas which are not first directed to Basin #2. Table #3 shows the total reduction in non-point source pollutants from the proposed development.

In the tables below, loads are shown in pounds per the water quality rainfall event.

Table #1 – Basin #2

Pollutant	Load	Load Removed	Remaining Load directed to Basin #1
TSS	12.81	8.84	3.97
TN	0.45	0.25	0.197
TP	0.064	0.025	0.039
Zn	0.046	0.02	0.025
TPH	0.32	0.144	0.176
DIN	0.069	0.024	0.044

Table #2 – Basin #1

Pollutant	Load	Load Removed
TSS	16.825	11.609
TN	0.589	0.329
TP	0.084	0.032
Zn	0.061	0.027
TPH	0.420	0.189
DIN	0.090	0.032

Table #3 – Total Pollutant Load Reductions

Pollutant	Total Load	Total Load Removed	Total Percent Removed
TSS	29.644	23.196	78.2
TN	1.037	0.691	66.6
TP	0.148	0.073	49.3
Zn	0.108	0.056	55.7
TPH	0.741	0.413	55.7
DIN	0.160	0.072	44.8

Conclusion:

The proposed stormwater management system will significantly reduce non-point source pollutants from the proposed development which will ultimately reach Lake Pocotopaug. This analysis did not consider the TSS trapping ability in a standard catch basin sump of 5%, so it is a conservative analysis. The pollutant removal efficiencies will increase over time as the wetland plants become fully established in the two stormwater basins.

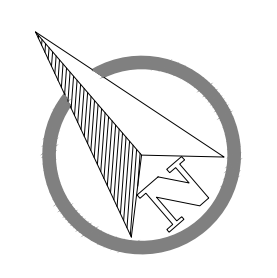
Respectfully Submitted,
Trinkaus Engineering, LLC



Steven Trinkaus, PE

Appendix D

Proposed Site Development Plans

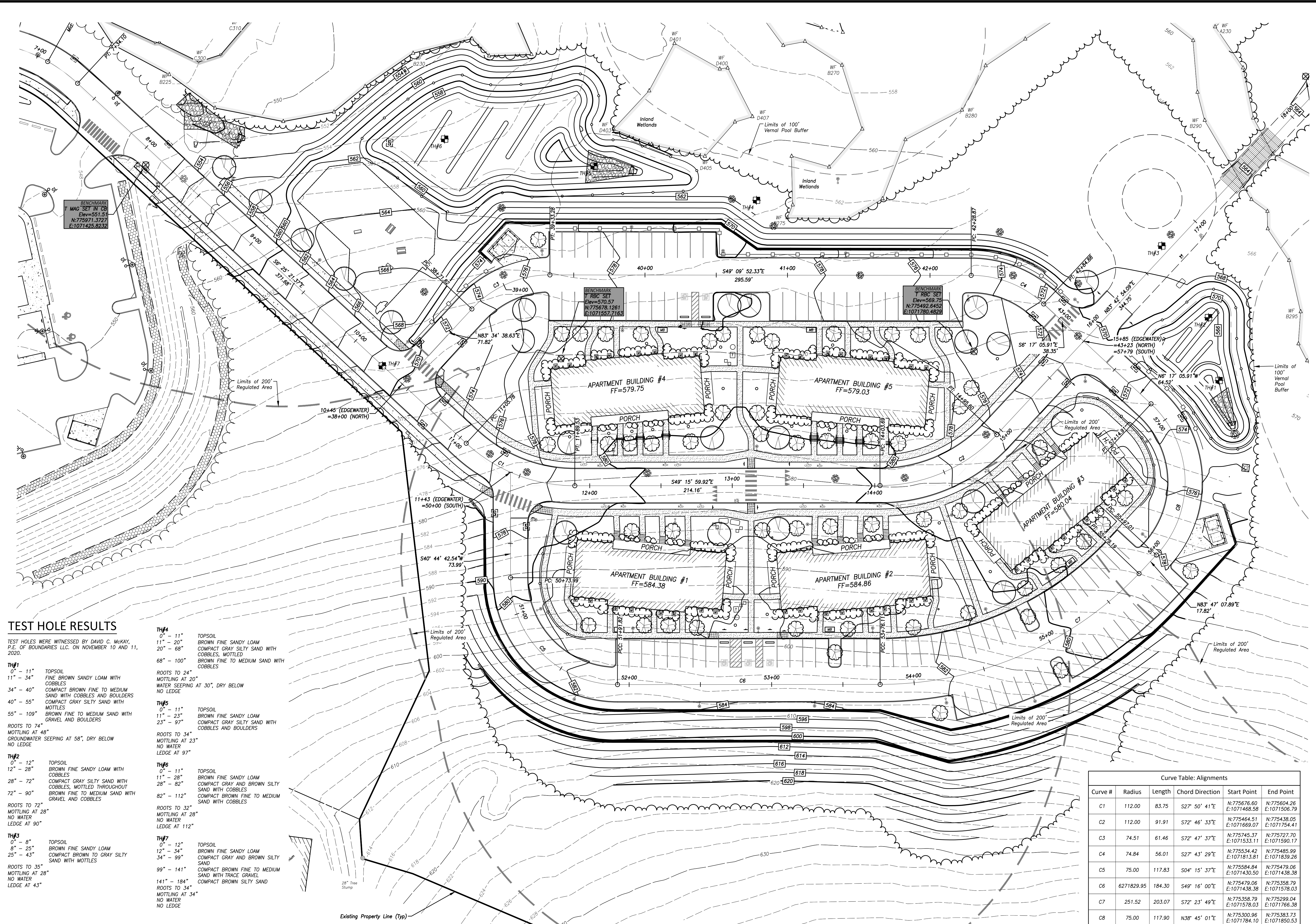


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 DATE: December 2020
 JOB I.D. NO.: 20-2853
Revisions
 Rev. A - IWWC Comments & Stormwater Quality - 1/18/21

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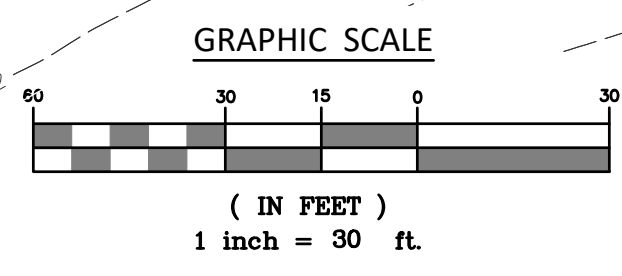
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TEST HOLE RESULTS

TEST HOLES WERE WITNESSED BY DAVID C. MCKAY, P.E. OF BOUNDARIES LLC, ON NOVEMBER 10 AND 11, 2020.

- TH#1**
 0" - 11" TOPSOIL
 11" - 34" FINE BROWN SANDY LOAM WITH COBBLES
 34" - 40" COMPACT BROWN FINE TO MEDIUM SAND WITH COBBLES AND BOULDERS
 40" - 55" COMPACT GRAY SILTY SAND WITH MOTTLES
 55" - 109" BROWN FINE TO MEDIUM SAND WITH GRAVEL AND BOULDERS
 ROOTS TO 74"
 MOTTLING AT 49"
 GROUNDWATER SEEPING AT 58", DRY BELOW NO LEDGE
- TH#2**
 0" - 12" TOPSOIL
 12" - 28" BROWN FINE SANDY LOAM WITH COBBLES
 28" - 72" COMPACT GRAY SILTY SAND WITH COBBLES, MOTTLED THROUGHOUT
 72" - 90" BROWN FINE TO MEDIUM SAND WITH GRAVEL AND COBBLES
 ROOTS TO 72"
 MOTTLING AT 28"
 NO WATER
 LEDGE AT 90"
- TH#3**
 0" - 8" TOPSOIL
 8" - 25" BROWN FINE SANDY LOAM
 25" - 43" COMPACT BROWN TO GRAY SILTY SAND WITH MOTTLES
 ROOTS TO 35"
 MOTTLING AT 28"
 NO WATER
 LEDGE AT 43"
- TH#4**
 0" - 11" TOPSOIL
 11" - 20" BROWN FINE SANDY LOAM
 20" - 68" COMPACT GRAY SILTY SAND WITH COBBLES, MOTTLED
 68" - 100" BROWN FINE TO MEDIUM SAND WITH COBBLES
 ROOTS TO 24"
 MOTTLING AT 20"
 WATER SEEPING AT 30", DRY BELOW NO LEDGE
- TH#5**
 0" - 11" TOPSOIL
 11" - 23" BROWN FINE SANDY LOAM
 23" - 97" COMPACT GRAY SILTY SAND WITH COBBLES AND BOULDERS
 ROOTS TO 34"
 MOTTLING AT 23"
 NO WATER
 LEDGE AT 97"
- TH#6**
 0" - 11" TOPSOIL
 11" - 28" BROWN FINE SANDY LOAM
 28" - 82" COMPACT GRAY AND BROWN SILTY SAND WITH COBBLES
 82" - 112" COMPACT BROWN FINE TO MEDIUM SAND WITH COBBLES
 ROOTS TO 32"
 MOTTLING AT 28"
 NO WATER
 LEDGE AT 112"
- TH#7**
 0" - 12" TOPSOIL
 12" - 34" BROWN FINE SANDY LOAM
 34" - 99" COMPACT GRAY AND BROWN SILTY SAND
 99" - 141" COMPACT BROWN FINE TO MEDIUM SAND WITH TRACE GRAVEL
 141" - 184" COMPACT BROWN SILTY SAND
 ROOTS TO 34"
 MOTTLING AT 34"
 NO WATER
 NO LEDGE



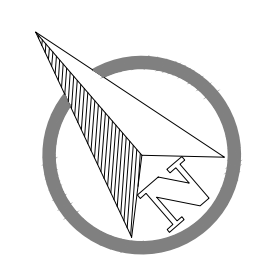
Curve Table: Alignments					
Curve #	Radius	Length	Chord Direction	Start Point	End Point
C1	112.00	83.75	S27° 50' 41"E	N:775676.60 E:1071468.58	N:775604.26 E:1071506.79
C2	112.00	91.91	S72° 46' 33"E	N:775464.51 E:1071669.07	N:775438.05 E:1071754.41
C3	74.51	61.46	S72° 47' 37"E	N:775745.37 E:1071533.11	N:775727.70 E:1071590.17
C4	74.84	56.01	S27° 43' 29"E	N:775534.42 E:1071813.81	N:775485.99 E:1071839.26
C5	75.00	117.83	S04° 15' 37"E	N:775584.84 E:1071430.50	N:775479.06 E:1071438.38
C6	6271829.95	184.30	S49° 16' 00"E	N:775479.06 E:1071438.38	N:775358.79 E:1071578.03
C7	251.52	203.07	S72° 23' 49"E	N:775358.79 E:1071578.03	N:775299.04 E:1071766.38
C8	75.00	117.90	N38° 45' 01"E	N:775300.96 E:1071784.10	N:775383.73 E:1071850.53

NOT FOR CONSTRUCTION
 1/18/2021

PLAN NOTES
 1. SEE COVER SHEET FOR ENGINEER AND SURVEYOR SIGNATURES AND SEALS.
 2. SEE SHEET 2 FOR LEGEND & ABBREVIATIONS.

P:\CIVIL 3D PROJECTS\2020\20-2853 EDgewater-APARTMENTS\DWG\DESIGN\3 APARTMENT SITE PLAN.DWG

Salt Pond Apartments at Edgewater Hill
 "Grading Plan"
 Prepared for
 Edgewater Hill Enterprises, LLC
 000 East High Street - East Hampton, Connecticut

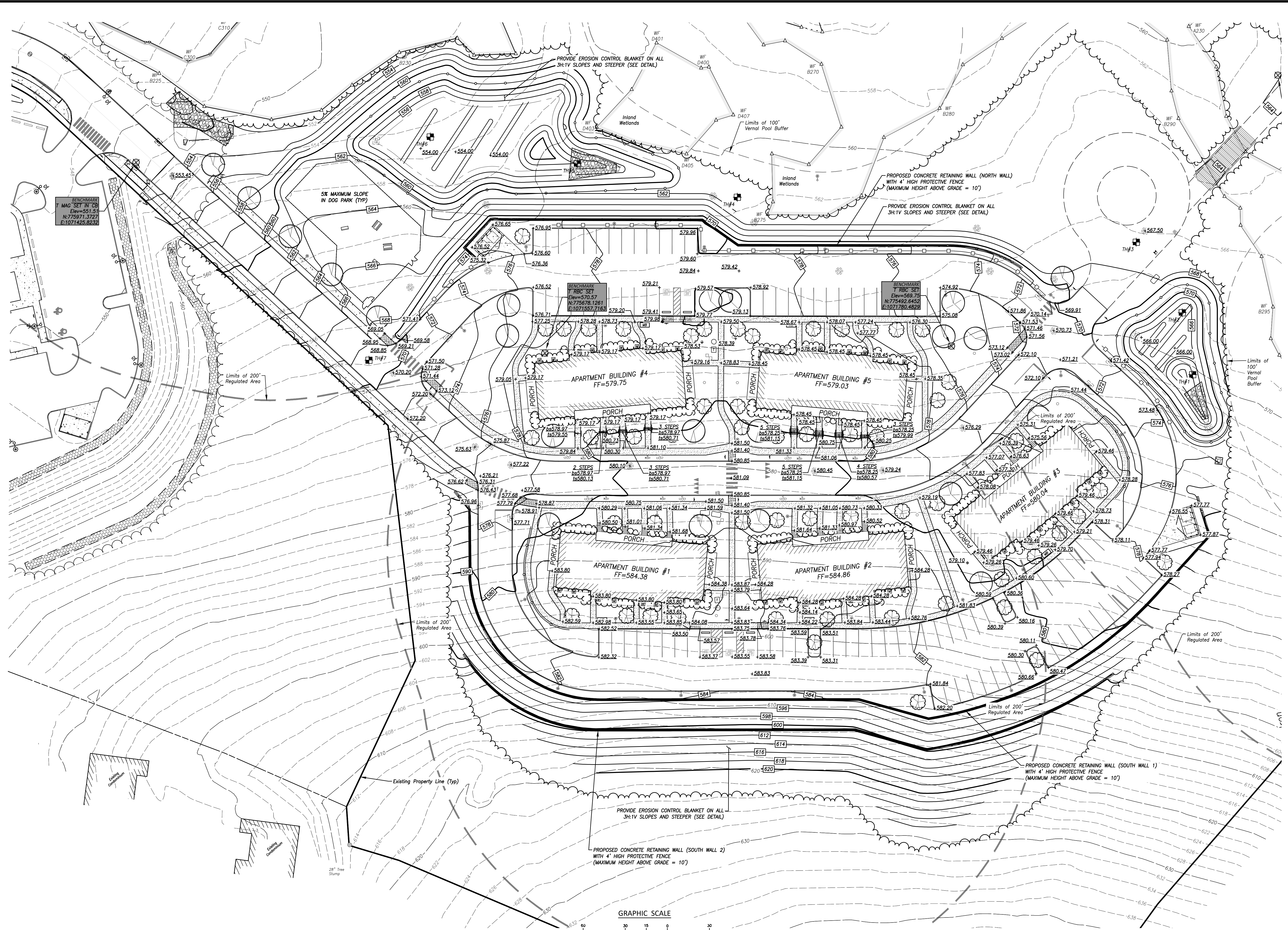


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Revisions
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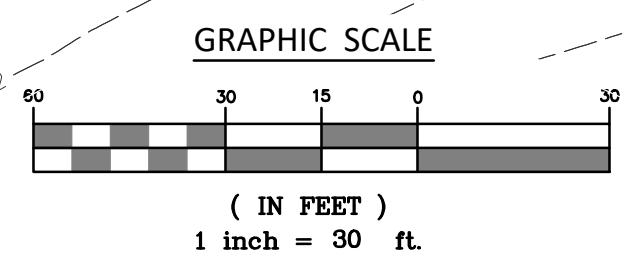
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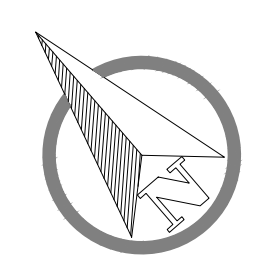
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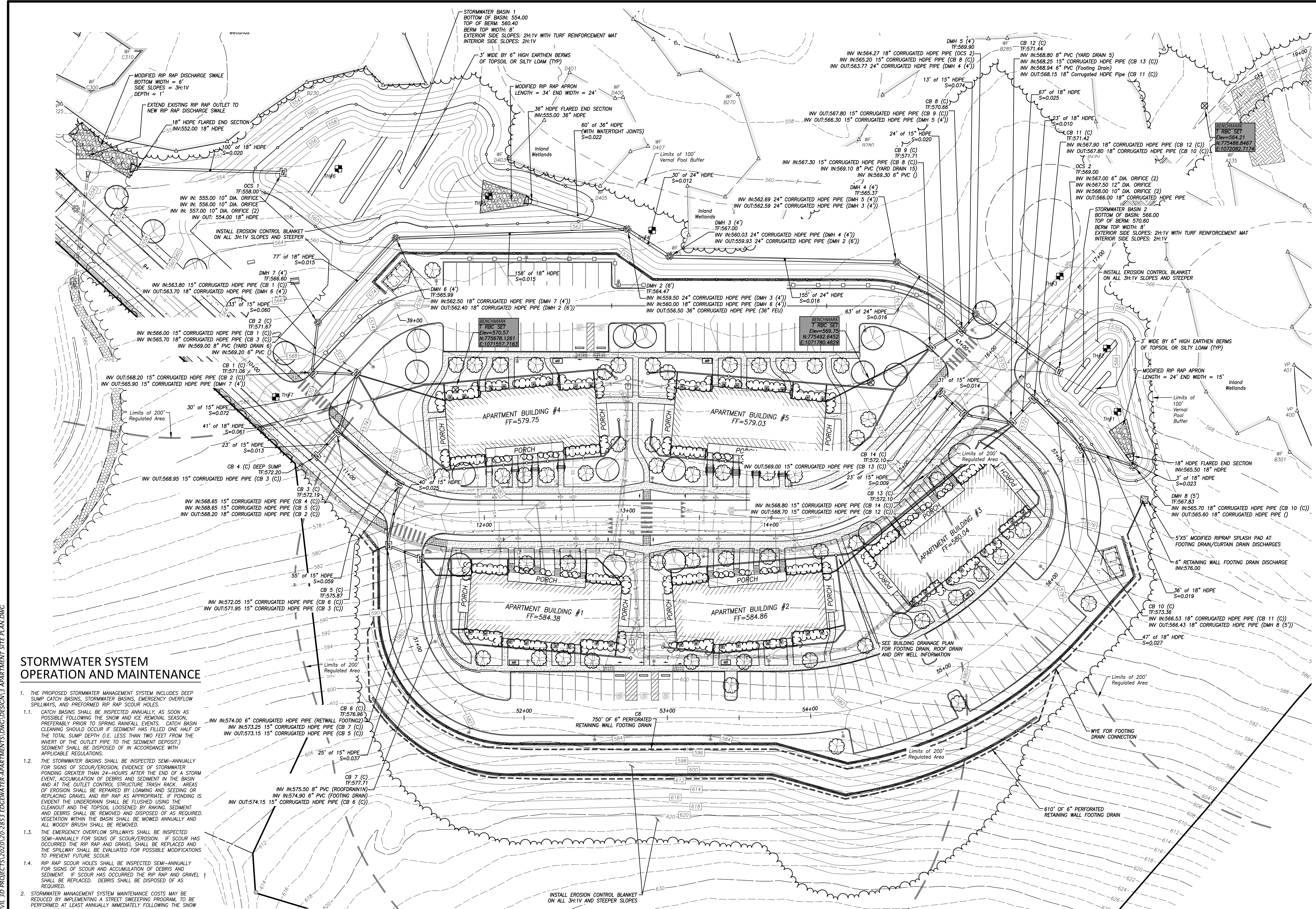
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PLAN NOTES
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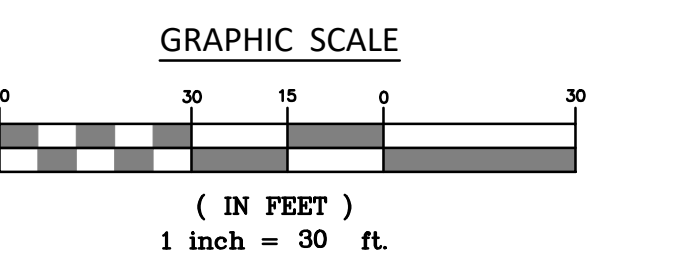
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STORMWATER SYSTEM OPERATION AND MAINTENANCE

1. THE PROPOSED STORMWATER MANAGEMENT SYSTEM INCLUDES DEEP SUMP CATCH BASINS, STORMWATER BASINS, EMERGENCY OVERFLOW SPILLWAYS, AND PREFORMED RIP RAP SCOUR HOLES.
 - 1.1. CATCH BASINS SHALL BE INSPECTED ANNUALLY, AS SOON AS POSSIBLE FOLLOWING THE SNOW AND ICE REMOVAL SEASON, PREFERABLY PRIOR TO SPRING RAINFALL EVENTS. CATCH BASIN CLEANING SHOULD OCCUR IF SEDIMENT HAS FILLED ONE HALF OF THE TOTAL SUMP DEPTH (I.E. LESS THAN TWO FEET FROM THE INVERT OF THE OUTLET PIPE TO THE SEDIMENT DEPOSIT.) SEDIMENT SHALL BE DISPOSED OF IN ACCORDANCE WITH APPLICABLE REGULATIONS.
 - 1.2. THE STORMWATER BASINS SHALL BE INSPECTED SEMI-ANNUALLY FOR SIGNS OF SCOUR/EROSION, EVIDENCE OF STORMWATER PONDING GREATER THAN 24-HOURS AFTER THE END OF A STORM EVENT, ACCUMULATION OF DEBRIS AND SEDIMENT IN THE BASIN AND AT THE OUTLET CONTROL STRUCTURE TRASH RACK. AREAS OF EROSION SHALL BE REPAIRED BY LOAMING AND SEEDING OR REPLACING GRAVEL AND RIP RAP AS APPROPRIATE. IF PONDING IS EVIDENT THE UNDERDRAIN SHALL BE FLUSHED USING THE CLEANOUT AND THE TOPSOIL LOOSENED BY RAKING. SEDIMENT AND DEBRIS SHALL BE REMOVED AND DISPOSED OF AS REQUIRED. VEGETATION WITHIN THE BASIN SHALL BE MOWED ANNUALLY AND ALL WOODY BRUSH SHALL BE REMOVED.
 - 1.3. THE EMERGENCY OVERFLOW SPILLWAYS SHALL BE INSPECTED SEMI-ANNUALLY FOR SIGNS OF SCOUR/EROSION. IF SCOUR HAS OCCURRED THE RIP RAP AND GRAVEL SHALL BE REPLACED AND THE SPILLWAY SHALL BE EVALUATED FOR POSSIBLE MODIFICATIONS TO PREVENT FUTURE SCOUR.
 - 1.4. RIP RAP SCOUR HOLES SHALL BE INSPECTED SEMI-ANNUALLY FOR SIGNS OF SCOUR AND ACCUMULATION OF DEBRIS AND SEDIMENT. IF SCOUR HAS OCCURRED THE RIP RAP AND GRAVEL SHALL BE REPLACED. DEBRIS SHALL BE DISPOSED OF AS REQUIRED.
2. STORMWATER MANAGEMENT SYSTEM MAINTENANCE COSTS MAY BE REDUCED BY IMPLEMENTING A STREET SWEEPING PROGRAM TO BE PERFORMED AT LEAST ANNUALLY IMMEDIATELY FOLLOWING THE SNOW AND ICE REMOVAL SEASON.



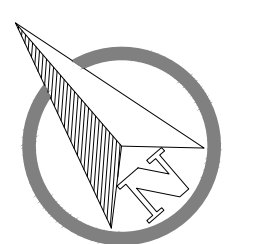
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I:\192_168.2_3\PROJECTS\CIVIL 3D PROJECTS\2020-2025\EDGEWATER-APARTMENTS\DWG\DESIGN\3 APARTMENT SITE PLAN.DWG

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Salt Pond Apartments at Edgewater Hill
"Building Drainage Plan"
Prepared for
Edgewater Hill Enterprises, LLC
000 East High Street - East Hampton, Connecticut

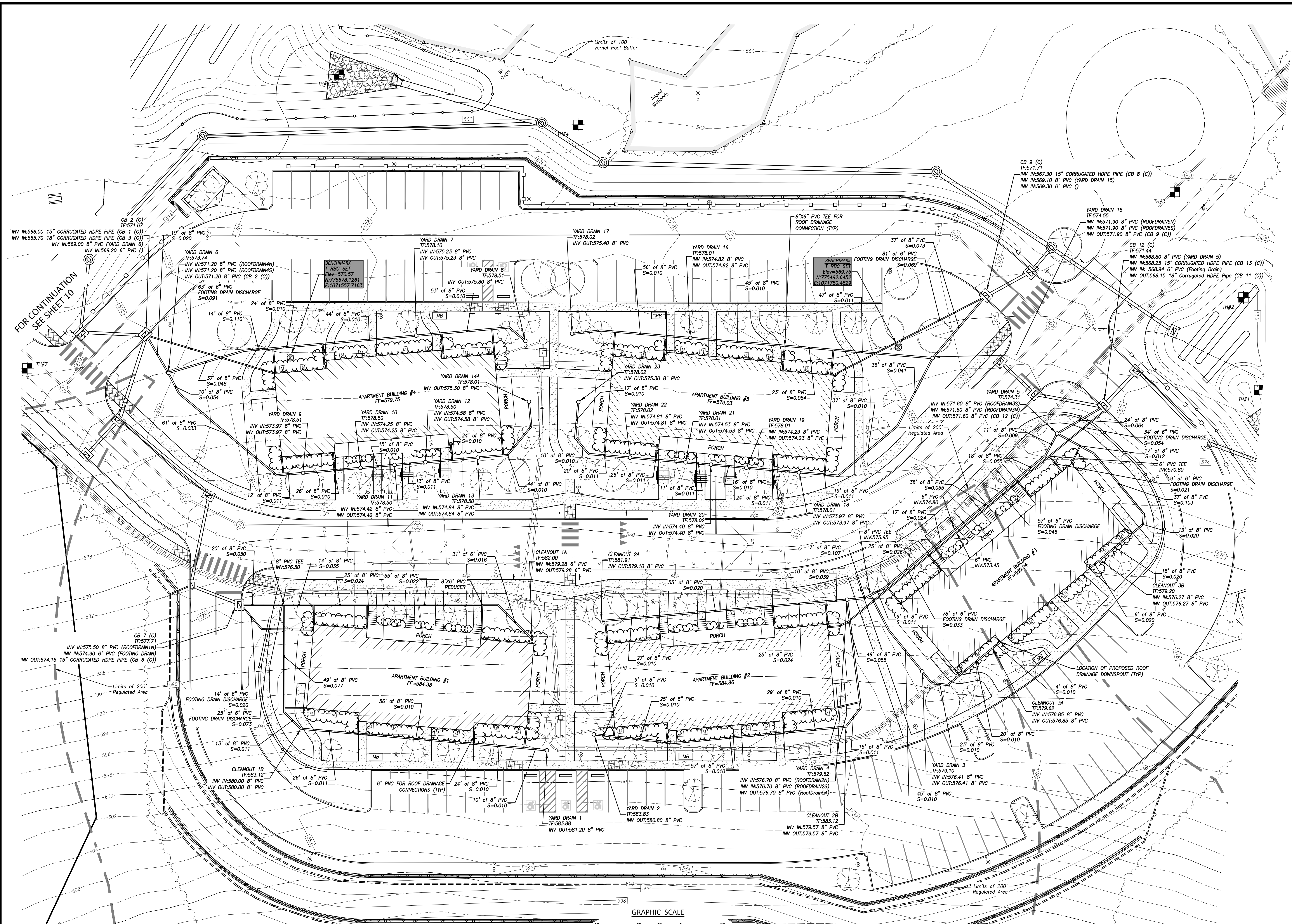


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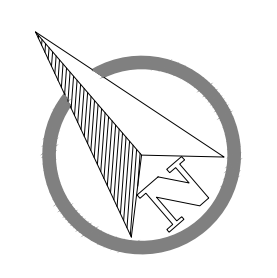
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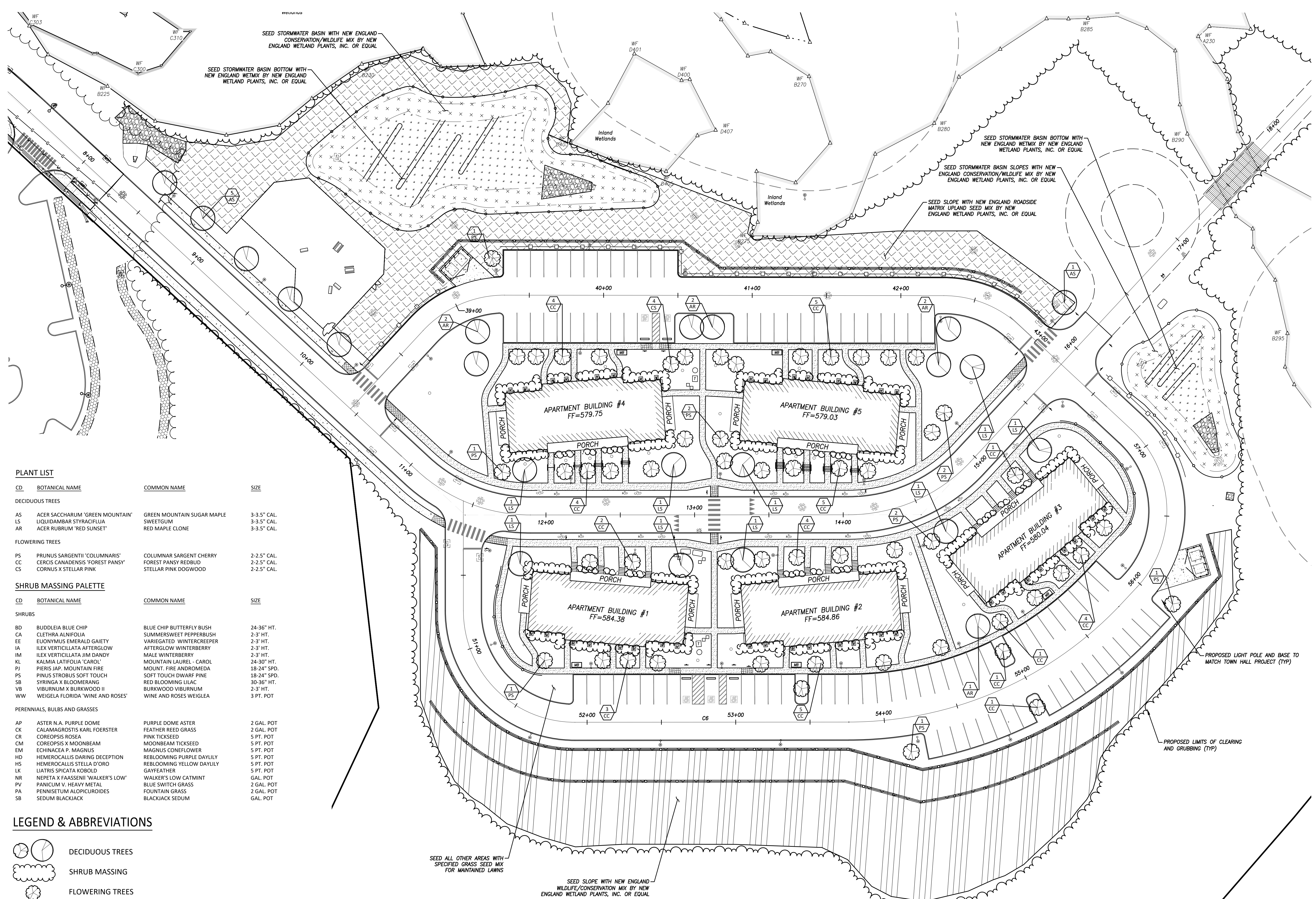
Salt Pond Apartments at Edgewater Hill
 "Landscape Plan"
 Prepared for
 Edgewater Hill Enterprises, LLC
 000 East High Street - East Hampton, Connecticut



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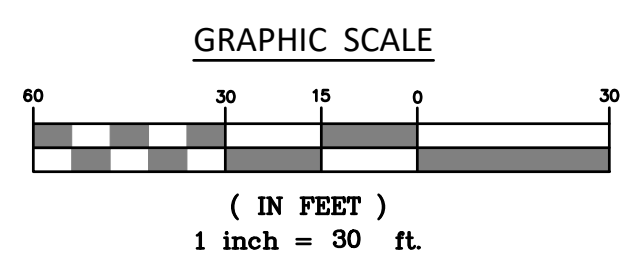


PLANT LIST

CD	BOTANICAL NAME	COMMON NAME	SIZE
DECIDUOUS TREES			
AS	ACER SACCHARUM 'GREEN MOUNTAIN'	GREEN MOUNTAIN SUGAR MAPLE	3-3.5" CAL.
LS	LIQUIDAMBAR STYRACIFLUA	SWEETGUM	3-3.5" CAL.
AR	ACER RUBRUM 'RED SUNSET'	RED MAPLE CLONE	3-3.5" CAL.
FLOWERING TREES			
PS	PRUNUS SARGENTII 'COLUMNARIS'	COLUMNAR SARGENT CHERRY	2-2.5" CAL.
CC	CERCIS CANADENSIS 'FOREST PANSY'	FOREST PANSY REDBUD	2-2.5" CAL.
CS	CORNUS X STELLAR PINK	STELLAR PINK DOGWOOD	2-2.5" CAL.
SHRUB MASSING PALETTE			
CD	BOTANICAL NAME	COMMON NAME	SIZE
SHRUBS			
BD	BUDDLEIA BLUE CHIP	BLUE CHIP BUTTERFLY BUSH	24-36" HT.
EE	CLETHRA ALNIFOLIA	SUMMERSWEET PEPPERBUSH	2-3' HT.
CA	EUONYMUS EMERALD GAJETY	VARIEGATED WINTERCREEPER	2-3' HT.
IA	ILEX VERTICILLATA AFTERGLOW	AFTERGLOW WINTERBERRY	2-3' HT.
IM	ILEX VERTICILLATA JIM DANDY	MALE WINTERBERRY	2-3' HT.
KL	KALMIA LATIFOLIA 'CAROL'	MOUNTAIN LAUREL - CAROL	24-30" HT.
PJ	PIERIS JAP. MOUNTAIN FIRE	MOUNT. FIRE ANDROMEDA	18-24" SPD.
PS	PINUS STROBUS SOFT TOUCH	SOFT TOUCH DWARF PINE	18-24" SPD.
SB	SYRINGA X BLOOMERANG	RED BLOOMING LILAC	30-36" HT.
VB	VIBURNUM X BURKWOOD II	BURKWOOD VIBURNUM	2-3' HT.
WW	WEIGELA FLORIDA 'WINE AND ROSES'	WINE AND ROSES WEIGELA	3 PT. POT
PERENNIALS, BULBS AND GRASSES			
AP	ASTER N.A. PURPLE DOME	PURPLE DOME ASTER	2 GAL. POT
CK	CALAMAGROSTIS KARL FOERSTER	FEATHER REED GRASS	2 GAL. POT
CR	COREOPSIS ROSEA	PINK TICKSEED	5 PT. POT
CM	COREOPSIS X MOONBEAM	MOONBEAM TICKSEED	5 PT. POT
EM	ECHINACEA P. MAGNUS	MAGNUS CONEFLOWER	5 PT. POT
HD	HEMEROCALLIS DARING DECEPTION	REBLOOMING PURPLE DAYLILY	5 PT. POT
HS	HEMEROCALLIS STELLA D'ORO	REBLOOMING YELLOW DAYLILY	5 PT. POT
LK	LIASTRIS SPICATA KOBOLD	GAYFEATHER	5 PT. POT
NR	NEPETA X FASSENII 'WALKER'S LOW'	WALKER'S LOW CATMINT	GAL. POT
PA	PANICUM V. HEAVY METAL	BLUE SWITCH GRASS	2 GAL. POT
PV	PENNISETUM ALOPECUROIDES	FOUNTAIN GRASS	2 GAL. POT
SB	SEDUM BLACKJACK	BLACKJACK SEDUM	GAL. POT

LEGEND & ABBREVIATIONS

- DECIDUOUS TREES
- SHRUB MASSING
- FLOWERING TREES
- LANDSCAPE MATERIAL IDENTIFIER

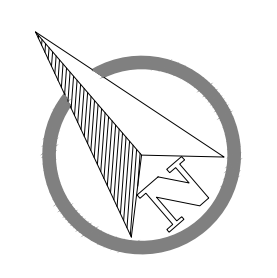


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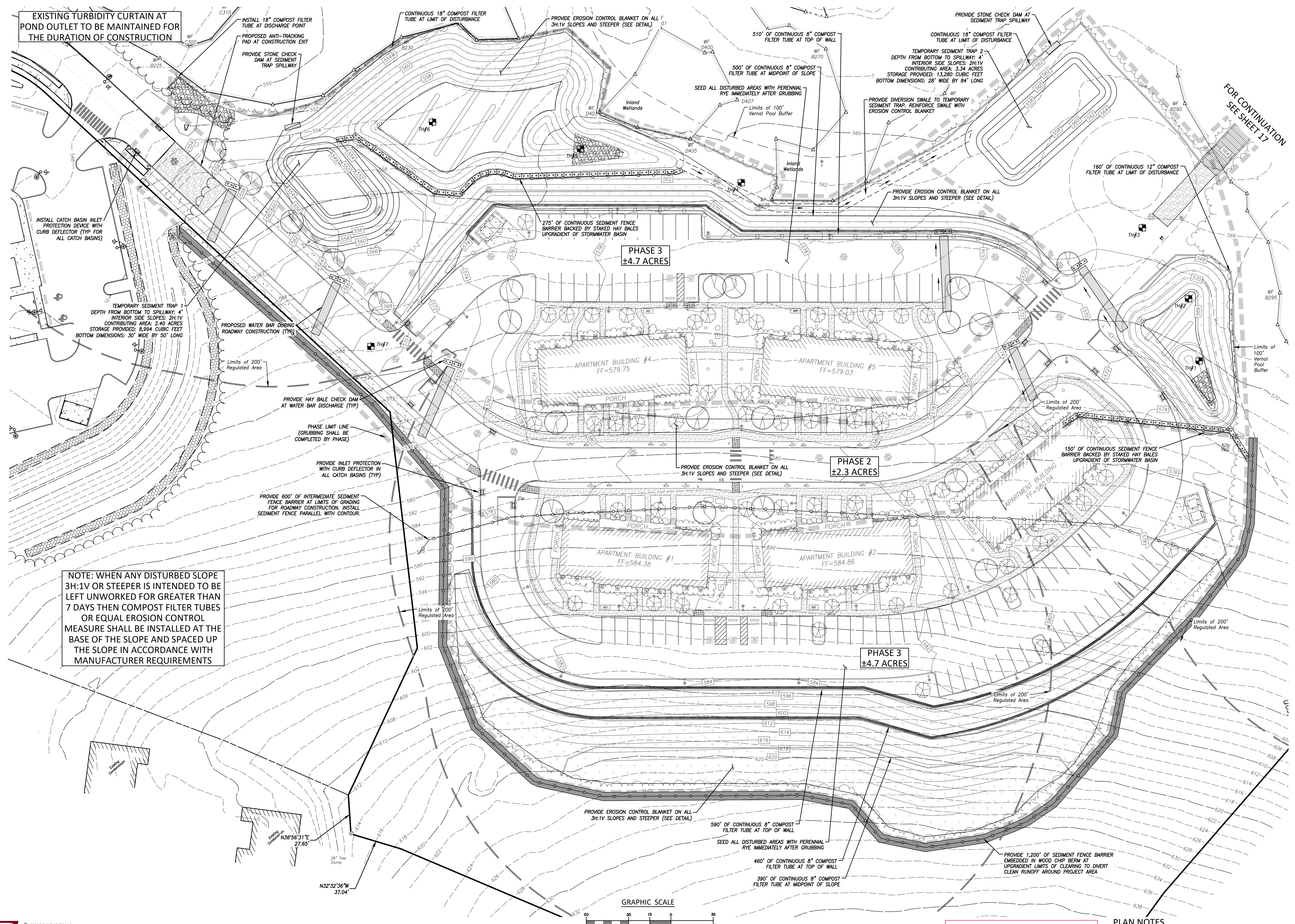
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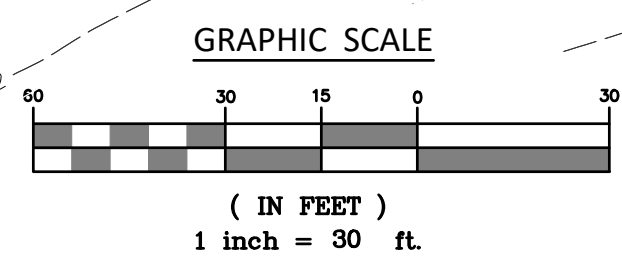
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EXISTING TURBIDITY CURTAIN AT POND OUTLET TO BE MAINTAINED FOR THE DURATION OF CONSTRUCTION

NOTE: WHEN ANY DISTURBED SLOPE 3H:1V OR STEEPER IS INTENDED TO BE LEFT UNWORKED FOR GREATER THAN 7 DAYS THEN COMPOST FILTER TUBES OR EQUAL EROSION CONTROL MEASURE SHALL BE INSTALLED AT THE BASE OF THE SLOPE AND SPACED UP THE SLOPE IN ACCORDANCE WITH MANUFACTURER REQUIREMENTS



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NARRATIVE:

THIS PROPOSAL CONSISTS OF THE DEVELOPMENT OF FIVE (5) EIGHT-UNIT APARTMENT BUILDINGS ON #9.1 ACRES IN THE EDGEWATER HILL MIXED USE DEVELOPMENT DISTRICT. THE PROJECT INCLUDES THE CONSTRUCTION OF #800 LINEAR FEET OF NEW ACCESS ROADWAY, ASSOCIATED SIDEWALKS, CIRCULATION DRIVES AND PARKING AREAS AND THE EXTENSION OF SEWER, WATER, GAS, ELECTRICITY AND COMMUNICATIONS UTILITIES TO SERVE THE PROPOSED BUILDINGS.

STORMWATER RUNOFF FROM THE PROPOSED IMPERVIOUS AREAS WILL BE COLLECTED IN DEEP SUMP CATCH BASINS WITH HOODED OUTLETS AT THE DOWNSTREAM STRUCTURE PRIOR TO DISCHARGING TO TWO STORMWATER BASINS FOR DETENTION OF PEAK STORMWATER RUNOFF RATES. THE LOW LEVEL OUTLETS OF THE STORMWATER BASINS ARE ELEVATED ABOVE THE BASIN BOTTOMS TO RETAIN THE WATER QUALITY VOLUME ON-SITE FOLLOWING STORM EVENTS. DUE TO THE PRESENCE OF A RESTRICTIVE LAYER AND PERCHED GROUNDWATER TABLES THE BOTTOM OF THE BASINS ARE SLOPED AND WILL BE PROVIDED WITH UNDERDRAINS SIZED TO DRAIN THE BASINS TO DRAIN WITHIN 72 HOURS FOLLOWING STORM EVENTS. GROUNDWATER RECHARGE WILL BE PROVIDED BY DRY WELLS WITH HIGH LEVEL OVERFLOWS THAT WILL CAPTURE THE RUNOFF FROM THE PROPOSED BUILDING ROOFS AND GRASSED AREAS.

ACCORDING TO THE UNITED STATES DEPARTMENT OF AGRICULTURE (USDA), NATURAL RESOURCES CONSERVATION SERVICE (NRCS) WEB SOIL SURVEY FOR THE STATE OF CONNECTICUT, THE SOILS LOCATED IN THE DEVELOPMENT AREA ARE AS FOLLOWS:

- 3 RIDGEBURY, LEICESTER & WHITMAN SOILS, 0-8% SLOPES, EXTREMELY STONY (HSG D) (CT WETLAND SOIL)
460 WOODBRIDGE FINE SANDY LOAM, 8-15% SLOPES, VERY STONY (HSG C/D)
860 PAXTON AND MONTAUK FINE SANDY LOAMS, 15-35% SLOPES, EXTREMELY STONY (HSG C)

INLAND WETLANDS LOCATED UPON THE SUBJECT PROPERTY ARE AS SHOWN ON THE APPROVED EDGEWATER HILL MASTER PLAN, AND PERMITS TO CONDUCT REGULATED ACTIVITIES FOR THE PROPOSED WORK ARE REQUIRED FROM THE MUNICIPAL WETLANDS AND WATERShed GROUNDWATER AGENCY. THE PROJECT PROPOSES THE REMOVAL OF ISOLATED WETLAND SERIES H (4,2,250 SF OF WETLAND ACTIVITY) AND THE INSTALLATION OF TIMBER MATS FOR THE CROSSING OF WETLAND SERIES A/B AT ITS NARROWEST POINT FOR THE HAUL ROAD (4,750 SF OF WETLAND ACTIVITY). THE DEVELOPMENT OF THE PROJECT INCLUDES #3,000 SQUARE FEET (0.07 ACRES) OF WETLAND ACTIVITY, 298,993 SQUARE FEET (6.86 ACRES) OF UPLAND REVEGETATION AREA, AND A TOTAL SITE DISTURBANCE OF 377,632 SQUARE FEET (8.67 ACRES).

CONTINUOUS SEDIMENT BARRIERS WILL BE INSTALLED AT LOCATIONS SHOWN PRIOR TO ANY EARTHWORK OPERATIONS. THESE MEASURES WILL BE MAINTAINED UNTIL ALL DISTURBED AREAS HAVE BEEN PERMANENTLY STABILIZED. GRUBBING OF STUMPS SHALL BE COMPLETED IN PHASES AS SHOWN ON THE EROSION AND SEDIMENTATION CONTROL PLAN TO LIMIT THE AMOUNT OF DISTURBED SOILS AT ANY TIME.

REFERENCE IS MADE TO:

- 1. CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL, MAY 2002.
2. SOIL SURVEY OF MIDDLESEX COUNTY CONNECTICUT, U.S.D.A. NATURAL RESOURCES CONSERVATION SERVICE.

DEVELOPMENT SCHEDULE:

PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR IS TO SCHEDULE A MANDATORY PRECONSTRUCTION MEETING ON SITE TO DISCUSS ISSUES AS THEY RELATE TO THE PROPOSED PROJECT. THESE ISSUES WILL INCLUDE BUT NOT BE LIMITED TO:

- 1. RESOURCE PROTECTION.
2. CONSTRUCTION VEHICLE ACCESS, PARKING AND FUELING.
3. CONSTRUCTION METHODS AND SCHEDULING.
4. EXISTING SITE UTILITIES AND MARK-OUT COORDINATION.
5. MATERIAL DELIVERY AND STORING.
6. UTILITY AS-BUILT DRAWINGS.
7. STORMWATER POLLUTION CONTROL PLAN AND SITE INSPECTION PROCEDURES.

SUGGESTED SEQUENCE OF CONSTRUCTION:

PHASE 1 - INSTALLATION OF EROSION CONTROLS

- 1. OBTAIN APPROPRIATE PERMITS, NOTIFY TOWN OFFICIALS OF CONSTRUCTION COMMENCEMENT, AND SUBMIT CONSTRUCTION TIMETABLE.
2. FLAG THE LIMITS OF CONSTRUCTION AND CLEARING LIMITS.
3. INSTALL THE CONSTRUCTION ENTRANCE/ANTI-TRACKING PAD.
4. ON-SITE CONSTRUCTION SEQUENCE SHALL START WITH CLEARING WITHIN THE PROPOSED CLEARING LIMITS AND REMOVE CUT WOOD, CHIP BRUSH AND SLASH, STOCKPILE CHIPS FOR FUTURE USE OR REMOVE OFF SITE, DO NOT GRUB STUMPS.
5. INSTALL GEOTEXTILE SEDIMENT FENCE, WOOD CHIP BERMS, AND/OR COMPOST FILTER TUBES AS SHOWN ON PLAN.
6. FOLLOWING INSTALLATION OF THE EROSION CONTROLS, THE CONTRACTOR SHALL CONTACT THE ENGINEER AND TOWN STAFF FOR INSPECTION AND APPROVAL OF INSTALLED MEASURES. NO WORK SHALL COMMENCE UNTIL ALL EROSION CONTROL MEASURES HAVE BEEN INSTALLED AND APPROVED.

PHASE 2 - SITE PREPARATION

- 1. GRUBBING SHALL BE COMPLETED IN PHASES AS SHOWN ON THE EROSION AND SEDIMENTATION CONTROL PLAN TO LIMIT THE AMOUNT OF DISTURBED SOIL AT ANY TIME.
2. STRIP AND STOCKPILE TOPSOIL FROM DESIGNATED GRADING AREAS BY PHASE AFTER EROSION AND SEDIMENT CONTROL MEASURES HAVE BEEN INSTALLED. THE TOPSOIL SHALL BE SEEDDED IMMEDIATELY AFTER STOCKPILING IN ORDER TO STABILIZE THE SLOPE AND LIMIT SEDIMENT RUNOFF. STOCKPILED TOPSOIL SHALL BE SEEDDED AND MULCHED WHEN IT IS TO BE STORED FOR MORE THAN 21 DAYS FROM TIME OF STOCKPILING.
3. MAKE ALL CUTS AND FILLS REQUIRED BY PHASE. ESTABLISH THE SUBGRADE FOR THE TOPSOIL AREAS, PARKING AND ROADWAY AS REQUIRED AND BENCH THE BUILDING TO A SUBGRADE. ALLOW A REASONABLE AMOUNT OF AREA AROUND THE FOOTPRINT OF THE BUILDING FOR THE CONSTRUCTION ACTIVITIES.
4. COMPACT SUBGRADE TO 95% MAXIMUM DENSITY PRIOR TO PLACING FILL OR SUBBASE FOR PAVED AREAS.

PHASE 3 - SITE IMPROVEMENTS AND BUILDING CONSTRUCTION

- 1. CONSTRUCT TEMPORARY HAUL ROAD, ASSOCIATED TEMPORARY SEDIMENT TRAP, AND ROUGH GRADE EXTENSION OF EDGEWATER CIRCLE.
2. PRIOR TO INSTALLING SURFACE WATER CONTROLS SUCH AS TEMPORARY DIVERSIONS AND WATER BARS, INSPECT EXISTING CONDITIONS TO ENSURE DISCHARGE LOCATIONS ARE STABLE. IF NOT STABLE, REVIEW DISCHARGE CONDITIONS WITH THE DESIGN ENGINEER AND IMPLEMENT ADDITIONAL STABILIZATION MEASURES PRIOR TO INSTALLING WATER SURFACE CONTROLS.
3. CONSTRUCT TEMPORARY SEDIMENT TRAPS 1 AND 2.
4. CONSTRUCT PERMANENT STORMWATER BASINS EARLY IN THE SEQUENCE OF CONSTRUCTION AND INSTALL UPGRADED EROSION CONTROL MEASURES TO PROTECT STORMWATER BASINS FROM RUNOFF. LOAM, SEED AND MULCH STORMWATER BASINS WITH SPECIFIED SEED MIXES.
5. INSTALL ALL SANITARY SEWERS, DRAINAGE SYSTEMS AND UTILITIES TO WITHIN 5 FEET OF THE BUILDING OR AS OTHERWISE MODIFIED BY THE DESIGN ENGINEER TO ADJUST FOR UNFORSEEN SITE CONDITIONS.
6. PERFORM MASS EARTHWORK AS REQUIRED TO ESTABLISH SUB-BASES FOR BUILDINGS 1 AND 2.
7. PREPARE SUB-BASE, SLOPES, PARKING AREAS, SHOULDER AREAS, ACCESS ROADS AND ANY OTHER AREA OF DISTURBANCE FOR FINAL GRADING.
8. INSTALL SUBBASE AND BASE COURSES OF GRAVEL IN PARKING AREAS.
9. PLACE TOPSOIL WHERE REQUIRED. COMPLETE THE PERIMETER LANDSCAPE PLANTINGS.
10. FINE GRADE, RAKE, SEED AND MULCH TO WITHIN 2 FEET OF THE CURBING.
11. UPON SUBSTANTIAL COMPLETION OF BUILDINGS 1 AND 2, COMPLETE THE BALANCE OF SITE WORK AND STABILIZATION OF ALL OTHER DISTURBED AREAS. INSTALL FIRST COURSE OF PAVING.
12. AFTER STABILIZATION OF ROADWAY AND AREAS SURROUNDING BUILDINGS 1 AND 2 CONTINUE EARTHWORK FOR BUILDINGS 3, 4 AND 5. EXCESS SOILS SHALL BE STOCKPILED IN THE DESIGNATED STAGING AREA, SURROUNDED WITH SILT FENCE, SEEDED WITH RYE GRASS, AND MULCHED WITH HAY.

PHASE 4 - FINAL SEEDING AND CLEANUP

- 1. EXCAVATE COLLECTED SEDIMENT FROM SEDIMENT TRAPS AND BACKFILL TO DESIGN GRADES.
2. WHEN ALL OTHER WORK HAS BEEN COMPLETED, REPAIR AND SWEEP ALL PAVED AREAS FOR THE FINAL COURSE OF PAVING. INSPECT THE DRAINAGE SYSTEM AND CLEAN AS NEEDED.
3. INSTALL FINAL COURSE OF PAVEMENT AFTER STORMWATER BASIN VEGETATION HAS BEEN ESTABLISHED.
4. ALL DISTURBED AREAS SHALL BE PREPARED WITH TOPSOIL AND SEEDDED AND MULCHED ACCORDING TO THIS PLAN.
5. AFTER ALL FINAL GRADED DISTURBED AREAS HAVE BEEN STABILIZED, REMOVE ALL EROSION AND SEDIMENT STRUCTURES. CLEAN ALL STORMWATER STRUCTURES OF SEDIMENT AND DEBRIS.

ANTICIPATED CONSTRUCTION SCHEDULE

Table with 3 columns: NO., PHASE DESCRIPTION, ESTIMATED DURATION. Rows include installation of erosion controls, site preparation, site improvements and building construction, and final paving, final seeding and cleanup.

EROSION CONTROL OPERATION & MAINTENANCE:

THE SITE CONTRACTOR SHALL BE RESPONSIBLE FOR THE INSTALLATION AND MAINTENANCE OF EROSION AND SEDIMENT CONTROL MEASURES THROUGHOUT THE PROJECT. NO CONSTRUCTION SHALL PROCEED UNTIL PROPER SEDIMENTATION AND EROSION CONTROL METHODS HAVE BEEN INSTALLED AS THE SEQUENCE OF CONSTRUCTION NECESSITATES.

MAINTENANCE OF EROSION AND SEDIMENT CONTROLS SHALL BE COMPLETED IN ACCORDANCE WITH THE CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL (2002). THE CONTRACTOR SHALL MAINTAIN A COPY OF THE GUIDELINES ON-SITE AND REFER TO THE APPROPRIATE MAINTENANCE PROCEDURES THAT SHALL BE UTILIZED DURING THE CONSTRUCTION (https://portal.ct.gov/DEEP/Water/Soil-Erosion-and-Sediment-Control-Guidelines/Guidelines-for-Soil-Erosion-and-Sediment-Control). A SUMMARY OF THE MAINTENANCE REQUIREMENTS FOR THE PROJECT IS PROVIDED BELOW.

DURING CONSTRUCTION, ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE MAINTAINED IN PROPER WORKING ORDER. DISTURBED AREAS SHALL BE KEPT TO A MINIMUM AND SHALL ONLY TAKE PLACE WHERE IMMEDIATELY REQUIRED TO FURTHER CONSTRUCTION. IT IS DESIRABLE FROM AN EROSION PREVENTION PERSPECTIVE TO MINIMIZE DISTURBED AREAS. FINAL GRADING AND SEEDING SHALL TAKE PLACE AS SOON AS PRACTICAL.

A RAIN GAUGE SHALL BE PLACED AT THE PROJECT IN A WORKABLE LOCATION AND MONITORED DURING RAINFALL PERIODS UNTIL ALL DISTURBED AREAS ARE STABILIZED.

EVERY PRECAUTION SHALL BE USED DURING CONSTRUCTION TO PREVENT AND MINIMIZE THE DEGRADATION OF THE EXISTING WATER QUALITY FROM STORMWATER RUNOFF DURING CONSTRUCTION. ALL ACTIVITIES SHALL BE IN CONFORMANCE TO AND CONSISTENT WITH ALL APPLICABLE WATER QUALITY STANDARDS AND MANAGEMENT PRACTICES AS SET FORTH BY LOCAL, STATE AND FEDERAL AGENCIES.

THE SITE CONTRACTOR SHALL APPOINT AN ONSITE AGENT WHO SHALL BE PERSONALLY RESPONSIBLE FOR IMPLEMENTING THIS EROSION AND SEDIMENT CONTROL PLAN AND ENFORCING THE PRESCRIBED SAFEGUARDS DURING THE EXCAVATION AND OPERATION PERIOD.

THIS RESPONSIBILITY INCLUDES THE INSTALLATION AND MAINTENANCE OF CONTROL MEASURES THROUGHOUT THE PROJECT, INFORMING ALL PARTIES ENGAGED ON SITE OF THE REQUIREMENTS AND OBJECTIVES OF THE PLAN, AND NOTIFYING THE PROPER AGENCY AND OFFICIALS OF ANY TRANSFER OF THIS RESPONSIBILITY.

ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE REPAIRED, CLEANED AND/OR REPLACED AS NECESSARY THROUGHOUT THE PROJECT IN ORDER TO MAINTAIN COMPLETE AND INTEGRAL EROSION AND SEDIMENT CONTROL PROTECTION. ONCE IN PLACE, ALL EROSION AND SEDIMENT CONTROL MEASURES ARE TO REMAIN IN PLACE IN PROPER CONDITION AND BE CONTINUOUSLY MAINTAINED UNTIL FINAL SITE RESTORATION HAS BEEN COMPLETED. FOLLOWING SUCH PERMANENT STABILIZATION, THE EROSION AND SEDIMENT CONTROL MEASURES SHALL BE DISMANTLED, REMOVED, AND DISPOSED OF IN AN APPROVED MANNER. ADDITIONAL MEASURES NECESSARY TO ADDRESS FIELD CONDITIONS AND/OR AS ORDERED OR PRESCRIBED HEREIN SHALL BE PUT IN PLACE, WHENEVER NECESSARY, TO ADDRESS FIELD CONDITIONS AND/OR AS ORDERED BY THE ENGINEER.

QUALIFIED PERSONNEL PROVIDED BY THE SITE CONTRACTOR SHALL INSPECT PERIMETER EROSION CONTROL MEASURES, ALL DISTURBED AREAS AND THE LOCATIONS WHERE VEHICLES ENTER AND LEAVE THE SITE. THESE AREAS SHALL BE INSPECTED AT LEAST ONCE EVERY SEVEN CALENDAR DAYS AND WITHIN TWENTY-FOUR HOURS AT THE END OF A STORM THAT IS 0.5 INCHES OR GREATER. ADDITIONAL MEASURES BEYOND THOSE INDICATED AND/OR SHOWN ON THIS PLAN SET OR PRESCRIBED HEREIN SHALL BE PUT IN PLACE WHENEVER NECESSARY TO ADDRESS FIELD CONDITIONS AND/OR AS ORDERED BY THE ENGINEER OR TOWN STAFF. WHERE SITES HAVE BEEN TEMPORARILY OR FINALLY STABILIZED, SUCH INSPECTION SHALL BE CONDUCTED AT LEAST ONCE EVERY MONTH FOR THREE CONSECUTIVE MONTHS.

NO SOIL, FILL OR OTHER MATERIALS SHALL BE DEPOSITED IN SURROUNDING INLAND WETLANDS.

ALL TEMPORARY STORAGE AND/OR STOCKPILE AREAS SHALL BE PROPERLY STABILIZED TO PREVENT EROSION AND SUITABLY CONTAINED TO PREVENT TURBID RUNOFF.

DUMPING OF OIL OR OTHER DELETERIOUS MATERIALS ON THE GROUND IS FORBIDDEN. THE APPLICANT SHALL PROVIDE A MEANS OF CATCHING, RETAINING AND PROPERLY DISPOSING OF DRAINED OIL, REMOVED OIL FILTERS, OR OTHER DELETERIOUS MATERIAL FROM EQUIPMENT USED ON SITE. MAJOR VEHICLE MAINTENANCE SHALL BE COMPLETED OFF SITE. ALL OIL SPILLS SHALL BE IMMEDIATELY REPORTED TO THE DEPARTMENT OF ENERGY AND ENVIRONMENTAL PROTECTION/HAZARDOUS MATERIALS UNIT. FAILURE TO DO SO MAY RESULT IN THE IMPOSITION OF FINES UNDER THE APPLICABLE CONNECTICUT GENERAL STATUTES.

DURING CONSTRUCTION, THE SITE CONTRACTOR SHALL BE RESPONSIBLE FOR SITE INSPECTION AND MAINTENANCE TO INSURE PROPER PERFORMANCE OF EROSION CONTROL MEASURES. INSPECTION AND MAINTENANCE SHALL INCLUDE, AT A MINIMUM, THE FOLLOWING:

- INSPECT ALL SEDIMENT FENCE, WOOD CHIP BERMS AND OTHER EROSION CONTROL MEASURES. REPAIR OR REPLACE ANY DAMAGED PORTION IN ORDER TO INSURE ITS PROPER AND EFFECTIVE OPERATION. REMOVE ACCUMULATED SEDIMENT IF REQUIRED (GREATER THAN 4" DEPTH).
- INSPECT ALL STOCKPILES. REPAIR OR REPLACE ANY DAMAGED PORTION OF EROSION CONTROL MEASURES SURROUNDING THESE AREAS IN ORDER TO PREVENT SEDIMENTATION DOWNDRAIN. RESEED AND RE-MULCH AS REQUIRED TO STABILIZE STOCKPILES.
- INSPECT GRASS RESTORED AREAS. REVEGETATE ANY ERODED OR DISTURBED AREAS TO PROVIDE PERMANENT STABILIZATION. RESEED AND/OR REVEGETATE ANY AREAS THAT DO NOT HAVE A SUITABLE STAND OF GRASS OR ANY SCOURED AREAS TO PROVIDE PERMANENT STABILIZATION.
- INSPECT ANTI-TRACKING PAD. REMOVE AND DISPOSE OF PAD AND REPLACE IF PAD IS NO LONGER FUNCTIONING EFFICIENTLY OR ACCUMULATED SEDIMENT IS TO A DEPTH OF 2" BELOW THE STONE SURFACE.
- INSPECT ALL STONE CHECK DAMS, TEMPORARY DIVERSIONS, AND WATER BARS. REMOVE ACCUMULATED SEDIMENT IF REQUIRED (BLOCKING MORE THAN 3" DEPTH OF FLOW).
- INSPECT ALL TEMPORARY AND PERMANENT STORMWATER BASINS. REMOVE ACCUMULATED SEDIMENT IF REQUIRED (GREATER THAN 6" DEPTH). REVEGETATE IF NECESSARY TO PROVIDE STABILIZATION.
- INSPECT DOWNGRADIENT AREAS OF ALL STORMWATER DISCHARGES AND DEVELOPMENT AREAS. STABILIZE ANY ERODED AREAS IF FOUND.

EROSION AND SEDIMENT CONTROL BEST MANAGEMENT PRACTICES (BMP'S)

MINIMIZE DISTURBED AREA AND PROTECT NATURAL FEATURES AND SOIL

TOPSOIL:

TOPSOIL WILL BE REMOVED AND STOCKPILED ON SITE AND UTILIZED FOR FINAL GRADING. ADDITIONAL TOPSOIL IF REQUIRED, WILL BE SUPPLIED FROM OFF-SITE SOURCES. EXCESS MATERIALS RESULTING FROM "CUT SLOPES" IN THE AREAS OF THE PROPOSED CONSTRUCTION THAT ARE NOT INTENDED FOR REUSE WILL BE IMMEDIATELY REMOVED FROM THE SITE. WHEN SOIL IS STOCKPILED, THE SLOPE OF THE STOCKPILE WILL NOT EXCEED 2 HORIZONTAL TO 1 VERTICAL. GRUBBING OF STUMPS SHALL BE COMPLETED BY PHASE TO MINIMIZE AMOUNT OF DISTURBED SOILS. STOCKPILED TOPSOIL SHALL BE STORED FOR MORE THAN 21 DAYS FROM TIME OF STOCKPILING. INSPECT ALL TEMPORARY AND PERMANENT STOCKPILE AREAS. SEDIMENT FENCE WILL BE PLACED AROUND ANY STOCKPILES THAT ARE NOT IMMEDIATELY REMOVED FROM THE SITE TO PROTECT THE EXISTING DRAINAGE DITCHES AND OFF SITE AREAS.

MAINTENANCE AND INSPECTION: THE CUT AND FILL AREAS WILL BE INSPECTED WEEKLY FOR EROSION. THESE AREAS WILL BE STABILIZED IMMEDIATELY WITH EROSION CONTROLS OR GRADED TO AVOID POSSIBLE DISTURBANCE TO THE EXISTING DRAINAGE DITCHES OR OFF SITE AREAS. SEE ALSO MAINTENANCE AND INSPECTION PROCEDURES FOR SILT FENCE.

CONTROL STORMWATER FLOWING ONTO AND THROUGH THE PROJECT

AREA FOR SILT TO ACCUMULATE:

BMP INSTALLATION SCHEDULE: BEFORE ANY GRADING OPERATIONS BEGIN, A WOOD CHIP BERM OR SEDIMENT FENCE WILL BE INSTALLED ADJACENT TO THE AREAS UNDER CONSTRUCTION JUST OUTSIDE THE LIMITS OF DISTURBANCE. OTHER ADJACENT OFF SITE AREAS WILL ALWAYS BE PROTECTED BY A SEDIMENT FENCE OR ANOTHER BMP UNTIL FINAL STABILIZATION IS ACHIEVED. SEDIMENT FENCE IS ALSO PROPOSED UPGRADEMENT OF DISTURBED AREAS TO MINIMIZE CLEAN RUNOFF ENTERING THE PROJECT AREA.

CONSTRUCTION SPECIFICATIONS

WOOD CHIP BERM: THE MATERIAL FOR WOOD CHIP BERMS WILL BE ACQUIRED IN CONJUNCTION WITH THE REMOVAL AND CHIPPING OF TREES LOCATED WITHIN THE PROJECT AREA.

INSTALLATION: ERECT WOOD CHIP BERM IN A CONTINUOUS FASHION AT THE SPECIFIED HEIGHT AND WIDTH. MAINTENANCE: 1. SEDIMENT SHOULD BE REMOVED ONCE IT HAS ACCUMULATED TO A DEPTH OF 4". 2. BERM SHOULD BE REPAIRED IF IT HAS BEEN BREACHED. 3. BERM CAN BE LEFT IN PLACE PERMANENTLY AND LEFT TO DETERIORATE. 4. ALL SEDIMENT ACCUMULATED AT THE BERM SHOULD BE REMOVED AND PROPERLY DISPOSED OF IF THE BERM IS TO BE REMOVED.

SEDIMENT FENCE:

- 1. THE MATERIAL FOR SEDIMENT FENCES SHOULD BE A PERVIOUS SHEET OF SYNTHETIC FABRIC SUCH AS POLYPROPYLENE, NYLON, POLYESTER, OR POLYETHYLENE YARN.
2. THE STAKES USED TO ANCHOR THE FILTER FABRIC SHOULD BE WOOD OR METAL. WOODEN STAKES SHOULD BE AT LEAST 3 FEET LONG AND HAVE A MINIMUM DIAMETER OF 2 INCHES IF A HARDWOOD LIKE OAK IS USED. STAKES FROM SOFT WOODS LIKE PINE SHOULD BE AT LEAST 4 INCHES IN DIAMETER.
3. EACH SECTION OF FABRIC SHALL BE A CONTINUOUS ROLL OF FABRIC TO ELIMINATE GAPS IN THE FABRIC. IF A CONTINUOUS ROLL OF FABRIC IS NOT AVAILABLE, OVERLAP THE FABRIC FROM BOTH DIRECTIONS ONLY AT STAKES OR POSTS. OVERLAP AT LEAST 6 INCHES. EXCAVATE A TRENCH TO BURY THE BOTTOM OF THE FABRIC FENCE AT LEAST 2 INCHES BELOW THE GROUND SURFACE. THIS HELPS TO PREVENT GAPS FROM FORMING NEAR THE GROUND SURFACE. GAPS WOULD MAKE THE FENCING LESS AS A SEDIMENT BARRIER.
4. THE HEIGHT OF THE FENCE POSTS SHOULD BE 16 TO 34 INCHES ABOVE THE ORIGINAL GROUND SURFACE. SPACE THE POSTS NO MORE THAN 10 FEET APART.
5. THE FENCE SHOULD BE DESIGNED TO WITHSTAND THE RUNOFF FROM A 10-YEAR PEAK STORM EVENT. ONCE INSTALLED, IT SHOULD REMAIN IN PLACE UNTIL ALL AREAS UPSLOPE HAVE BEEN PERMANENTLY STABILIZED BY VEGETATION OR OTHER MEANS.

INSTALLATION: 1. DIG A 6" DEEP TRENCH ON THE UPHILL SIDE OF THE PROPOSED BARRIER LOCATION. 2. POSITION THE POSTS ON THE DOWNHILL SIDE OF THE FABRIC BARRIER AND DRIVE THE POST 12" INTO THE GROUND. 3. LAY THE BOTTOM 6" OF THE FABRIC BARRIER IN THE TRENCH TO PREVENT UNDERMINING AND BACKFILL COMPACT BACKFILLED SOILS.

MAINTENANCE:

- 1. SEDIMENT SHOULD BE REMOVED ONCE IT HAS ACCUMULATED TO 4" DEPTH.
2. FILTER FABRIC SHOULD BE REPLACED WHENEVER IT HAS DETERIORATED TO SUCH AN EXTENT THAT THE EFFECTIVENESS OF THE FABRIC IS REDUCED (APPROXIMATELY SIX MONTHS).
3. SEDIMENT FENCE SHOULD REMAIN IN PLACE UNTIL DISTURBED AREAS HAVE BEEN PERMANENTLY STABILIZED.
4. ALL SEDIMENT ACCUMULATED AT THE FENCE SHOULD BE REMOVED AND PROPERLY DISPOSED OF BEFORE THE FENCE IS REMOVED.

INSPECTION:

- 1. INSPECT SEDIMENT FENCE BEFORE ANTICIPATED STORM EVENTS (OR SERIES OF STORM EVENTS SUCH AS INTERMITTENT SHOWERS OVER ONE OR MORE DAYS) AND WITHIN 24 HOURS AFTER THE END OF A STORM EVENT OF 0.5 INCHES OR GREATER, AND AT LEAST ONCE EVERY SEVEN CALENDAR DAYS, AT LEAST 72 HOURS APART.
2. WHERE SITES HAVE BEEN FINALLY OR TEMPORARILY STABILIZED, SUCH INSPECTIONS MAY BE CONDUCTED ONCE PER MONTH.

HAY/STRAW BALE BARRIER

INSTALLATION:

- 1. EXCAVATE TRENCH 4" AND PLACE MATERIAL UPSLOPE OF TRENCH.
2. PLACE BALES IN A SINGLE ROW IN THE TRENCH, LENGTHWISE, WITH ENDS OF ADJACENT BALES TIGHTLY ABUTTING ONE ANOTHER AND THE ENDINGS ORIENTED AROUND THE SIDES RATHER THAN ALONG THE TOPS AND BOTTOMS OF THE BALES TO AVOID PREATURE ROTTING OF THE ENDINGS).
3. ANCHOR EACH BALE WITH AT LEAST 2 STAKES DRIVEN THE FIRST STAKE IN EACH BALE TOWARD THE PREVIOUSLY LAID BALE TO FORCE THE BALES TOGETHER. STAKES MUST BE DRIVEN A MINIMUM OF 18 INCHES INTO THE GROUND. FILL ANY GAPS BETWEEN THE BALES WITH STRAW TO PREVENT WATER FROM ESCAPING BETWEEN THE BALES.
4. BACKFILL THE BALES WITH THE EXCAVATED TRENCH MATERIAL TO A MINIMUM DEPTH OF 4 INCHES ON THE UPHILL SIDE OF THE BALES. TAMP BY HAND OR MACHINE AND COMPACT THE SOIL. LOOSE HAY/STRAW SCATTERED OVER THE DISTURBED AREA IMMEDIATELY UPHILL FROM THE HAY BALE BARRIER TENDS TO INCREASE BARRIER EFFICIENCY.

MAINTENANCE

- 1. INSPECT THE HAY/STRAW BALE BARRIER AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL AMOUNT OF 0.5 INCH OR GREATER TO DETERMINE MAINTENANCE NEEDS. FOR DEWATERING OPERATIONS, INSPECT FREQUENTLY BEFORE, DURING, AND AFTER PUMPING OPERATIONS. REMOVE THE SEDIMENT DEPOSITS WHEN SEDIMENT DEPOSITS REACH APPROXIMATELY ONE HALF THE HEIGHT OF THE BARRIER.
2. REPLACE OR REPAIR THE BARRIER WITHIN 24 HOURS OF OBSERVED FAILURE. FAILURE OF THE BARRIER HAS OCCURRED WHEN SEDIMENT FAILS TO BE RETAINED BY THE BARRIER BECAUSE:
(a) THE BARRIER HAS BEEN OVERTOPPED, UNDERCUT OR BYPASSED BY RUNOFF WATER,
(b) THE BARRIER HAS BEEN MOVED OUT OF POSITION, OR
(c) THE BALES HAVE DETERIORATED OR BEEN DAMAGED.
3. WHEN REPETITIVE FAILURES OCCUR AT THE SAME LOCATION, REVIEW CONDITIONS AND LIMITATIONS FOR USE AND DETERMINE IF ADDITIONAL CONTROLS ARE NEEDED TO REDUCE FAILURE RATE OR REPLACE HAY/STRAW BALE BARRIER.
4. MAINTAIN THE HAY/STRAW BALE BARRIER UNTIL THE CONTRIBUTING AREA IS STABILIZED. AFTER THE UPSLOPE AREAS HAVE BEEN PERMANENTLY STABILIZED, PULL THE STAKES OUT OF THE HAY BALES. REMOVE SEDIMENT.

DUST CONTROL:

JUST FROM THE SITE WILL BE CONTROLLED BY USING A MOBILE PRESSURE-TYPE DISTRIBUTOR TRUCK THAT WILL APPLY POTABLE WATER AT RATE OF 300 GALLONS PER ACRE AND MINIMIZED AS NEEDED TO AVOID PONDING. INSTALLATION SCHEDULE: DUST CONTROL WILL BE IMPLEMENTED AS NEEDED ONCE SITE GRADING HAS BEEN INITIATED, AND DURING WINDY CONDITIONS EXCEEDING 20MPH, WHILE SITE GRADING IS OCCURRING. SPRAYING OF POTABLE WATER WILL BE PERFORMED ONCE PER DAY DURING THE MONTHS OF MARCH THROUGH MAY AND NO MORE THAN THREE TIMES PER DAY FROM JUNE TO SEPTEMBER OR WHENEVER DRYNESS OF SOIL WARRANTS IT. MAINTENANCE SCHEDULE: AT LEAST ONE MOBILE UNIT WILL BE AVAILABLE AT ALL TIMES DURING CONSTRUCTION TO APPLY POTABLE WATER. EACH MOBILE UNIT SHALL BE EQUIPPED WITH A POSITIVE SHUTOFF VALVE TO PREVENT OVER WATERING OF DISTURBED AREAS.

RETAIN SEDIMENT ON-SITE AND CONTROL DEWATERING PRACTICES

SIZE AND CONSTRUCT THE BASIN IN ACCORDANCE WITH THE REQUIREMENTS OF THE "CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL, MAY 2002".

SITE PREPARATION:

CLEAR, GRUB AND STRIP TOPSOIL TO REMOVE TREES, VEGETATION, ROOTS, OR OTHER UNSUITABLE MATERIAL FROM AREAS IN CONTACT WITH THE EMBANKMENT OR ANY STRUCTURAL WALLS ADJACENT TO THE BASIN. CLEAR AND GRUB THE AREA OF MOST FREQUENT INUNDATION (MEASURED FROM THE TOP OF THE OUTLET CONTROL STRUCTURE) OF ALL BRUSH AND TREES TO FACILITATE CLEAN OUT AND RESTORATION. INSTALL SEDIMENT CONTROLS FOR CONTRIBUTING AREAS. INSTALL SEDIMENT CONTROLS TO TRAP SEDIMENT BEFORE IT ENTERS AND LEAVES THE DETENTION BASIN CONSTRUCTION SITE. STABILIZE THE BASIN IN ACCORDANCE WITH THE ENGINEERED DESIGN. STABILIZE THE SPOIL AND BORROW AREAS, AND OTHER DISTURBED AREAS IN ACCORDANCE WITH THE TEMPORARY SEEDING OR PERMANENT SEEDING, WHICHEVER IS APPLICABLE. INSTALL SAFETY FEATURES AND DEVICES TO PROTECT HUMANS AND ANIMALS FROM SUCH ACCIDENTS AS FALLING OR DROWNING. TEMPORARY FENCING CAN BE USED UNTIL BARRIER PLANTINGS ARE ESTABLISHED. USE PROTECTIVE MEASURES SUCH AS GUARDRAILS AND FENCES ON SPILLWAYS AND IMPROVEMENTS AS NEEDED.

MAINTENANCE:

INSPECT THE TEMPORARY SEDIMENT BASIN AT LEAST ONCE A WEEK AND WITHIN 24 HOURS OF THE END OF A STORM WITH A RAINFALL AMOUNT OF 0.5 INCHES OR GREATER TO DETERMINE CONDITIONS IN THE BASIN. CLEAN THE BASIN OF COLLECTED SEDIMENTS WHEN SEDIMENT ACCUMULATES 6 INCHES. SEDIMENT LEVELS SHALL BE MARKED WITHIN THE SEDIMENT STORAGE AREA BY STAKES OR OTHER MEANS SHOWING THE THRESHOLD ELEVATION FOR SEDIMENT CLEANOUT. PRIOR TO THE REMOVAL OF SEDIMENTS, DEWATER THE BASIN THROUGH PUMPING OR OTHER MEANS TO EXPOSE PREVIOUSLY SUBMERGED SEDIMENTS. DO NOT ALLOW SEDIMENT TO FLOSH INTO THE DRAINAGEWAY. STOCKPILE THE SEDIMENT IN SUCH A MANNER THAT IT WILL NOT ERODE FROM THE SITE OR INTO A WETLAND, WATERCOURSE OR OTHER SENSITIVE AREA.

TEMPORARY SEDIMENT BASIN BOTTOM SHALL BE 2 FEET ABOVE THE PROPOSED BOTTOM OF THE PERMANENT STORMWATER BASIN. THE STORMWATER BASIN SHALL BE EXCAVATED TO DESIGN GRADES ONLY AFTER ALL UPGRADED AREAS HAVE BEEN STABILIZED AND BEFORE FINAL PAVING.

DEWATERING:

BMP DESCRIPTION/INSTALLATION: IN THE EVENT GROUNDWATER IS ENCOUNTERED DURING CONSTRUCTION, DEWATERING MAY BE REQUIRED THROUGH THE USE OF SUMP PUMPS. INSTALLATION OF SUMPS SHALL FOLLOW THE REQUIREMENTS OF THE SUMP PIT. THE PURPOSE OF THIS PRACTICE IS TO REMOVE EXCESSIVE WATER FROM EXCAVATIONS IN A MANNER THAT IMPROVES THE QUALITY OF THE WATER BEING PUMPED. PUMPED WATER SHALL BE DISCHARGED TO AN APPROVED FILTERING SYSTEM.

CONSTRUCTION SPECIFICATIONS

SUMP PIT

- 1. A PERFORATED VERTICAL STANDPIPE SHALL BE PLACED IN THE CENTER OF THE PIT TO COLLECT FILTERED WATER. THE STANDPIPE SHALL BE SLOTTED OR PERFORATED CORRUGATED METAL OR PVC PIPE AND ITS DIAMETER AND NUMBER OF PERFORATIONS SHALL BE COMPATIBLE WITH THE PUMP SIZE BEING USED.
2. WATER SHALL THEN BE PUMPED FROM THE CENTER OF THE PIPE TO A SUITABLE DISCHARGE AREA (SEDIMENT FILTER BAG OR DEWATERING SETTLING BASIN).
3. THE PIT SHALL BE FILLED WITH CRUSHED STONE OR GRAVEL NO SMALLER THAN CT DOT #67 SIZE NOR LARGER THAN CT DOT #1 SIZE. CRUSHED STONE SHALL EXTEND A MINIMUM OF 12" BELOW THE BOTTOM OF THE STANDPIPE.
4. DISCHARGE OF WATER PUMPED FROM THE STANDPIPE SHALL BE TO A SUITABLE PRACTICE SUCH AS A SEDIMENT FILTER BAG OR AN APPROVED DEWATERING SETTLING BASIN.
5. FILTER FABRIC SHALL BE WRAPPED AROUND THE STANDPIPE TO ENSURE CLEAN WATER DISCHARGE. IT IS RECOMMENDED THAT 1/4 TO 1/2 INCH HARDWARE CLOTH WIRE MESH BE WRAPPED AROUND AND SECURED TO THE STANDPIPE PRIOR TO ATTACHING THE FILTER FABRIC. THIS WILL INCREASE THE RATE OF WATER SEEPAGE INTO THE STANDPIPE.

SOIL STABILIZATION:

TEMPORARY STABILIZATION:

BMP DESCRIPTION: HYDROMULCHING WILL BE USED ON SLOPES WHERE CONSTRUCTION WILL CEASE FOR MORE THAN 14 DAYS AND OVER THE WINTER MONTHS TO STABILIZE ERODIBLE MATERIALS. HAY/STRAW MULCH AND WOOD FIBER WILL BE MIXED WITH A TACKIFIER AND APPLIED UNIFORMLY BY MACHINE WITH AN APPLICATION RATE OF 2 TONS (100-200 BALES) PER ACRE. THE CONTRACTOR WILL USE CRIMPING EQUIPMENT TO BIND THE MULCH TO THE SOIL IF THE TACKIFIER IS NOT EFFECTIVE. NETTING WILL BE USED ON SMALL AREAS WITH STEEP SLOPES. IN AREAS WHERE HYDROMULCHING IS INACCESSIBLE, HAY/STRAW MULCH WILL BE APPLIED BY HAND AT THE SAME APPLICATION RATE. TEMPORARY SEEDING WILL BE USED ON ANY AREA WHERE CONSTRUCTION ACTIVITY IS SUSPENDED FOR MORE THAN TWENTY-ONE DAYS TO STABILIZE ERODIBLE MATERIALS. SEE BELOW FOR GUIDANCE ON SEEDING MIXTURES, RATES, AND ACCEPTABLE PLANTING DATES FOR TEMPORARY SEEDING.

INSTALLATION SCHEDULE: PORTIONS OF THE SITE WHERE CONSTRUCTION ACTIVITIES WILL TEMPORARILY CEASE FOR MORE THAN 14 DAYS WILL BE STABILIZED WITH MULCH. WHERE CONSTRUCTION ACTIVITIES WILL TEMPORARILY CEASE FOR MORE THAN 21 DAYS IT WILL BE TEMPORARILY SEEDED. WATER STABILIZATION WILL BE PROVIDED BETWEEN DECEMBER 25 AND MARCH 30.

MAINTENANCE AND INSPECTION: MULCHED AREAS WILL BE INSPECTED WEEKLY TO ENSURE THAT ADEQUATE COVERAGE IS PROVIDED. REPAIRS WILL BE CONDUCTED AS NEEDED.

SEED MIXTURE FOR TEMPORARY SEEDING

Table with 3 columns: PERENNIAL RYEGRASS, SEED MIXTURE FOR TEMPORARY SEEDING, LBS./ACRE, LBS./1000 S.F. Values: 40, 1.0

SEE FIGURE TS-2 IN THE 2002 GUIDELINES FOR ADDITIONAL TEMPORARY SEED MIXES.

FINAL STABILIZATION:

PERMANENT SEEDING SHOULD BE APPLIED IMMEDIATELY AFTER THE FINAL DESIGN GRADES ARE ACHIEVED AT THE SITE BUT NO LATER THAN 14 DAYS AFTER THE PERMANENT SEEDING IS FINALLY CEASED. AFTER THE ENTIRE SITE IS STABILIZED, ANY SEDIMENT THAT HAS ACCUMULATED SHALL BE REMOVED AND HAULED OFF SITE. CONSTRUCTION DEBRIS, TRASH, AND TEMPORARY BMP'S SHALL ALSO BE REMOVED AND ANY AREAS DISTURBED DURING REMOVAL SHALL BE SEEDDED IMMEDIATELY.

SEEDBED PREPARATION:

- 1. TOPSOIL WILL BE SPREAD OVER FINAL GRADED AREAS AT A MINIMUM DEPTH OF FOUR INCHES. TOPSOIL SHALL INCLUDESIVELY MEAN A SOIL MEETING ONE OF THE FOLLOWING SOIL TEXTURAL CLASSES ESTABLISHED BY THE UNITED STATES DEPARTMENT OF AGRICULTURE CLASSIFICATION SYSTEM BASED UPON THE PROPORTION OF SAND, SILT AND CLAY SIZE PARTICLES. AFTER PASSING A 2 MILLIMETER (MM) SIEVE AND SUBJECTED TO A PARTICLE SIZE ANALYSIS:
1.1. LOAMY SAND, INCLUDING COARSE, LOAMY FINE, AND LOAMY VERY FINE SAND, SANDY LOAM, INCLUDING COARSE, FINE AND VERY FINE SANDY LOAM, LOAM, OR SILT LOAM WITH NO MORE THAN 60% SILT;
1.2. CONTAINING NOT LESS THAN 6% AND NOT LESS THAN 20% ORGANIC MATTER AS DETERMINED BY LOSS-ON-IGNITION OF OVEN DRIED SAMPLES DRIED AT 105 DEGREES CENTIGRADE;

- 1.3. POSSESSING A PH RANGE OF 6.0-7.5, EXCEPT IF THE VEGETATIVE PRACTICE BEING USED SPECIFICALLY REQUIRES A LOWER PH, THEN PH MAY BE ADJUSTED ACCORDINGLY;
1.4. HAVING SOLUBLE SALTS NOT EXCEEDING 500 PPM;
1.5. AND THAT IS LOOSE AND FRABLE AND FREE FROM REFUSE, STUMPS, ROOTS, BRUSH, WEEDS, FROZEN PARTICLES, ROCKS, AND STONES OVER 1.25 INCHES IN DIAMETER, AND ANY MATERIAL THAT WILL PREVENT THE FORMATION OF A SUITABLE SEEDBED OR PREVENT SEED GERMINATION AND PLANT GROWTH.
2. FERTILIZER WILL BE APPLIED TO THE SEEDBED AS NEEDED. FERTILIZERS WILL BE COMMERCIAL TYPE OF UNIFORM COMPOSITION, FREE-FLOWING AND CONFORMING TO THE APPLICABLE STATE AND FEDERAL LAWS. CHOOSE NATIVE SPECIES THAT ARE ADAPTED TO LOCAL WEATHER AND SOIL CONDITIONS WHEREVER POSSIBLE TO REDUCE WATER AND FERTILIZER INPUTS AND LOWER MAINTENANCE OVERALL.
3. TOPSOIL WILL BE LOOSENEED BY RAKING, TILLING OR OTHER SUITABLE METHODS.
FINAL STABILIZATION SHOULD BE INSTALLED ON PORTIONS OF THE SITE WHERE CONSTRUCTION ACTIVITIES HAVE PERMANENTLY CEASED BUT NO LATER THAN 14 DAYS AFTER CONSTRUCTION CEASES.

SEED MIXTURE FOR LAWN AREAS

Table with 3 columns: KENTUCKY BLUEGRASS, CREEPING RED FESCUE, PERENNIAL RYEGRASS, LBS./ACRE, LBS./1000 S.F. Values: 20, 0.45, 5, 1.0

SEED MIXTURE FOR STORMWATER BASINS

Table with 3 columns: NEW ENGLAND EROSION CONTROL/RESTORATION MIX FOR DETENTIONS BASINS BY NEW ENGLAND WETLAND PLANTS, INC. OF AMHERST, MA, LBS./ACRE, LBS./1000 S.F. Values: 35, 0.80

SPECIES: RIVERBANK WILD RYE (ELYMUS RIPARIUS), CREEPING RED FESCUE (FESTUCA RUBRA), LITTLE BLUESTEM (SCHIZACHYRIUM SCOPARIUM), BIG BLUESTEM (ANDROPOGON GERARDII), SWITCH GRASS (PANICUM VIRGATUM), UPLAND BENTGRASS (AGROSTIS PERENNANS), NODDING BUR MARIGOLD (BIDENS CERNUA), HOLLOW-STEM JOE PYE WEED (EUPATORIUM FISTULOSUM/EUTROCHIUM FISTULOSUM), NEW ENGLAND ASTER (ASTER NOVAE-ANGLIAE), BONESET (EUPATORIUM PERFORIATUM), BLUE VERVAIN (VERBENA HASTATA), SOFT RUSH (JUNCUS EFFUSUS), WOOL GRASS (SCIRPUS CYPERNUS).

THE NEW ENGLAND EROSION CONTROL/RESTORATION MIX FOR DETENTION BASINS CONTAINS A SELECTION OF NATIVE GRASSES AND WILDFLOWERS DESIGNED TO COLON

**SPILL PREVENTION AND CONTROL
BEST MANAGEMENT PRACTICES (BMP'S) DESCRIPTION:**

1. MATERIAL HANDLING AND WASTE MANAGEMENT:

WASTE MATERIALS:

ALL WASTE MATERIALS WILL BE COLLECTED AND DISPOSED OF INTO METAL WASTE DUMPSTERS IN DESIGNATED AREAS. DUMPSTERS WILL HAVE A SECURE TIGHT LID, BE PLACED AWAY FROM STORM WATER DRAINS AND STRUCTURES, AND WILL MEET ALL FEDERAL, STATE, AND LOCAL REGULATIONS. ONLY TRASH AND CONSTRUCTION DEBRIS SHALL BE PLACED IN THE DUMPSTERS. CONSTRUCTION MATERIALS SHALL NOT BE BURIED ON SITE.

HAZARDOUS WASTE MATERIALS:

BMP DESCRIPTION: ALL HAZARDOUS WASTE MATERIALS INCLUDING OIL FILTERS, PETROLEUM PRODUCTS, PAINT, AND EQUIPMENT MAINTENANCE FLUIDS SHALL BE STORED IN STRUCTURALLY SOUND AND SEALED SHIPPING CONTAINERS IN A DESIGNATED AREA. HAZARDOUS WASTE MATERIALS SHALL BE STORED IN APPROPRIATE AND CLEARLY MARKED CONTAINERS AND SEGREGATED FROM OTHER NON-WASTE MATERIALS. SECONDARY CONTAINMENT SHALL BE PROVIDED FOR ALL WASTE MATERIALS IN A DESIGNATED AREA AND SHALL CONSIST OF COMMERCIALY AVAILABLE SPILL PALLETS OR EQUAL. ADDITIONALLY, ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL REGULATIONS.

HAZARDOUS WASTE MATERIALS:

BMP DESCRIPTION: ALL HAZARDOUS WASTE MATERIALS INCLUDING OIL FILTERS, PETROLEUM PRODUCTS, PAINT, AND EQUIPMENT MAINTENANCE FLUIDS SHALL BE STORED IN STRUCTURALLY SOUND AND SEALED SHIPPING CONTAINERS IN A DESIGNATED AREA. HAZARDOUS WASTE MATERIALS SHALL BE STORED IN APPROPRIATE AND CLEARLY MARKED CONTAINERS AND SEGREGATED FROM OTHER NON-WASTE MATERIALS. SECONDARY CONTAINMENT SHALL BE PROVIDED FOR ALL WASTE MATERIALS IN A DESIGNATED AREA AND SHALL CONSIST OF COMMERCIALY AVAILABLE SPILL PALLETS OR EQUAL. ADDITIONALLY, ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL REGULATIONS.

HAZARDOUS WASTE MATERIALS: HAZARDOUS WASTE MATERIALS SHALL NOT BE DISPOSED OF INTO THE ON-SITE DUMPSTERS. **MAINTENANCE AND INSPECTION:** THE HAZARDOUS WASTE MATERIALS AREA SHALL BE INSPECTED WEEKLY AND AFTER STORM EVENTS. THE STORAGE AREA SHALL BE KEPT CLEAN, WELL ORGANIZED AND EQUIPPED WITH AMPLIFIED CLEANUP SUPPLIES AS APPROPRIATE FOR THE MATERIALS BEING STORED. SAFETY DATA SHEETS, MATERIAL INVENTORY, AND EMERGENCY CONTACT NUMBERS SHALL BE MAINTAINED IN THE PROJECT OFFICE.

SANITARY WASTE:

BMP DESCRIPTION: PORTABLE TOILETS, LOCATED IN THE STAGING AREA, SHALL BE PROVIDED AT THE SITE THROUGHOUT THE CONSTRUCTION PHASE. THE TOILETS SHALL BE LOCATED AWAY FROM CONCENTRATED DRAINAGE FLOW PATHS AND SHALL HAVE COLLECTION PANS UNDERNEATH AS SECONDARY CONTAINMENT.

MAINTENANCE AND INSPECTION:

SANITARY WASTE SHALL BE COLLECTED A MINIMUM OF ONCE A WEEK AND SHALL BE INSPECTED WEEKLY FOR EVIDENCE OF LEAKING HOLDING TANKS.

RECYCLING:

BMP DESCRIPTION: WOOD PALLETS, CARDBOARD BOXES, AND OTHER RECYCLABLE CONSTRUCTION SCRAPS SHALL BE DISPOSED OF IN A DESIGNATED DUMPSTER FOR RECYCLING. THE DUMPSTER SHALL HAVE A SECURE WATERTIGHT LID, BE PLACED AWAY FROM STORMWATER CONVEYANCES AND DRAINS AND MEET ALL LOCAL AND STATE SOLID-WASTE MANAGEMENT REGULATIONS. ONLY SOLID RECYCLABLE CONSTRUCTION SCRAPS FROM THE SITE SHALL BE DEPOSITED IN THE DESIGNATED DUMPSTER.

2. DESIGNATE WASHOUT AREAS:

CONCRETE WASHOUT

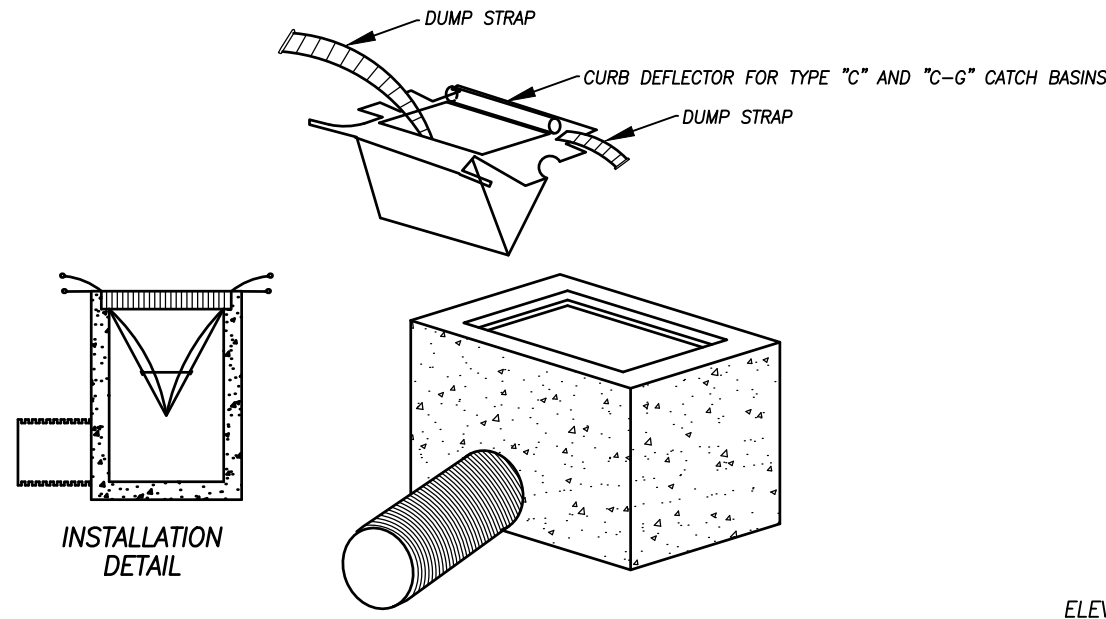
BMP DESCRIPTION: A DESIGNATED TEMPORARY, ABOVE-GRADE CONCRETE WASHOUT AREA SHALL BE CONSTRUCTED FOR CONCRETE WASHOUT. THE WASHOUT AREA SHALL BE LINED WITH PLASTIC SHEETING AT LEAST 10 MILS THICK AND REINFORCED WITH STEEL REBAR. CONCRETE POURS WILL NOT BE CONDUCTED DURING OR BEFORE AN ANTICIPATED STORM EVENT. CONCRETE MIXER TRUCKS AND CHUTES SHALL BE WASHED IN THE DESIGNATED WASHOUT AREA OR CONCRETE WASTES SHALL BE PROPERLY DISPOSED OF OFF-SITE. WHEN THE TEMPORARY WASHOUT AREA IS NO LONGER NEEDED FOR THE CONSTRUCTION PROJECT, THE HARDENED CONCRETE AND MATERIALS USED TO CONSTRUCT THE AREA WILL BE REMOVED AND DISPOSED OF IN ACCORDANCE WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL REGULATIONS, AND THE AREA SHALL BE STABILIZED.

INSTALLATION SCHEDULE: THE WASHOUT AREA SHALL BE CONSTRUCTED BEFORE CONCRETE POURS OCCUR AT THE SITE.

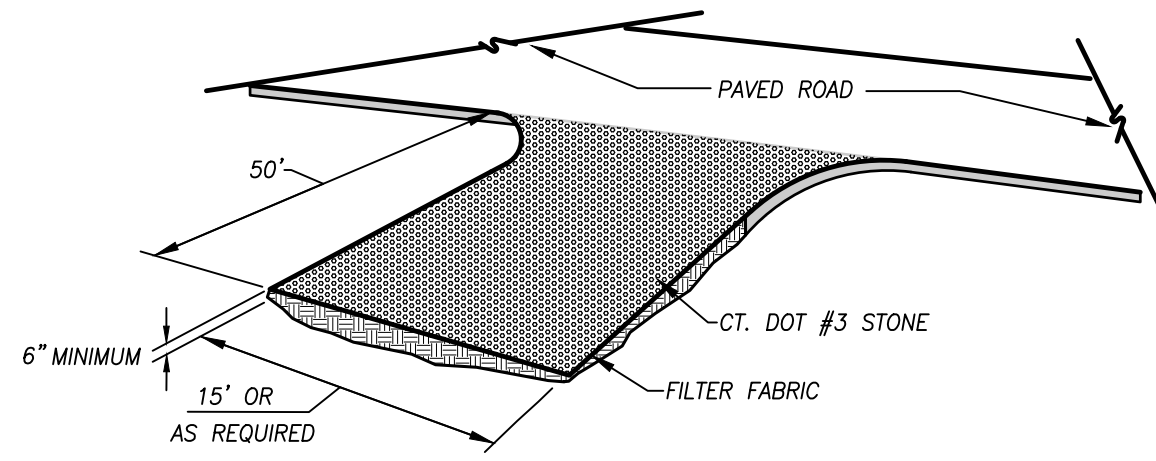
3. VEHICLE FUELING AND MAINTENANCE PRACTICES:

BMP DESCRIPTION: SEVERAL TYPES OF VEHICLES AND EQUIPMENT WILL BE USED ON-SITE THROUGHOUT THE PROJECT, INCLUDING GRADERS, EXCAVATORS, LOADERS, ROLLERS, TRUCKS AND TRAILERS, AND BACKHOES. EQUIPMENT MAINTENANCE AND FUELING SHALL BE PERFORMED IN THE STAGING AREA. THIS PROPOSED ACTIVITY SHALL BE SITUATED SO THAT DRAINAGE FACILITIES OR WATER COURSES LOCATED IN THE AREA ARE NOT AT RISK FROM POTENTIAL INFILTRATION, ABSORBENT, SPILL-CLEANUP MATERIALS AND SPILL KITS SHALL BE AVAILABLE AT THE COMBINED STAGING AND MATERIALS STORAGE AREA. FUEL SHALL BE DELIVERED TO THE SITE ON AN AS NEEDED BASIS BY A FUEL DELIVERY SERVICE. FUELING AND MINOR MAINTENANCE OF EQUIPMENT WILL ONLY OCCUR IN DESIGNATED FUELING AREAS ON AN IMPERVIOUS SURFACE. VEHICLE AND EQUIPMENT WASHING IS PROHIBITED ON SITE.

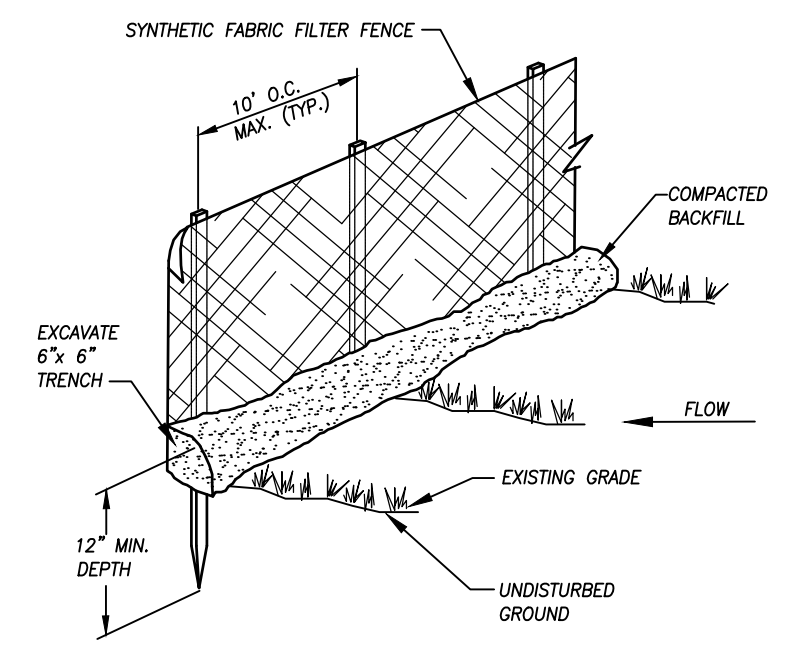
INSTALLATION SCHEDULE: BMP'S IMPLEMENTED FOR FUELING ACTIVITIES SHALL BEGIN AT THE START OF THE PROJECT.



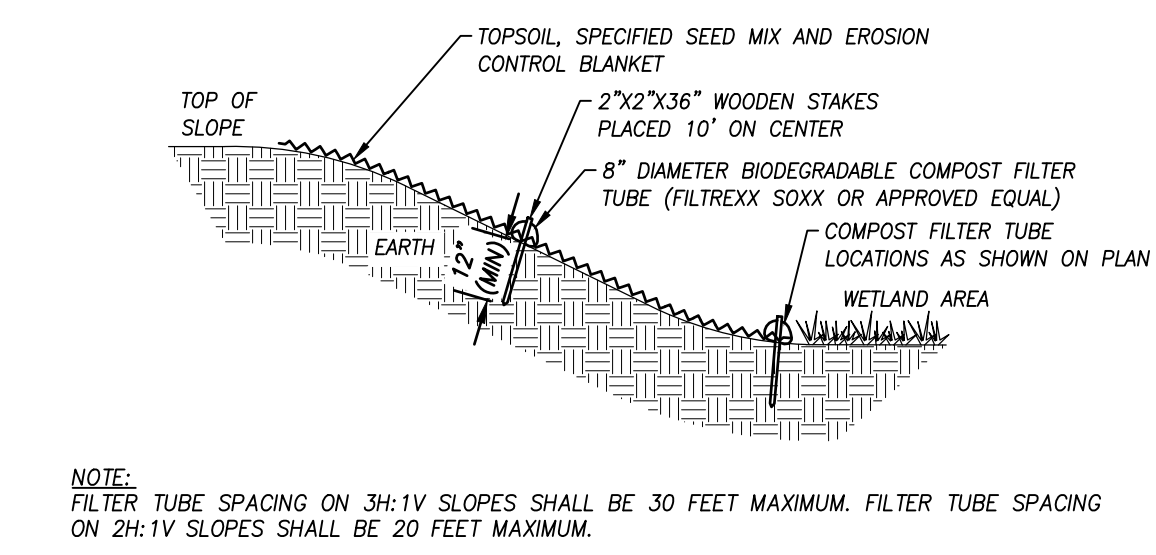
INLET SEDIMENT CONTROL DEVICE
NOT TO SCALE



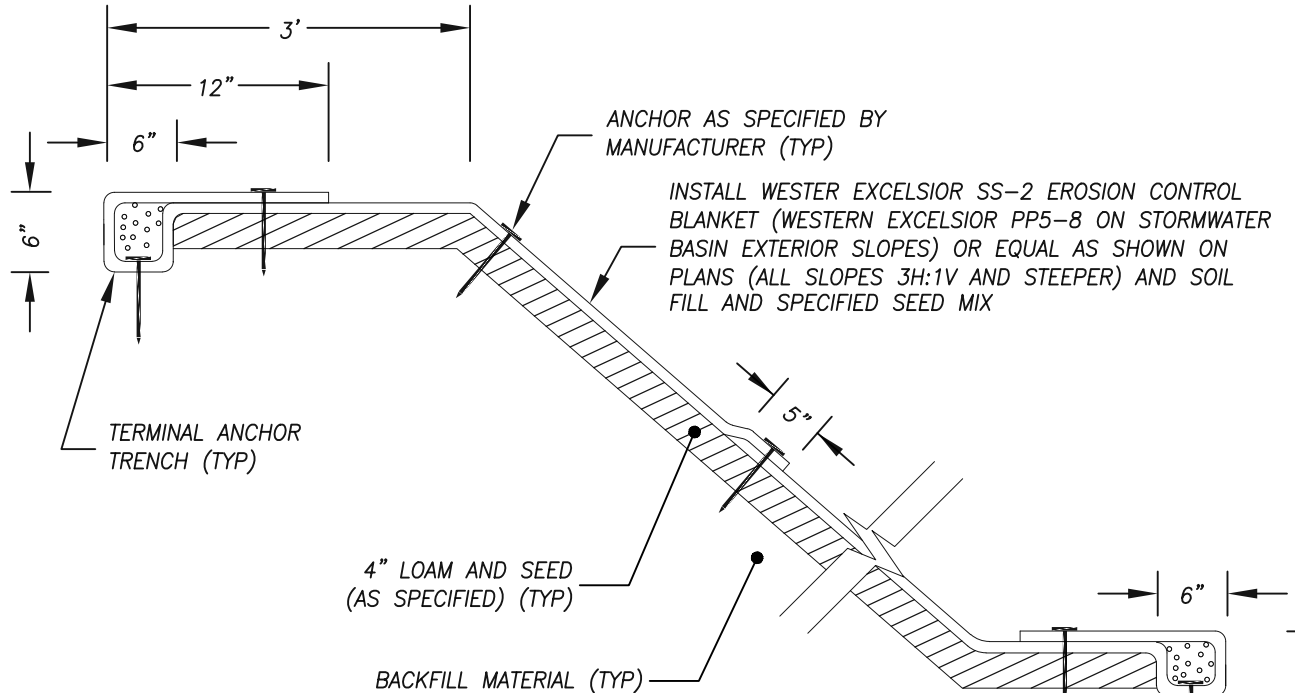
ANTI-TRACKING PAD
NOT TO SCALE



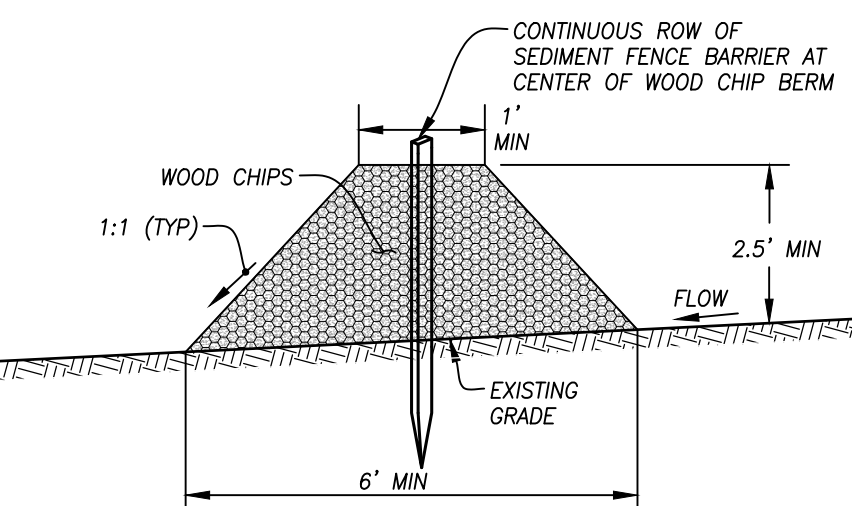
SEDIMENT FENCE DETAIL
NOT TO SCALE



COMPOST FILTER TUBE INSTALLATION DETAIL
NOT TO SCALE



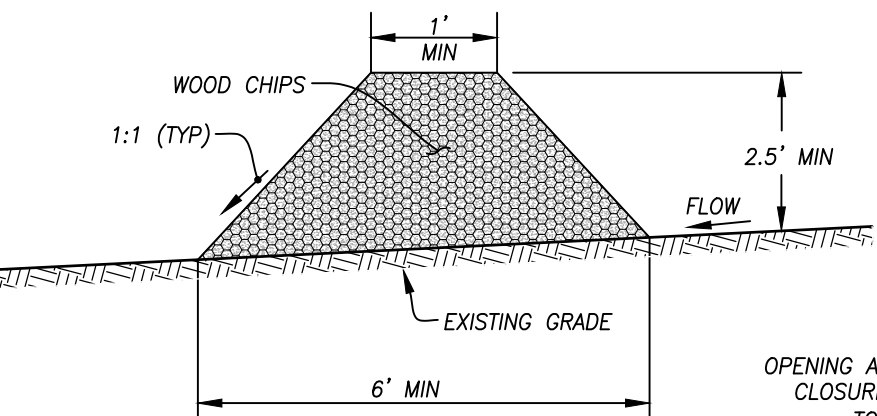
EROSION CONTROL BLANKET DETAIL
NOT TO SCALE



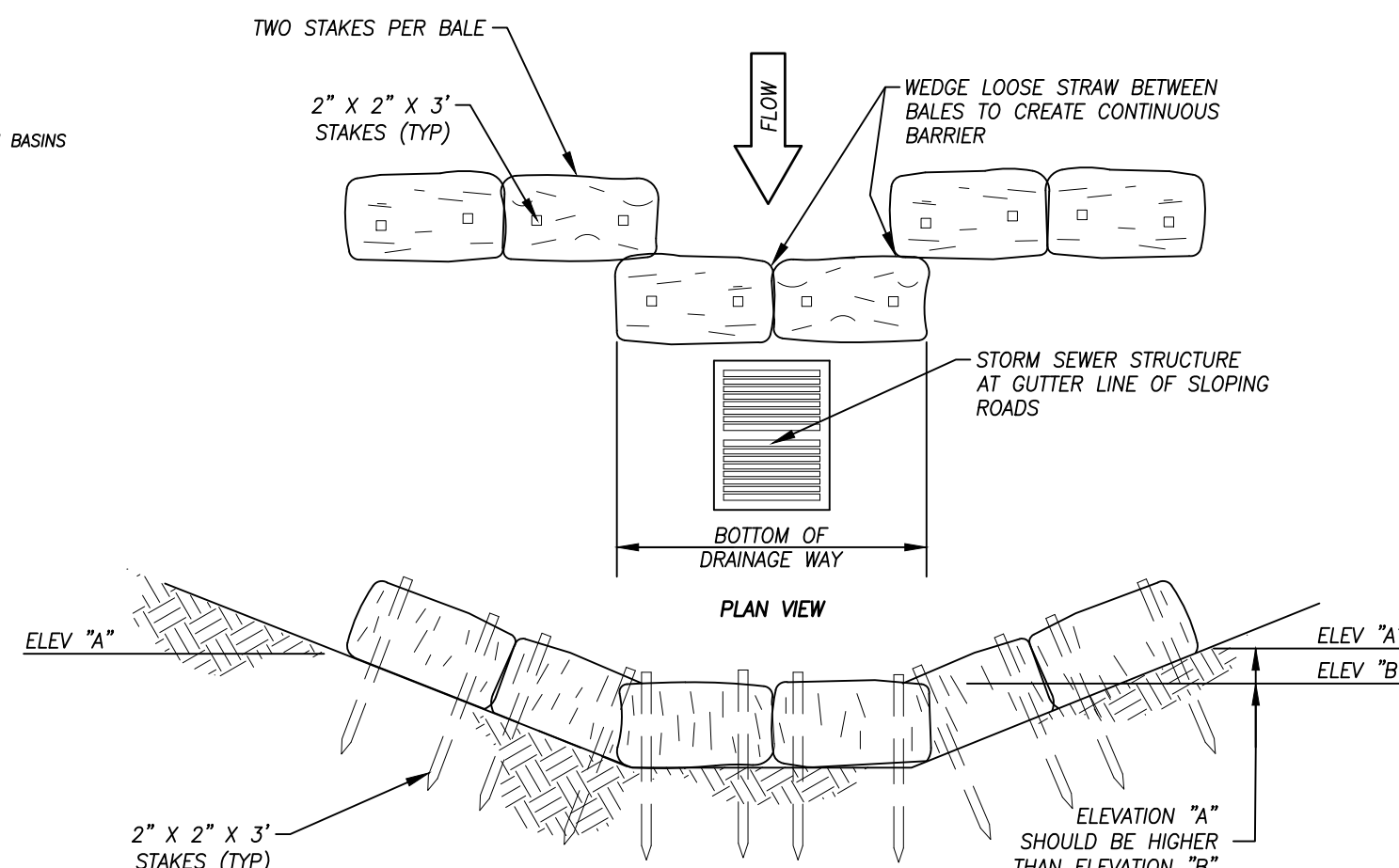
WOOD CHIP BERM WITH SEDIMENT FENCE DETAIL
NOT TO SCALE



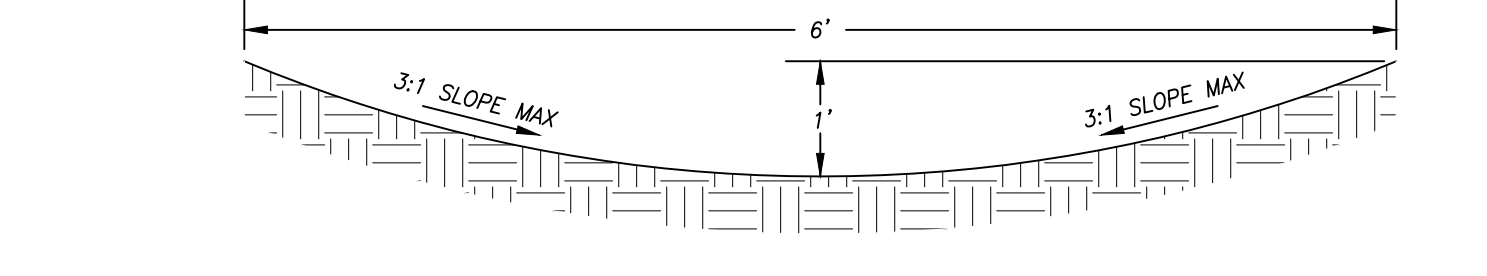
COMPOST FILTER TUBE DETAIL
NOT TO SCALE



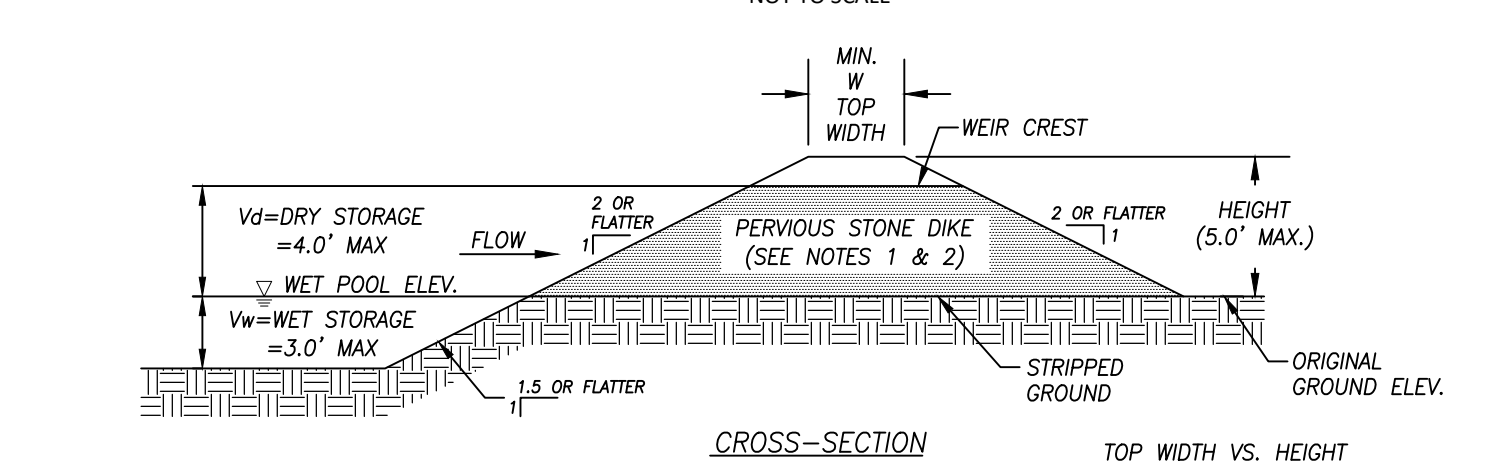
WOOD CHIP BERM DETAIL
NOT TO SCALE



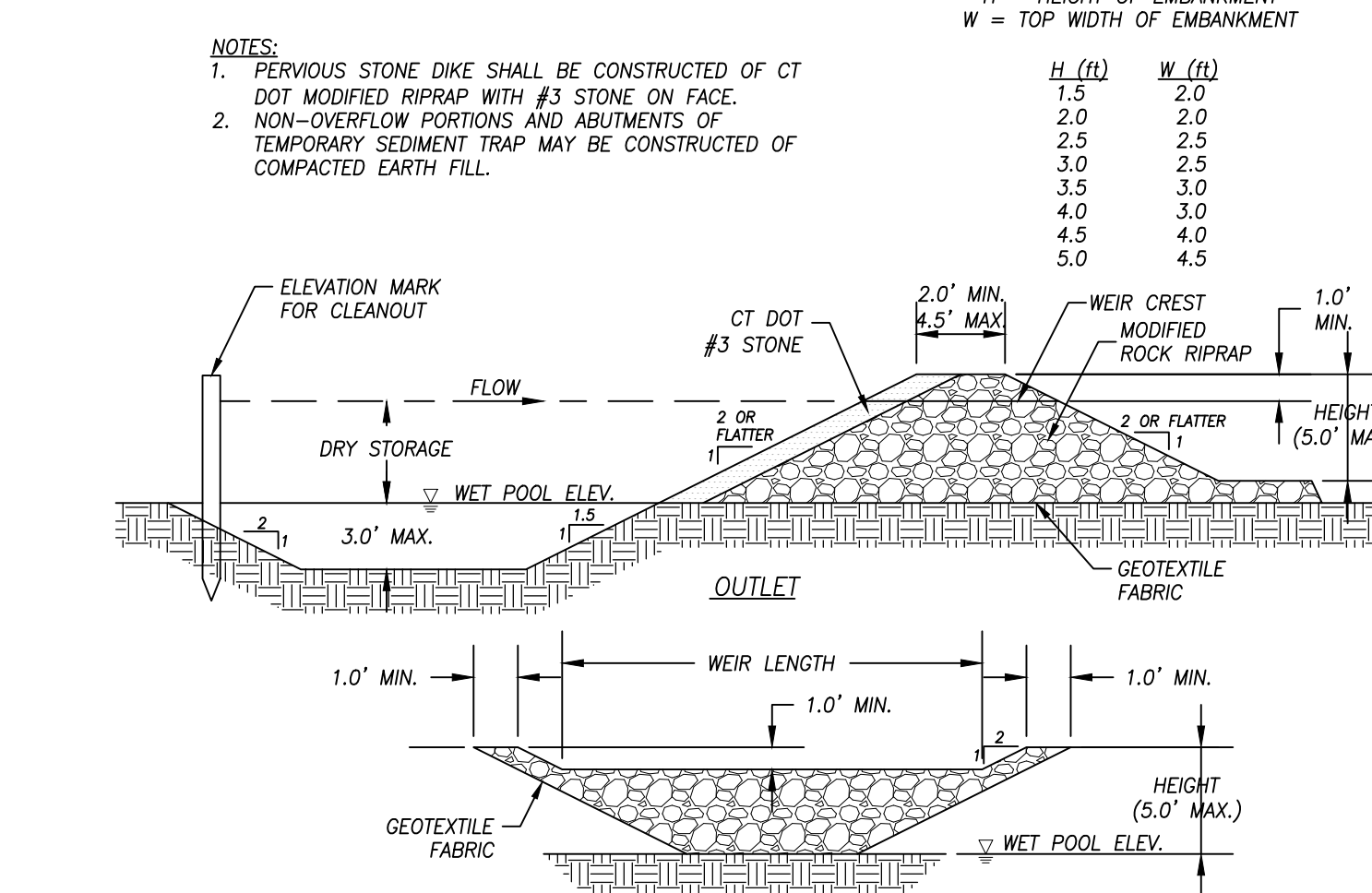
HAY BALE CHECK DAM
NOT TO SCALE



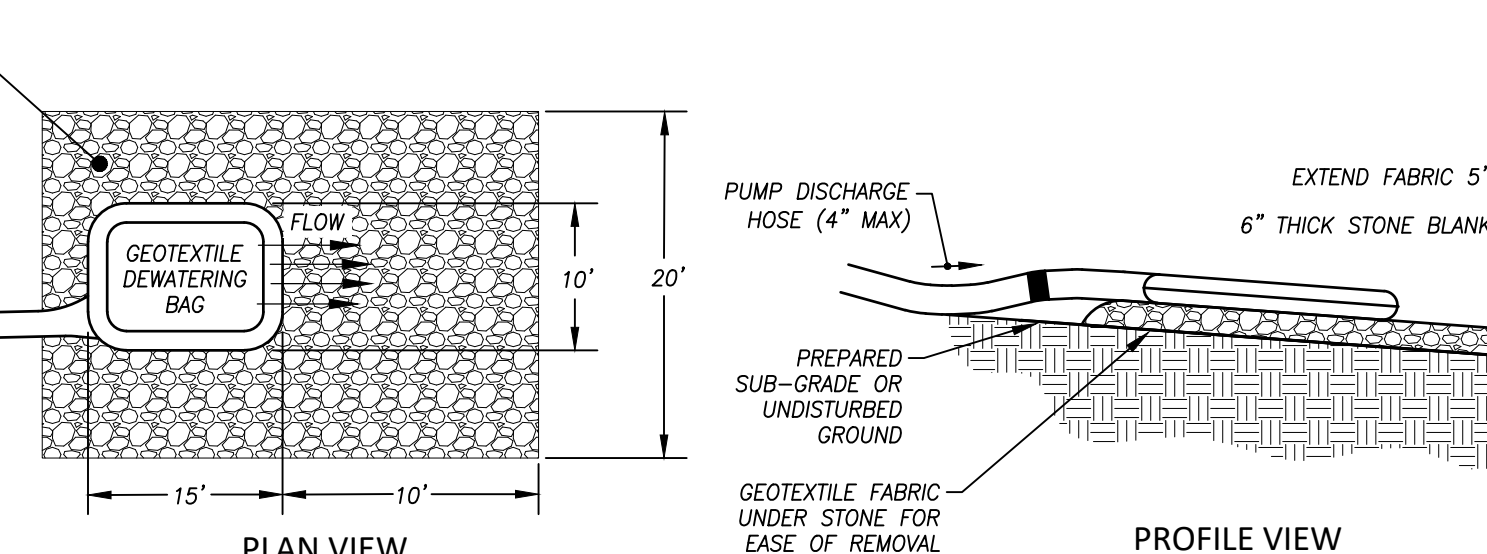
DIVERSION SWALE DETAIL
NOT TO SCALE



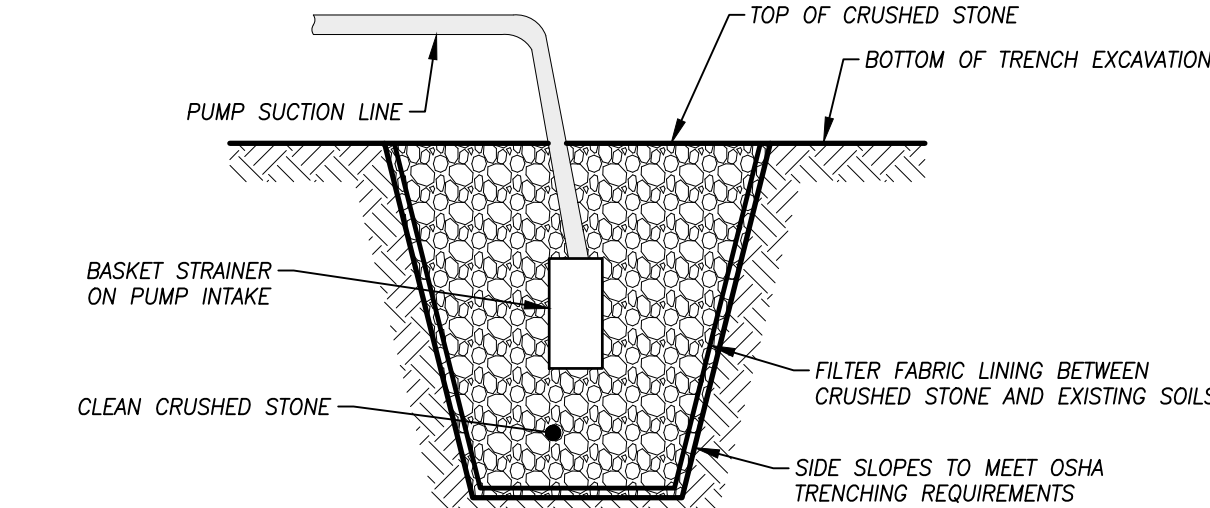
TYPICAL PUMP SETTLING BASIN DETAIL
NOT TO SCALE



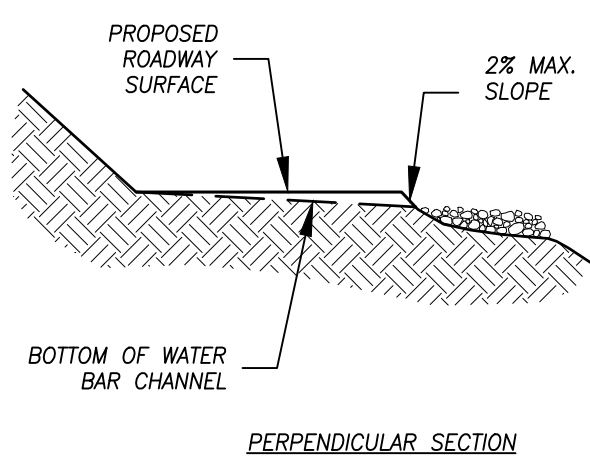
DETAIL FOR TEMPORARY SEDIMENT TRAPS 3 AND 4
NOT TO SCALE



GEOTEXTILE DEWATERING BAG
NOT TO SCALE



TYPICAL PUMP INTAKE DETAIL
NOT TO SCALE



WATER BAR DETAIL
NOT TO SCALE

NOTES:
1. THE CONTRACTOR SHALL SIZE BASIN BASED ON THE SELECTED PUMP DISCHARGE FLOWS, AND ENLARGE AS NECESSARY AT NO ADDITIONAL COST TO THE OWNER, TO ALLOW FOR PROPER FUNCTION OF THE BASIN.
2. ALTERNATE PUMPING, SETTLING BASIN OR FRACTIONATION TANKS MAY BE USED WITH PRIOR APPROVAL OF THE ENGINEER.

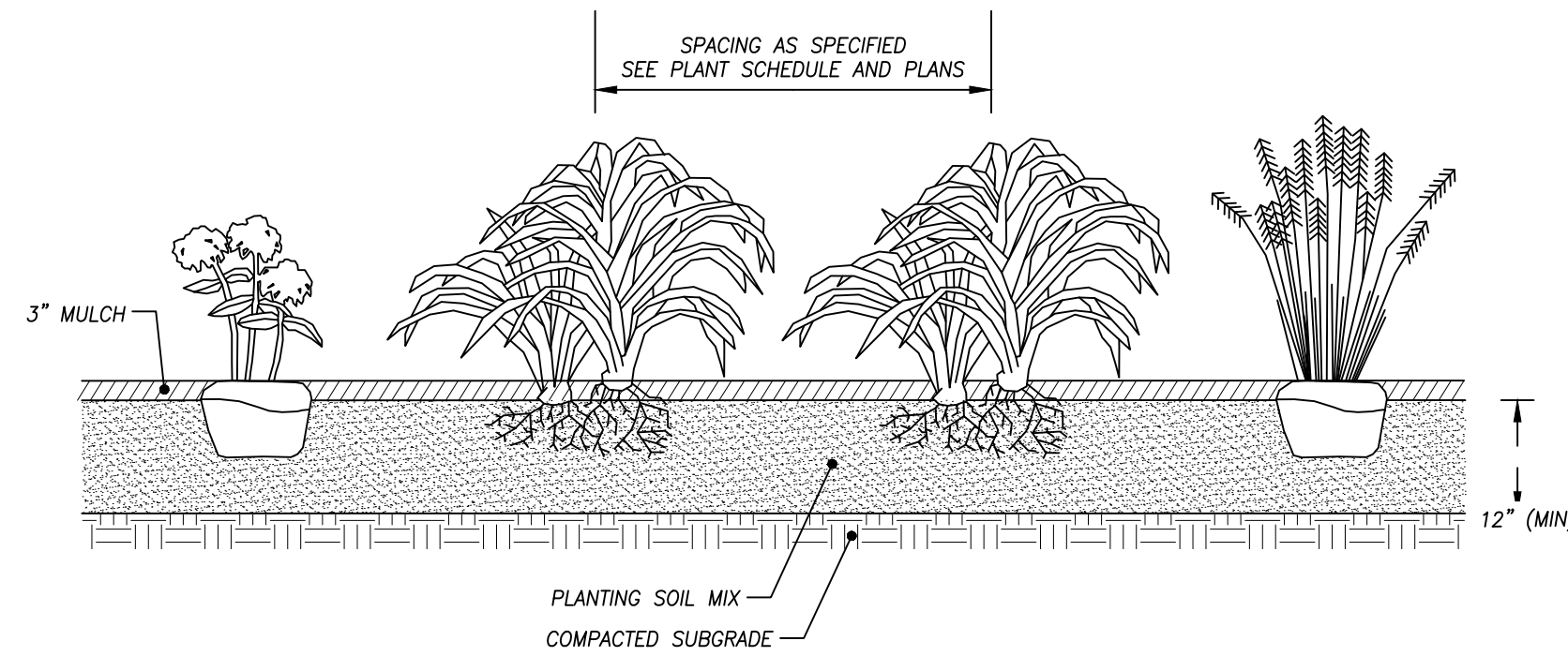
NOTES:
1. THE CONTRACTOR SHALL SIZE SUMP BASED ON THE SELECTED PUMP DISCHARGE FLOWS, AND ENLARGE AS NECESSARY AT NO ADDITIONAL COST TO THE OWNER, TO ALLOW FOR PROPER FUNCTION OF THE SUMP.
2. MINIMUM SUMP DIMENSIONS ARE 2' DEEP (MEASURED FROM THE BOTTOM OF THE TRENCH EXCAVATION) AND 2' DIAMETER.
3. CRUSHED STONE SHALL BE NO SMALLER THAN CT DOT #67 SIZE NOR LARGER THAN CT DOT #3 SIZE.
4. SUMPS SHALL BE EXCAVATED AND RELOCATED AS REQUIRED TO MAINTAIN A DRY EXCAVATION.
5. ALTERNATE PUMP INTAKE PROTECTION AND DEWATERING METHODS MAY BE USED WITH PRIOR APPROVAL OF THE ENGINEER.

NOTES:
TYPICALLY, SEDIMENT TRAPS ARE REQUIRED FOR ANY DISCHARGE POINT THAT SERVES AN AREA BETWEEN 2 AND 5 DISTURBED ACRES OF LAND. ALL TEMPORARY SEDIMENT TRAPS SHALL BE DESIGNED IN CONFORMANCE WITH THE "2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL". GENERALLY, TEMPORARY SEDIMENT TRAPS SHALL BE SIZED TO PROVIDE A MINIMUM OF 1.54 CUBIC YARDS OF WATER STORAGE PER ACRE DRAINED. ALL TEMPORARY SEDIMENT TRAPS SHALL BE MAINTAINED TO ASSURE EFFICIENT OPERATION UNTIL THE CONTRIBUTING AREA IS COMPLETELY STABILIZED. TEMPORARY SEDIMENT TRAPS MAY BE RELOCATED DURING CONSTRUCTION TO ACCOMMODATE PHASING. CONTRACTOR SHALL REVIEW LOCATIONS OF TEMPORARY SEDIMENT TRAPS WITH DESIGN ENGINEER PRIOR TO INSTALLATION. NO TEMPORARY SEDIMENT TRAP SHALL HAVE MORE THAN 5 ACRES OF DISTURBED LAND CONTRIBUTING TO IT.

NOTES:
1. GEOTEXTILE BAG MATERIAL SHALL BE A NON-WOVEN MATERIAL.
2. DO NOT OVER PRESSURIZE BAG OR USE BEYOND CAPACITY.
3. LOCATE DISCHARGE SITE ON FLAT UPLAND AREAS AS FAR AWAY AS POSSIBLE FROM STREAMS, WETLANDS, AND OTHER RESOURCES AND POINTS OF CONCENTRATED FLOW.
4. DOWNGRADIENT FROM RECEIVING AREA MUST BE WELL VEGETATED OR OTHERWISE STABLE FROM EROSION, E.G., FOREST FLOOR OR COARSE GRAVEL/STONE.

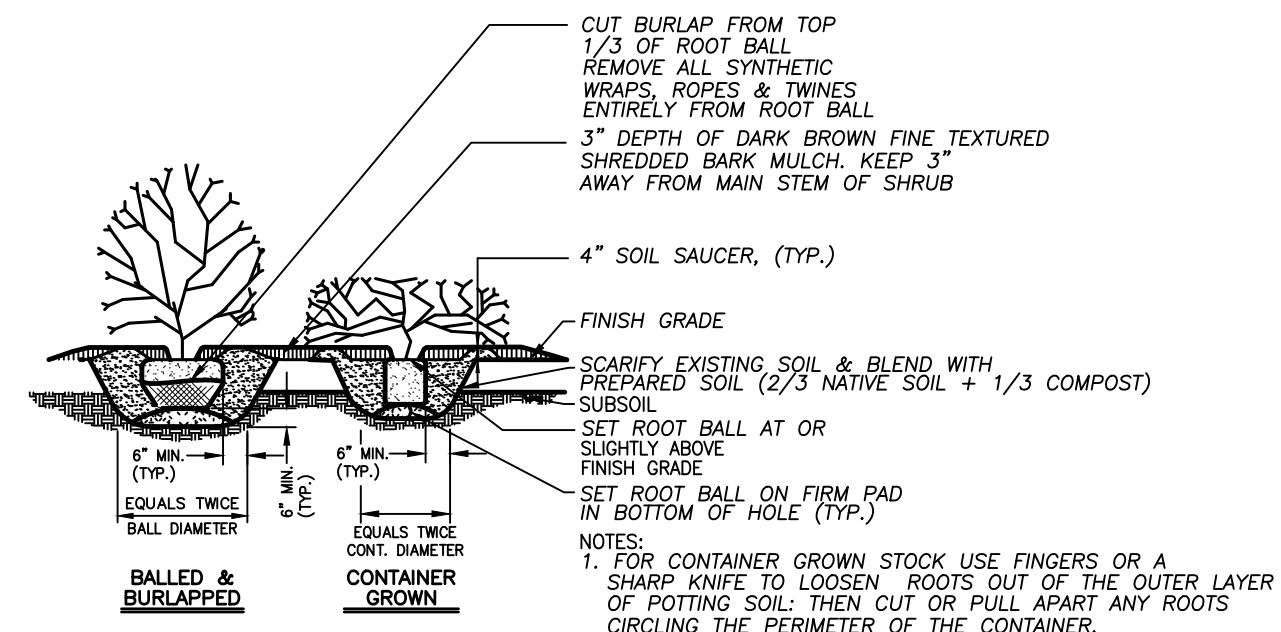
PLAN NOTES
1. SEE COVER SHEET FOR ENGINEER AND SURVEYOR SIGNATURES AND SEALS.
2. SEE SHEET 2 FOR LEGEND & ABBREVIATIONS.

NOT FOR CONSTRUCTION
1/15/2021



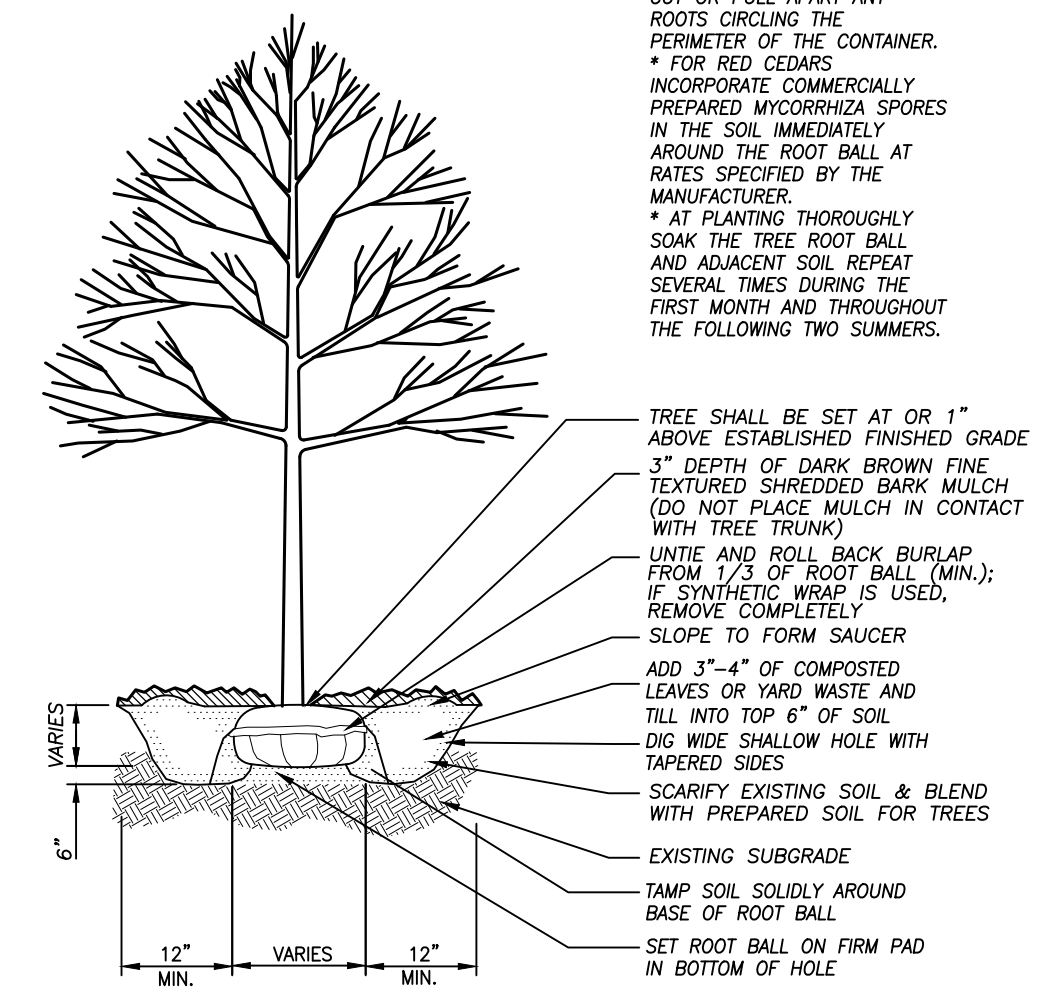
- NOTES:**
1. ROTOTILL FERTILIZER AND LIME INTO SOIL PRIOR TO PLANTING IN ACCORDANCE WITH SOIL ANALYSIS RECOMMENDATIONS.
 2. DO NOT OVER-COMPACT PLANTING BED. WATER THOROUGHLY AFTER PLANTING.
 3. ADJUST PLANTING DEPTH AS RECOMMENDED BY SUPPLIER.
 4. MULCH SHALL NOT COME INTO CONTACT WITH CROWNS OF PERENNIALS.

PERENNIAL/GROUNDCOVER PLANTING DETAIL
NOT TO SCALE



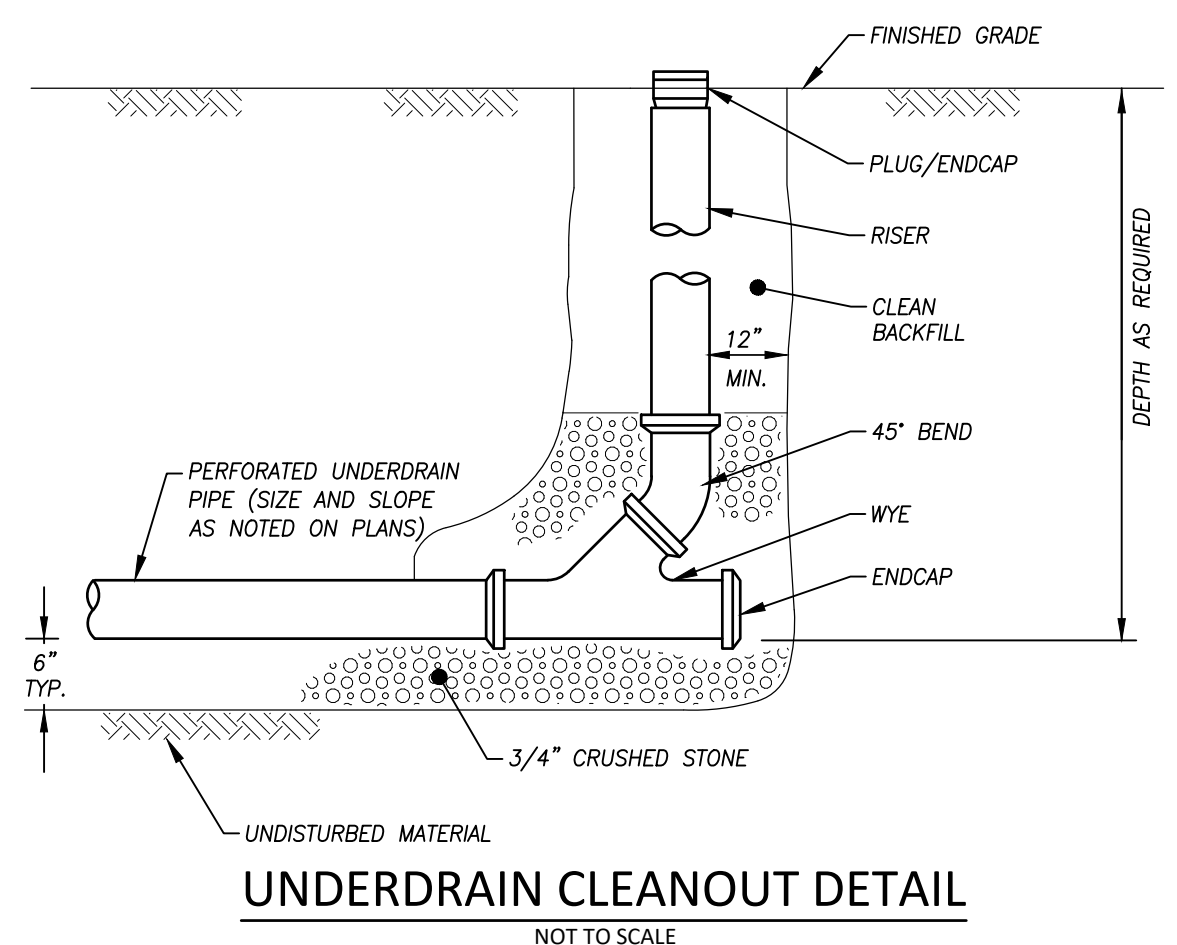
- NOTES:**
1. FOR CONTAINER-GROWN STOCK USE FINGERS OR A SHARP KNIFE TO LOOSEN ROOTS OUT OF THE OUTER LAYER OF POTTING SOIL; THEN CUT OR PULL APART ANY ROOTS CIRCLING THE PERIMETER OF THE CONTAINER.
 2. AT PLANTING THOROUGHLY SOAK THE ROOT MASS AND ADJACENT SOIL. REPEAT SEVERAL TIMES DURING THE FIRST MONTH AND THROUGHOUT THE FOLLOWING TWO SUMMERS.

SHRUB PLANTING DETAIL
NOT TO SCALE

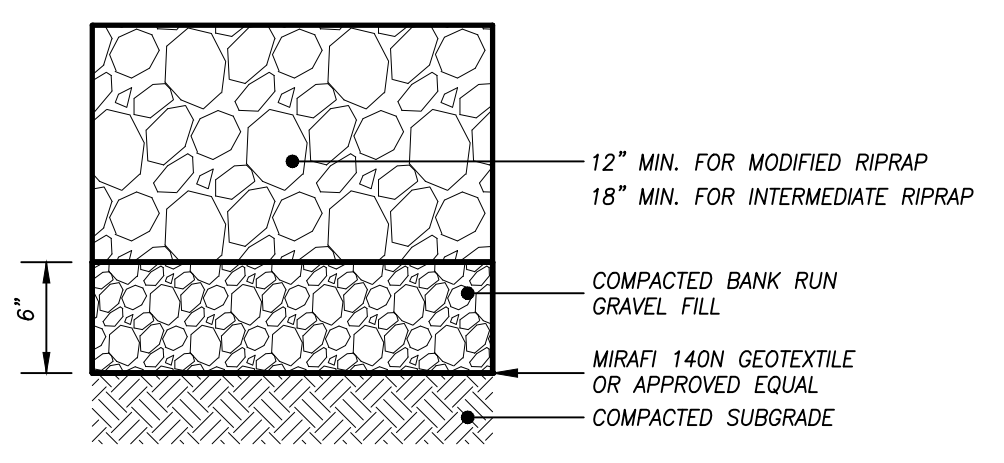


- NOTES:**
- * DO NOT STAKE OR WRAP TRUNK.
 - * FOR CONTAINER-GROWN TREES, USE FINGERS OR SMALL HAND TOOLS TO PULL THE ROOTS OUT OF THE OUTER LAYER OF POTTING SOIL; THEN CUT OR PULL APART ANY ROOTS CIRCLING THE PERIMETER OF THE CONTAINER.
 - * FOR RED CEDARS INCORPORATE COMMERCIALY PREPARED MYCORRHIZA SPORES IN THE SOIL IMMEDIATELY AROUND THE ROOT BALL AT RATES SPECIFIED BY THE MANUFACTURER.
 - * AT PLANTING THOROUGHLY SOAK THE TREE ROOT BALL AND ADJACENT SOIL REPEAT SEVERAL TIMES DURING THE FIRST MONTH AND THROUGHOUT THE FOLLOWING TWO SUMMERS.

TREE PLANTING DETAIL
NOT TO SCALE

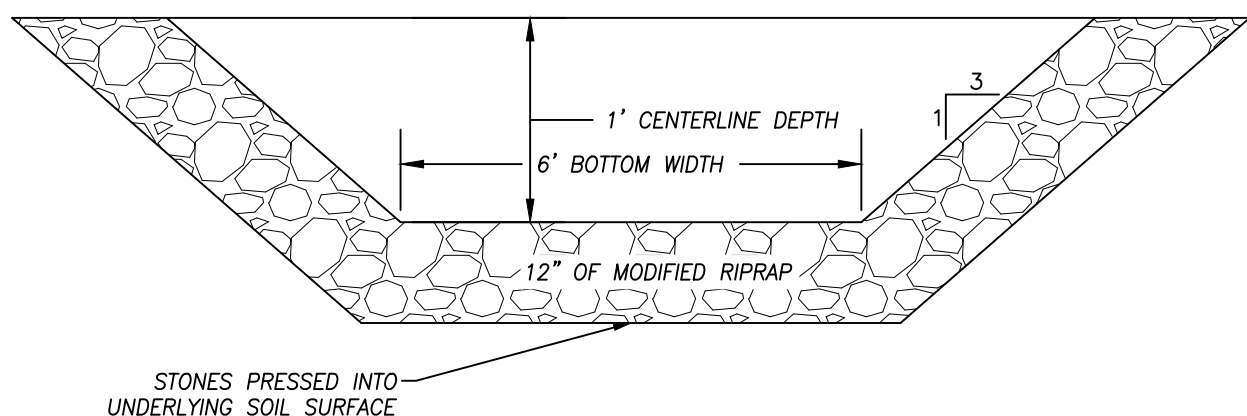


UNDERDRAIN CLEANOUT DETAIL
NOT TO SCALE

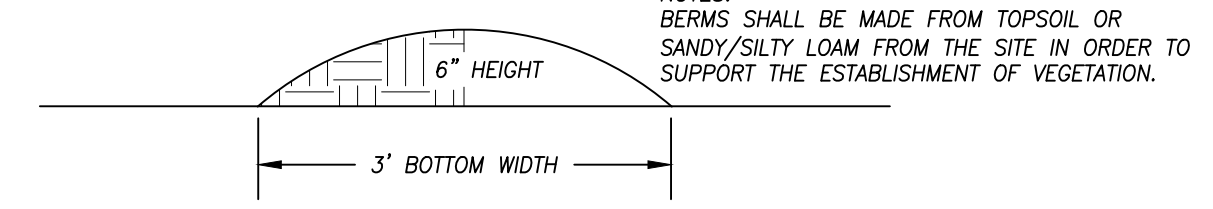


- NOTES:**
1. TO BE USED AT PIPE DISCHARGES AND RIP RAP SWALE. SEE PLAN FOR APRON DIMENSIONS.

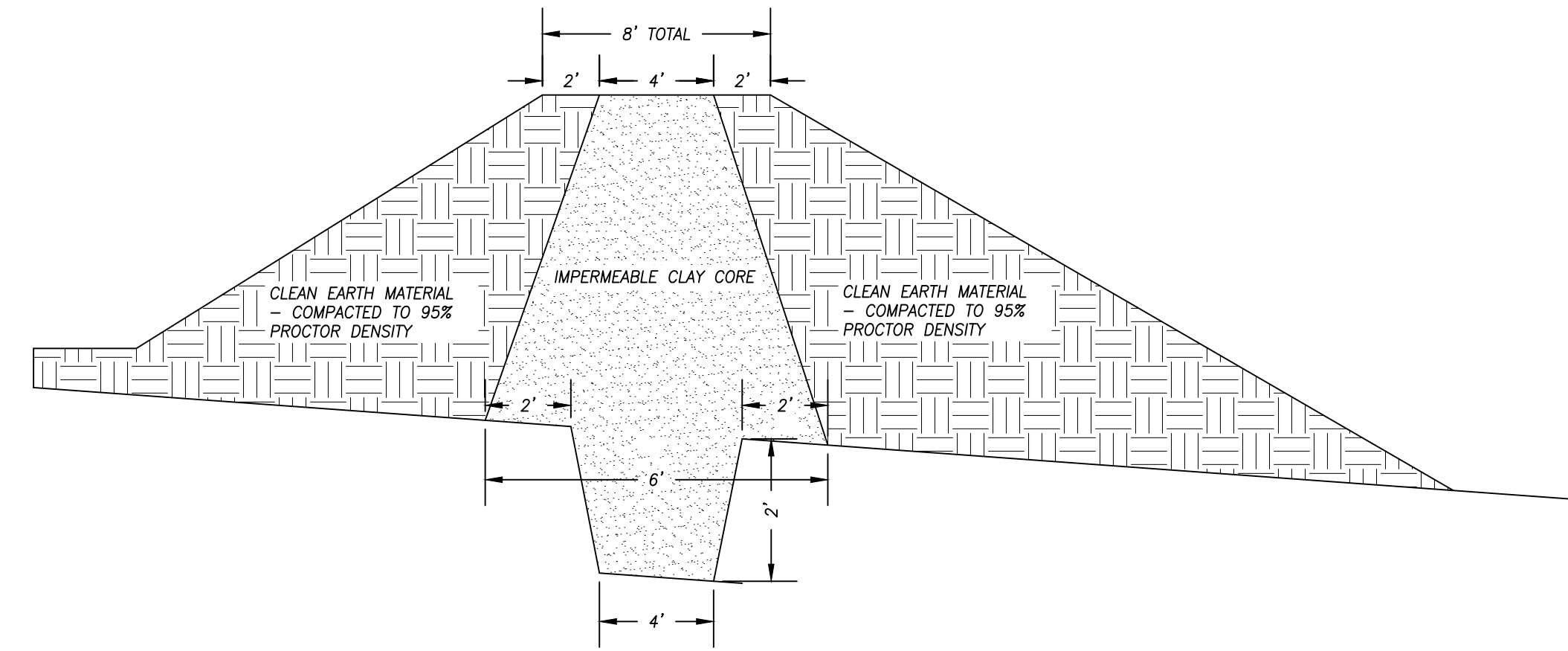
TYPICAL RIPRAP SECTION
NOT TO SCALE



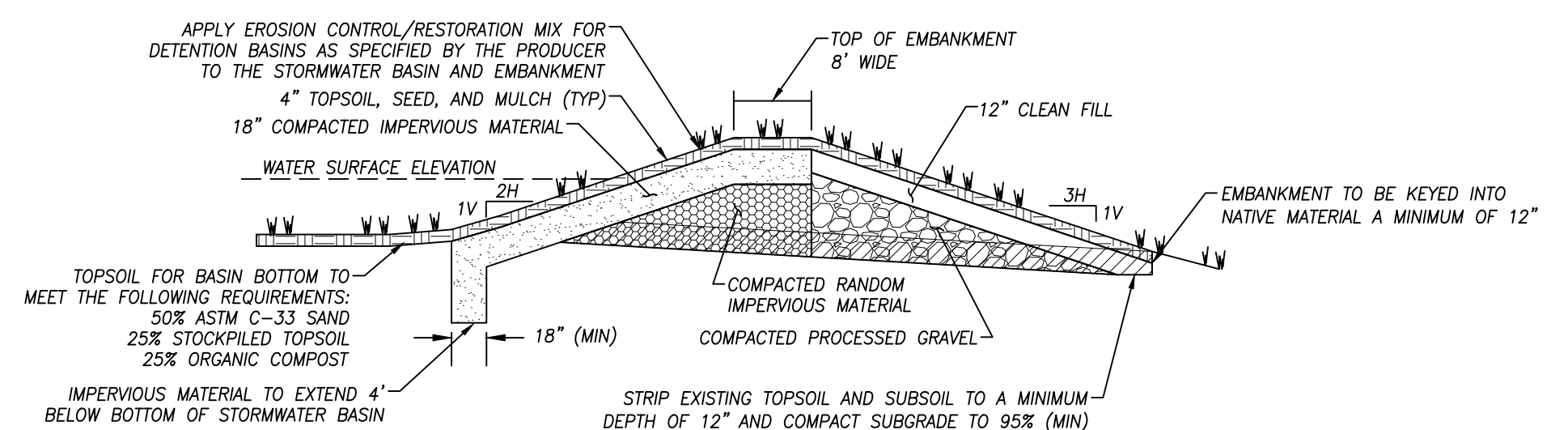
MODIFIED RIP RAP SWALE DETAIL
NOT TO SCALE



DETAIL OF EARTH BERMS IN CONSTRUCTED WETLAND SYSTEM
NOT TO SCALE



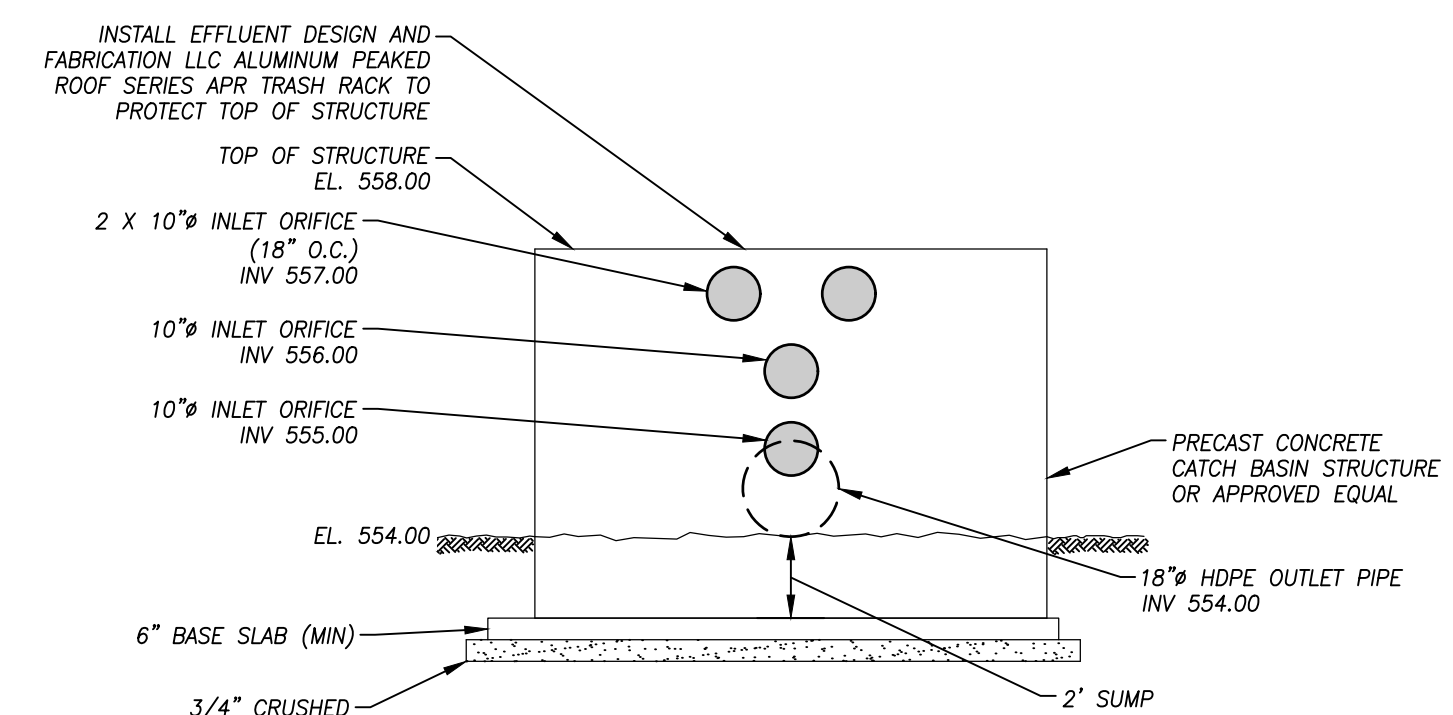
SECTION THROUGH STORMWATER BASIN 1 EMBANKMENT SHOWING IMPERMEABLE CORE
NOT TO SCALE



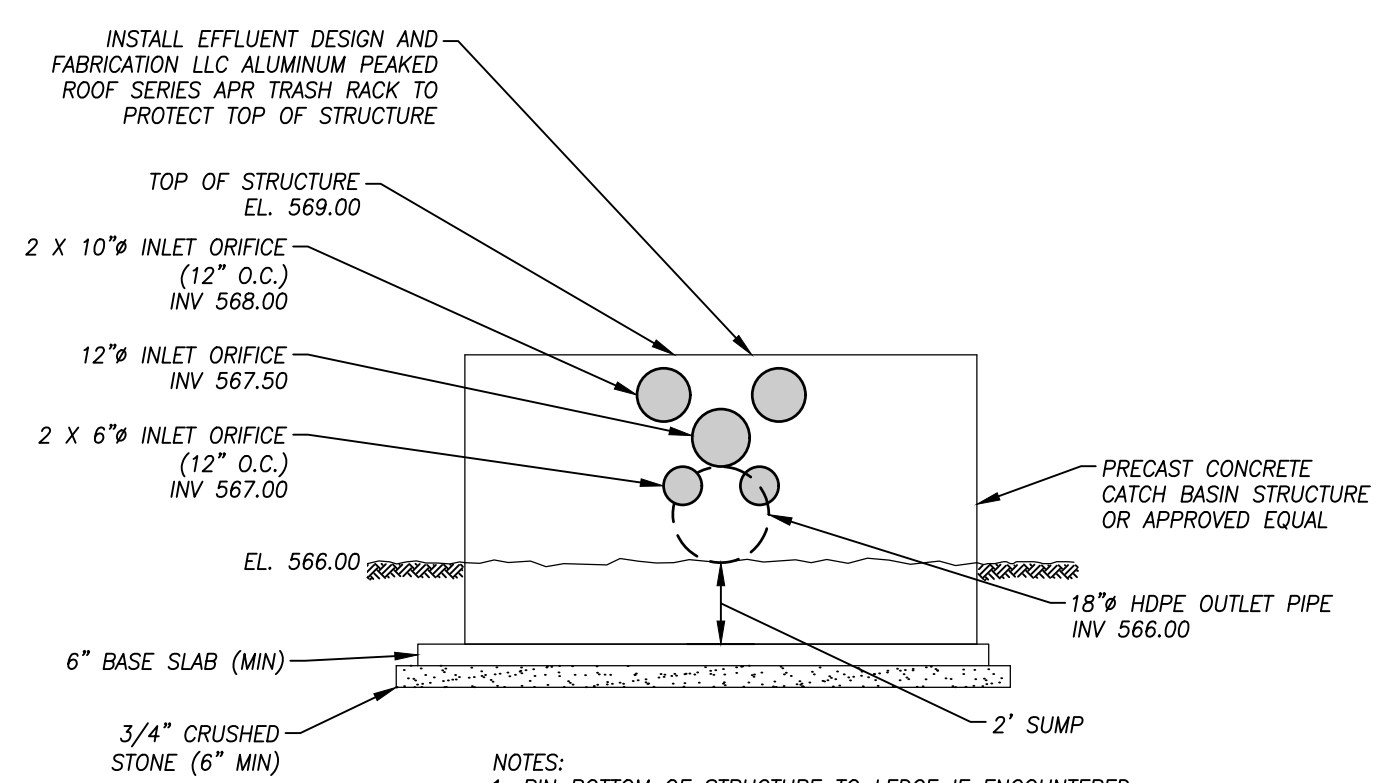
- NOTES:**
1. REMOVE VEGETATION, DEBRIS, ORGANIC MATERIALS, AND TOPSOIL TO A MINIMUM OF 12" BELOW EXISTING GRADE PRIOR TO EMBANKMENT CONSTRUCTION. COMPACTED EXPOSED SUBSOIL AND SCARIFY SURFACE.
 2. FILL MATERIALS SHALL BE PLACED IN LIFTS NOT EXCEEDING 12". PRIOR TO COMPACTION EACH LIFT SHALL BE MOISTENED AS NECESSARY TO ACHIEVE THE OPTIMUM MOISTURE CONTENT. THE TOP 12" OF SUBGRADE AND EACH LIFT SHALL BE COMPACTED TO 95% OF MAXIMUM DENSITY AT OPTIMUM MOISTURE CONTENT AS DETERMINED IN ACCORDANCE WITH ASTM D1557. FILL MATERIAL SHALL NOT BE PLACED ON SURFACES THAT ARE MUDDY, FROZEN, OR CONTAINING FROST, ICE, OR ORGANICS.
 3. CLEAN FILL MATERIAL SHALL BE FREE OF ORGANICS AND NO STONES GREATER THAN 3".
 4. PROCESSED GRAVEL SHALL MEET THE REQUIREMENTS OF CT DOT FORM 817 M.02.06 GRADATION A.
 5. IMPERVIOUS MATERIAL SHALL BE DENSE GRADED AND HAVE A PERMEABILITY RATE OF 1 X 10⁻⁴ CM/SEC OR LESS, HAVE A PERCENTAGE OF MATERIALS PASSING THE NO. 200 SIEVE OF GREATER THAN 10%, AND AN EFFECTIVE GRAIN SIZE DIAMETER (D10) OF 0.05 MM OR LESS. IT SHALL BE FREE OF ORGANICS AND SHALL HAVE NO STONES GREATER THAN 2".
 6. RANDOM IMPERVIOUS MATERIAL SHALL BE DENSE GRADED AND FREE OF ORGANICS WITH NO STONES LARGER THAN 2". MATERIAL SHALL MEET ONE OF THE FOLLOWING GRADATIONS:

Sieve Size	Percent Passing	1-1/4" Processed Aggregate	2" Processed Aggregate
2-1/2"	100	100	100
2"	100	96	96
1-1/2"	99	91	91
1"	61	67	67
3/4"	51	58	58
1/4"	40	33	33
#40	16	15	15
#200	7	5	5

STORMWATER BASIN 2 EMBANKMENT DETAIL
NOT TO SCALE



OUTLET CONTROL STRUCTURE 1
NOT TO SCALE



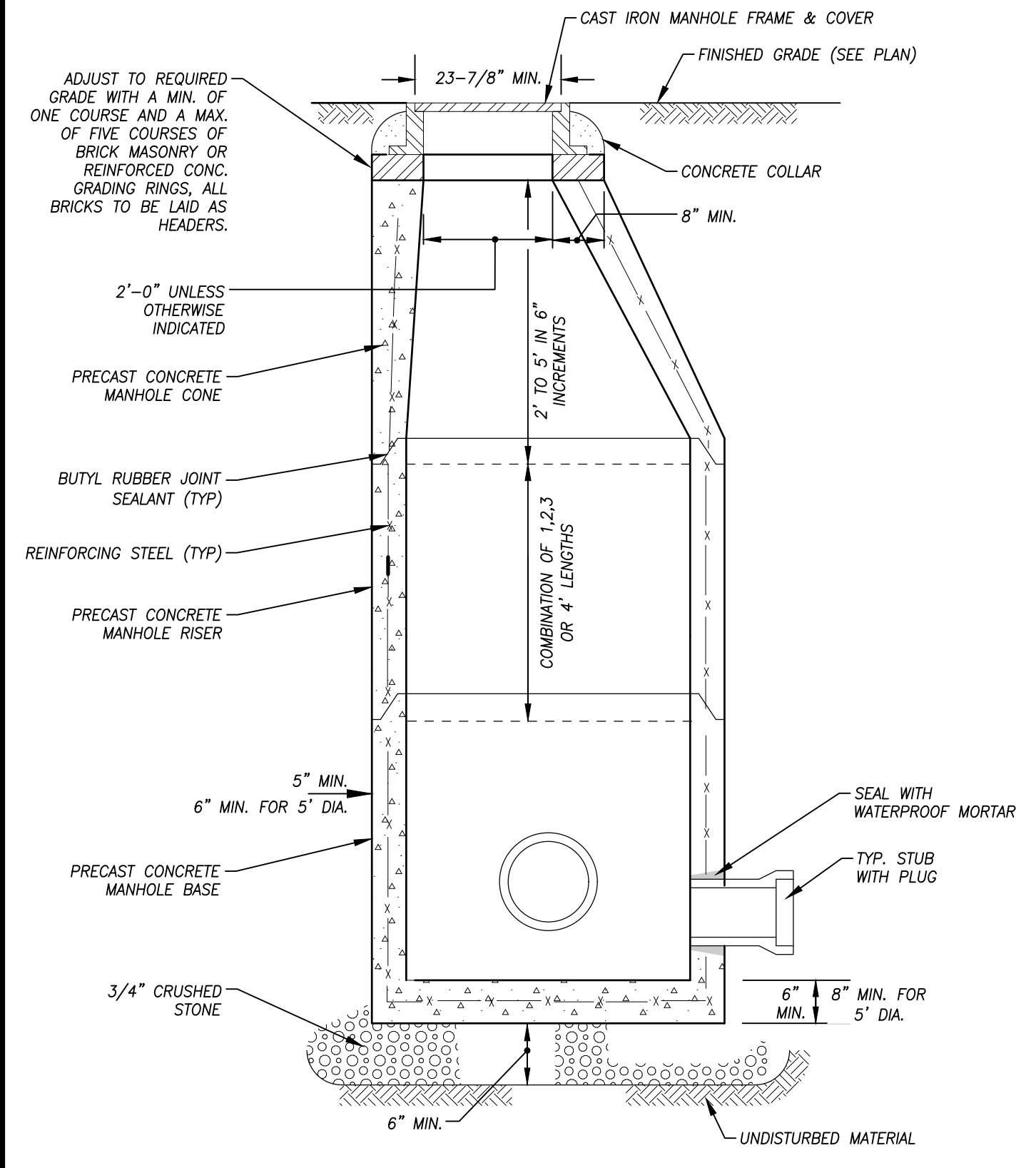
OUTLET CONTROL STRUCTURE 2
NOT TO SCALE

NOT FOR CONSTRUCTION
1/15/2021

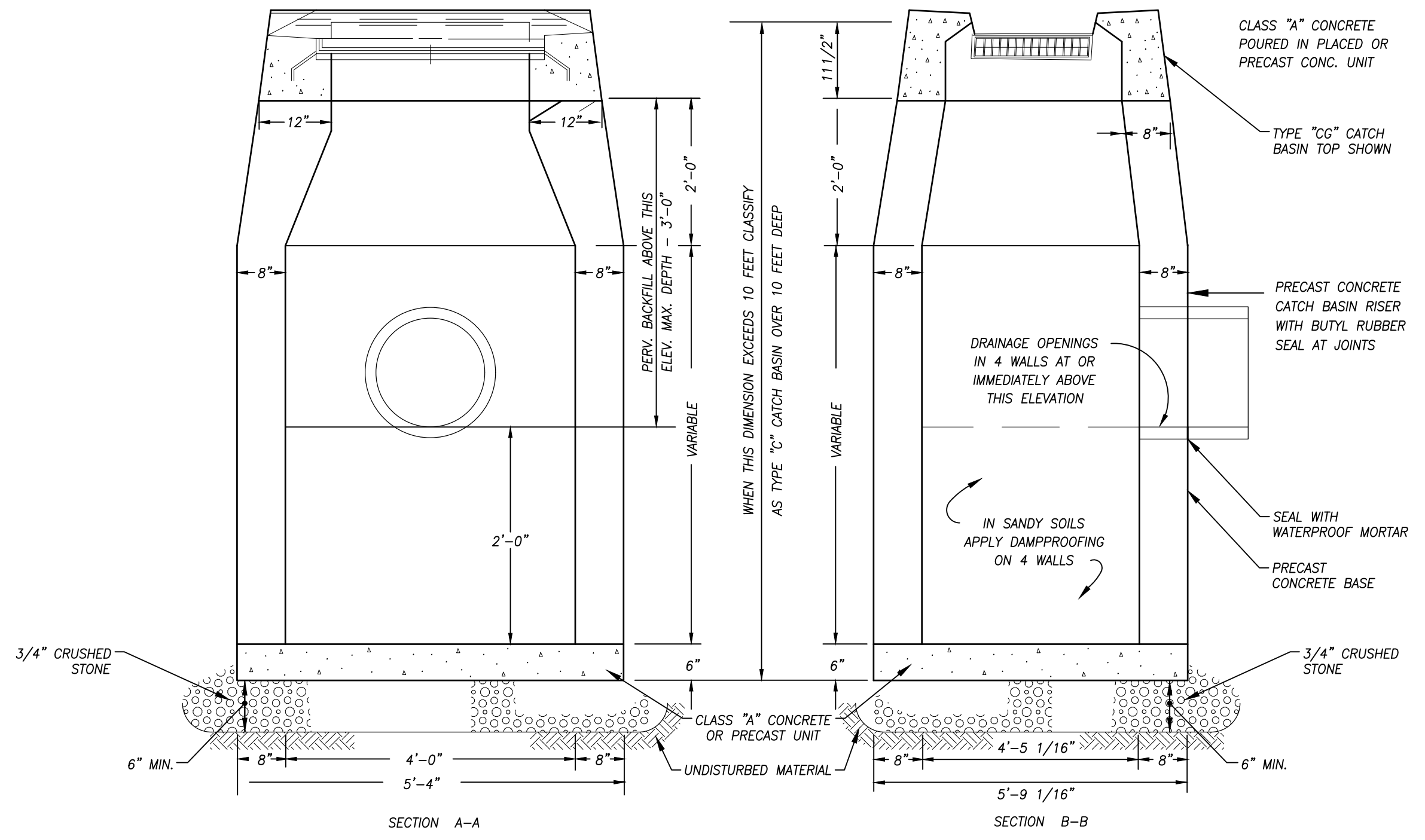
PLAN NOTES

1. SEE COVER SHEET FOR ENGINEER AND SURVEYOR SIGNATURES AND SEALS.
2. SEE SHEET 2 FOR LEGEND & ABBREVIATIONS.

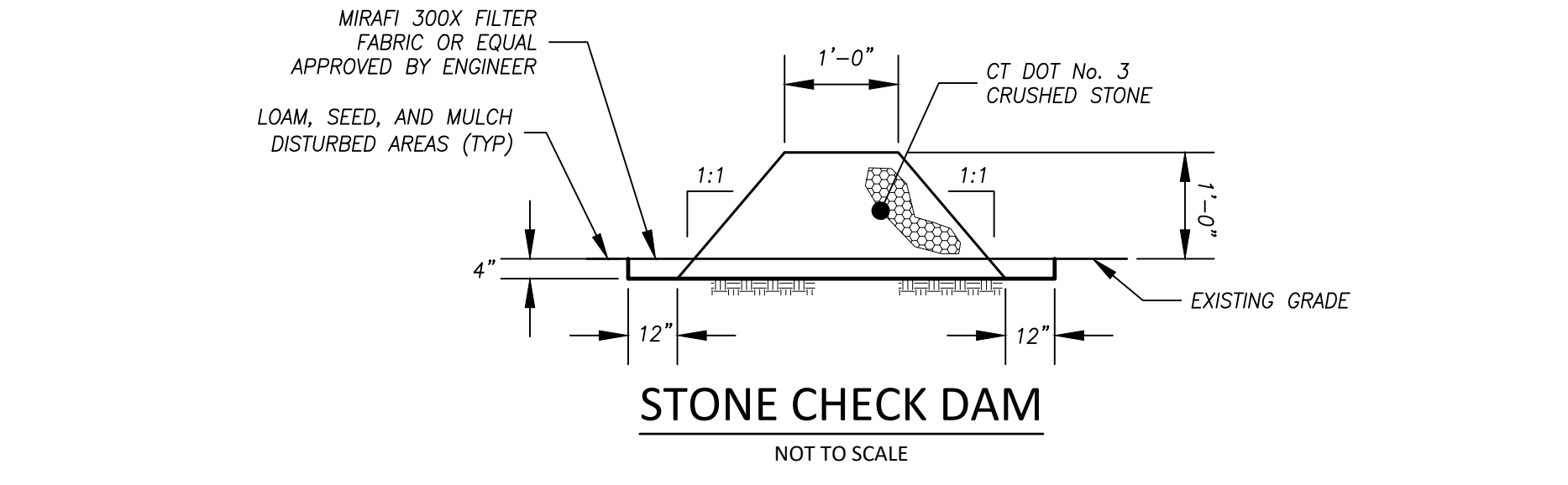
P:\CIVIL 3D PROJECTS\2020\20-2853 EDgewater-APARTMENTS\DWG\DESIGN\4 NOTES AND DETAILS.DWG



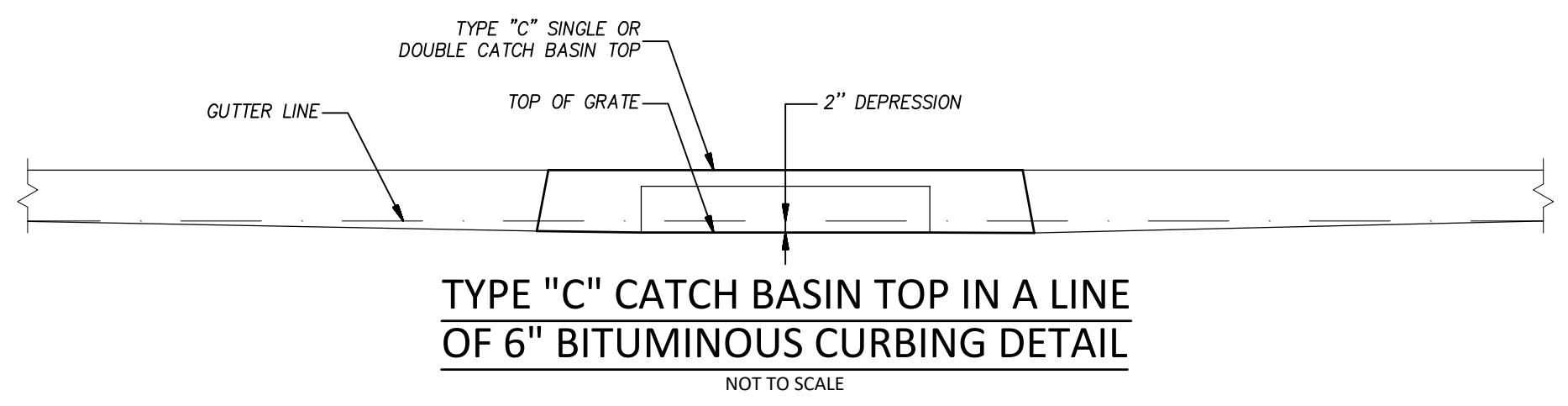
PRECAST CONCRETE STORM DRAIN MANHOLE DETAIL
 NOT TO SCALE



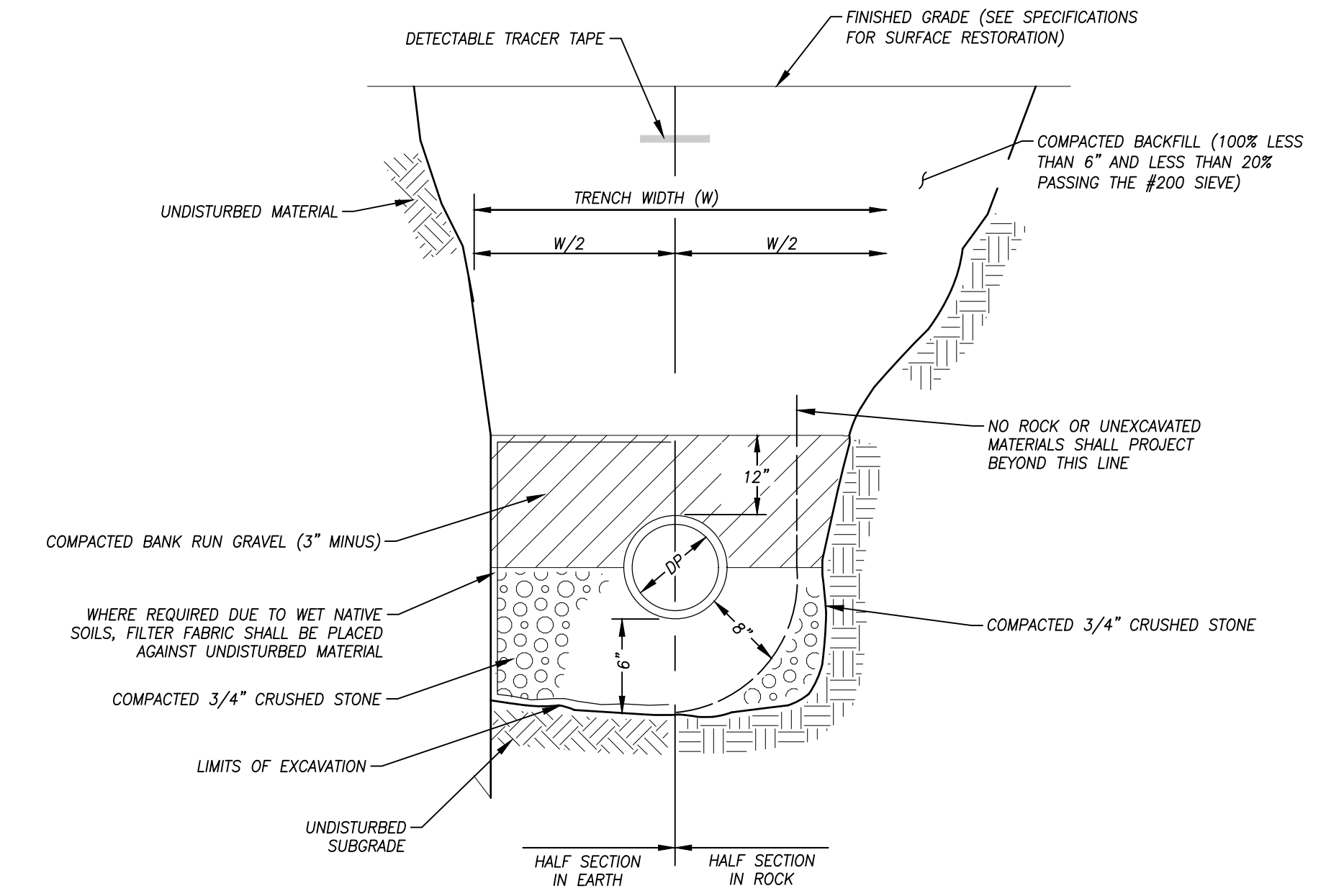
PRECAST CATCH BASIN DETAIL
 NOT TO SCALE



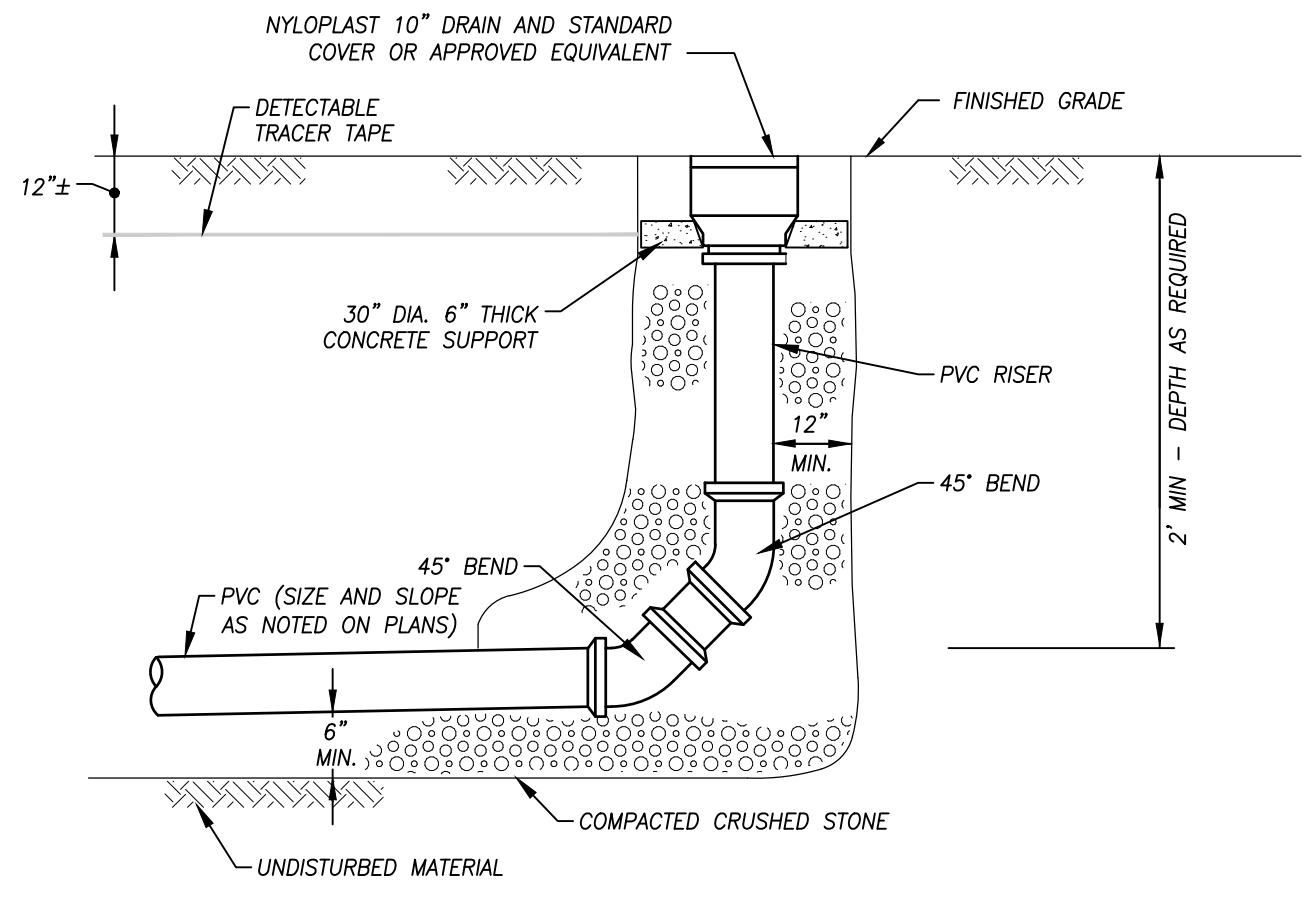
STONE CHECK DAM
 NOT TO SCALE



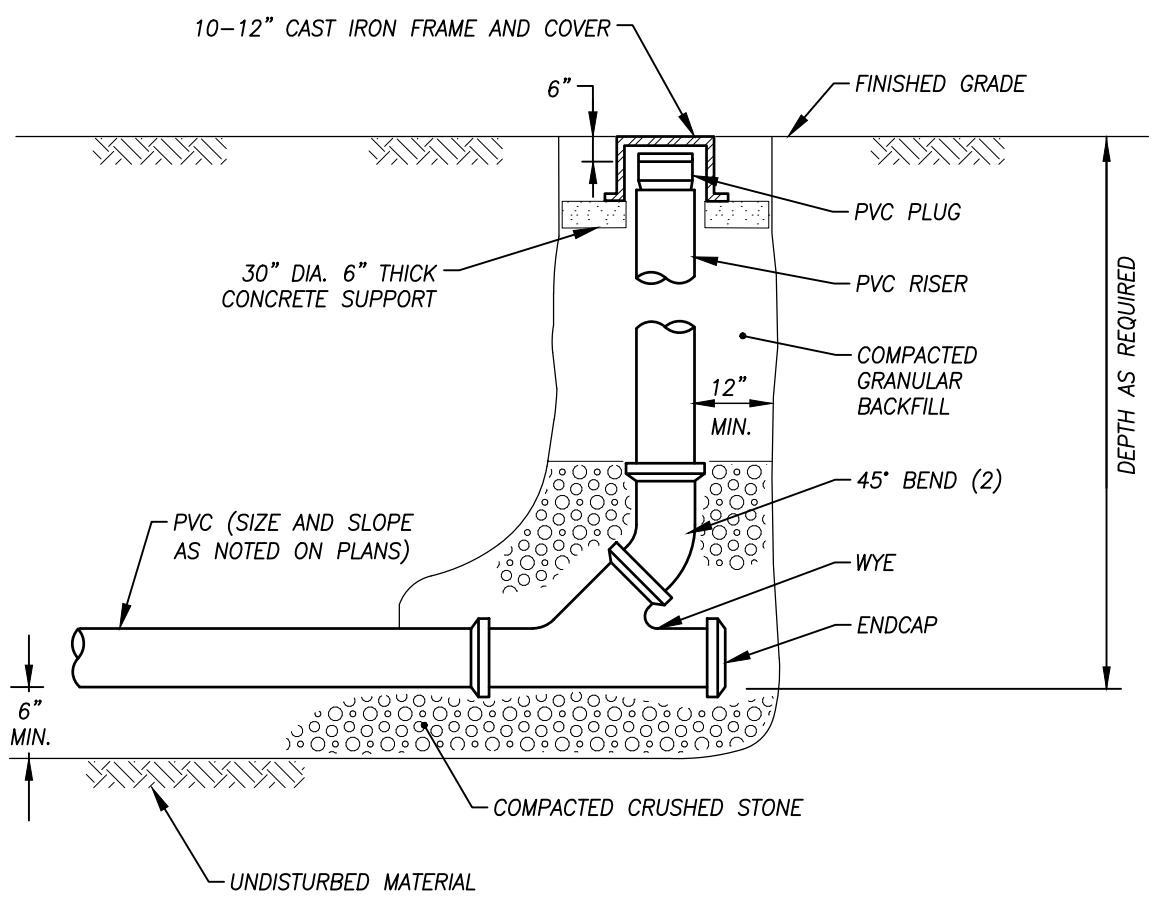
TYPE "C" CATCH BASIN TOP IN A LINE OF 6" BITUMINOUS CURBING DETAIL
 NOT TO SCALE



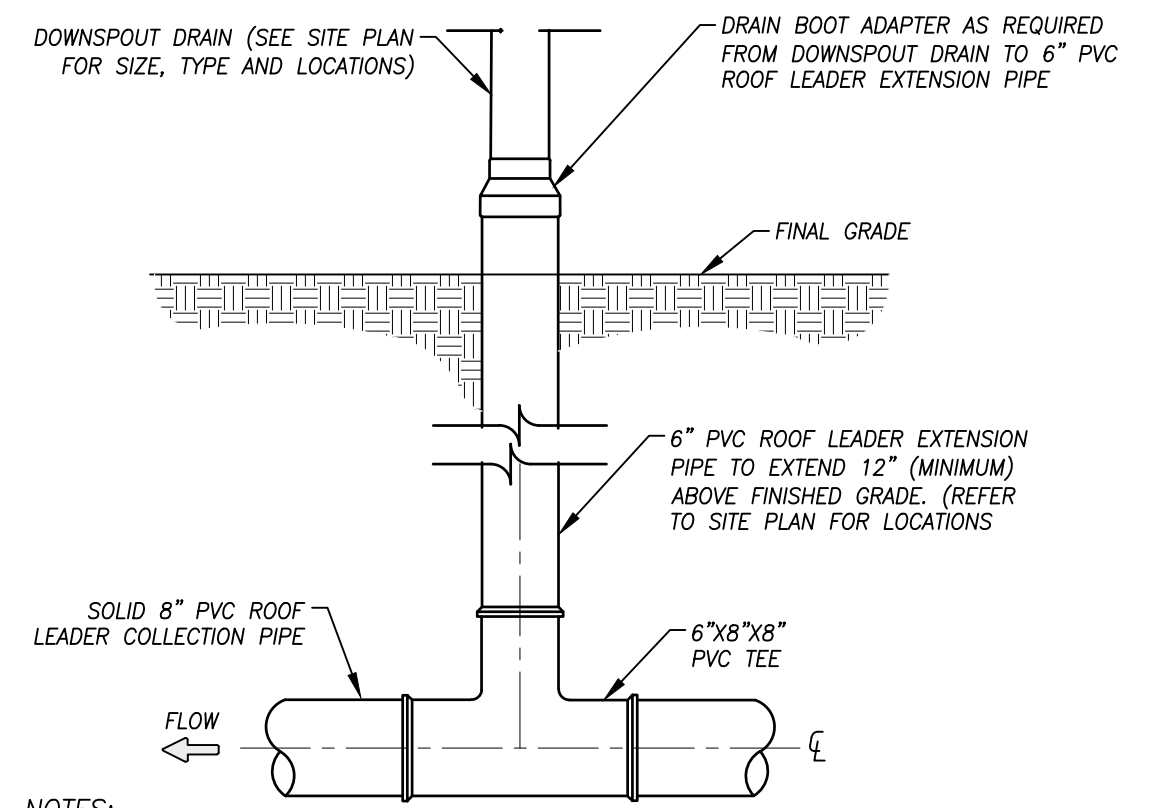
TRENCH DETAIL (STORM DRAINAGE)
 NOT TO SCALE



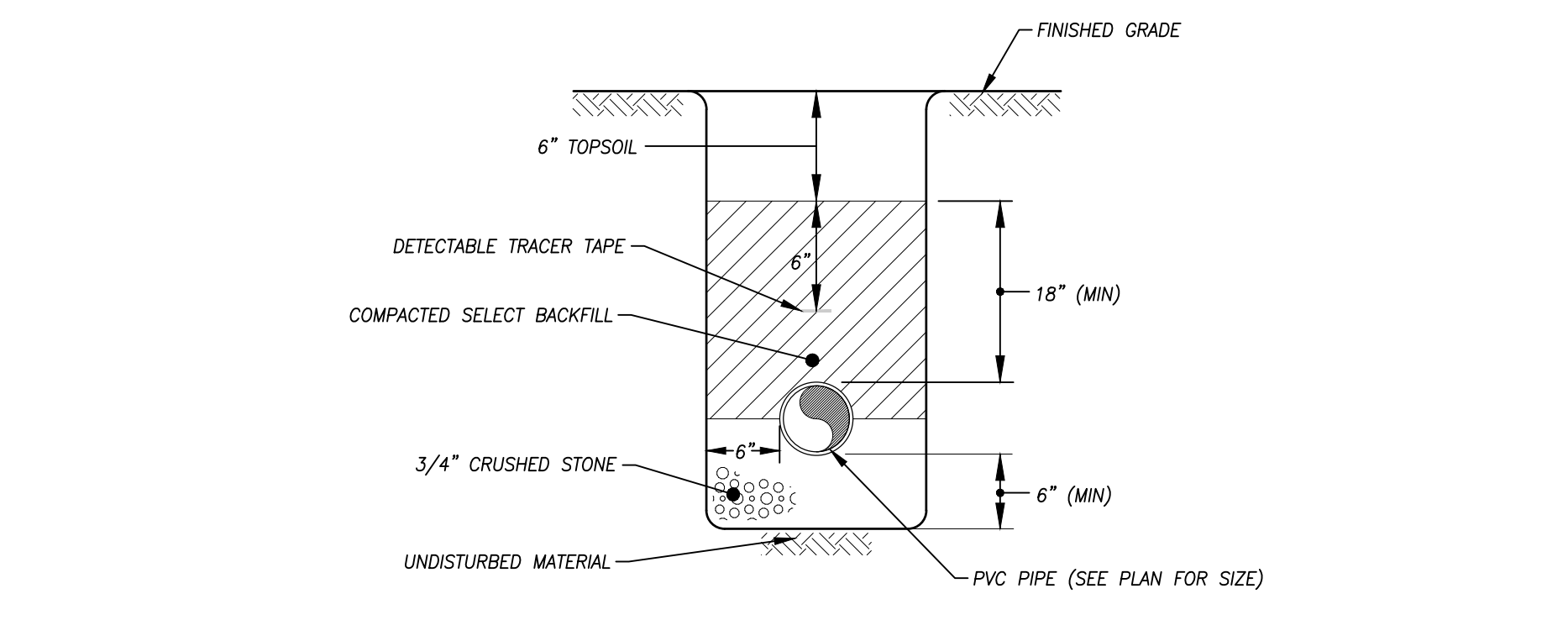
YARD DRAIN DETAIL
 NOT TO SCALE



CLEANOUT DETAIL
 NOT TO SCALE



DOWNSPOUT CONENCTION & PERIMETER ROOF DRAIN DETAIL
 NOT TO SCALE



YARD/ROOF DRAIN TRENCH DETAIL
 NOT TO SCALE

NOT FOR CONSTRUCTION
 1/15/2021

PLAN NOTES
 1. SEE COVER SHEET FOR ENGINEER AND SURVEYOR SIGNATURES AND SEALS.
 2. SEE SHEET 2 FOR LEGEND & ABBREVIATIONS.

SCALE:	As Noted
DATE:	December 2020
JOB I.D. NO.:	20-2853
Revisions	
Rev. A - IWWC Comments & Stormwater Quality - 1/18/21	

SHEET NO.

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 25